

STORM WATER & EROSION CONTROL CALCULATIONS FOR:

Montessori School

CITY OF WAUKESHA, WI Excel Job #: 1818660

BASED ON SCS TR-55 METHOD, MANNINGS EQUATION, AND SLAMM JULY 9, 2018



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OVERVIEW:

The proposed project is located on the northeast corner of University Avenue and Summit Avenue within the City of Waukesha, WI. This development involves the placement of a 18,500 sf school addition, parking lot reconfiguration and improvement to the existing parking lot on the east side of the site. The addition and parking area will be constructed over previously developed property. The project will combine the 3 existing lots into 1 overall property. The stormwater plan has accounted for all development shown on the plan. The existing site is being reconfigured and will meet city setback requirements. The existing zoning is I-1 Institutional — as part of City zoning code. The combined site is 8.42 acres and approximately 6 acres will be disturbed as part of the project.

The existing site generally drains from north to south into Summit Avenue's storm system. The post developed site will be routed with 100yr storm pipe to drain to the dry stormwater detention pond on the south side of the property and into the City storm system. A stormwater filter will be installed to treat the redeveloped site for TSS removal. The area consists of a portion of new and redevelopment, therefore the storm filter treats for the prorated amount. See the attached proposed stormwater calculations in Appendix E.

SOIL INFORMATION:

Existing Soils data: Soil Type: BsA: Brookston silt loam, 0-2% slopes, Hydro. Soil Rating C/D.

HmB: Hochheim Ioam, 2-6% slopes, Hydro Soil Rating D. HmC2: Hochheim Ioam, 6-12% slopes, Hydro Soil Rating D.

Soil classifications for the proposed property were taken off of the USDA Web Soil Survey. Please see attached hydrologic soil group map showing the soils within the drainage areas in Appendix C.

DRAINAGE CALCULATIONS:

Rainfall depths used for the runoff calculations were referenced from The City of Waukesha Stormwater Ordinance Chapter 32.11(a)2. Calculations use Type II distribution.

1-year: 2.3 inches 2-year: 2.7 inches 10-year: 4.0 inches 100-year: 5.6 inches

Curve Numbers: Impervious – 98 Lawn (B) – 61 Lawn (C) – 74 Lawn (D) – 80 Lawn (D) - 80

Woods (C) - 70

Woods (D) – 77

WATER QUANTITY

<u>City of Waukesha Requirements</u> – New development shall maintain or reduce the 2, 10, & 100-Year/24 hour post construction peak runoff discharge rates to the 2, 10, & 100-Year /24 hour predevelopment peak runoff discharge rates respectively. Peak discharge rates as required will be maintained or reduced as part of the project.

<u>Wisconsin Department of Natural Resources</u> – Maintain or reduce the 1-Year/24 hour and the 2-Year/24 hour post construction peak runoff discharge rates to the 1-Year/24 hour and the 2-Year/24 hour predevelopment peak runoff discharge rates respectively.

The analysis has detained the 1, 2, 10, and 100year flows to predevelopment levels with the use of a dry detention pond. The stormwater pond(s) will hold and treat the 100 year storm in the pond and discharge to the storm system prior to Summit Avenue storm system. The pond will tie into the existing stormwater catchbasin for connection to this system (See Appendix E for information). The peak discharge from the site to the existing square grate is maintained or reduced. See below for modeled data.

SITE RUNOFF SUMMARY:

Runoff Summary Chart for Detention Pond and Offsite flows (in cfs)

Storm (24-hour)	Pre-Development Basin A Runoff (cfs)	Total Post Development Runoff (cfs)	Pond Elevation
1- yr.	3.37	3.26	137.88
2-yr	4.78	4.71	138.15
10yr	9.98	7.99	138.97
100yr	17.03	16.09	139.80

WATER QUALITY

City of Waukesha & Wisconsin DNR Requirements

 Reduce total suspended solids load by 80 percent for new impervious and 40 percent for redevelopment as compared to no controls.

Since a portion of the site was previously developed, a prorated quality requirement has been calculated for the site. In the proposed condition, 5.73 acres will be disturbed. 2.63 acres will be redeveloped and 3.10 acres will be new development. Based on this information, a prorated requirement of 61.6% of the TSS will be required to be removed on site. See SLAMM map table in Appendix B.

Particulate Solids	Particulate Solids Yield after	Particulate
For drainage Area (lbs)	drainage and Controls (lbs)	<u>Removed</u>

Total Filter w/ offsite 1,595 573.20 1,021.80

SLAMM calculations show that the proposed development with offsite flows meets the quality requirement with a 15 filter UpfloFilter system. See Appendix F for calculations.

Results: 1,021.8/1,595 = 0.6406 => 64.06% Removed, therefore stormwater quality requirements are met.

INFILTRATION:

<u>City of Waukesha, Wisconsin and DNR Requirements (Redevelopment)</u> – site is exempt due to it being a redevelopment per NR 151.124(3)(b)3.

STORM SEWER PIPE DESIGN & 100-YEAR CONVEYANCE:

All storm pipes bringing water to the proposed pond were sized to convey the 100-year storm. See Appendix A, B, D, and E for calculations and basin map. The calculated 100-year storm event will be contained within the proposed stormwater management pond berm and will discharge over the banks after the 100year storm event to the south. Emergency overflows routes are provided on the north side of the site to convey runoff to the east and west of the building and ultimately overland to the pond.

EROSION AND SEDIMENT CONTROL:

The following are practices that will be used to control sediment during construction:

Silt Fence – Silt fence will be placed around the perimeter of the site for perimeter control as well as downhill of any disturbed areas where sheet flow will exist.

Tracking Pads – Stone tracking pads will be placed at all construction entrances to the site to ensure dirt and soil tracked onto public roads is limited.

Ditch Checks – Ditch checks will be provided to reduce the velocity of water flowing in ditch bottoms.

Erosion Matting – Erosion matting will be placed on any steep slopes as well as ditch bottoms to ensure that these areas are permanently stabilized over time.

The erosion control locations, specifications, construction sequence, site stabilization notes, and seeding notes can be seen on civil sheets C1.0 and C1.3.

POST CONSTRUCTION OPERATION AND MAINTENANCE PLAN FOR:

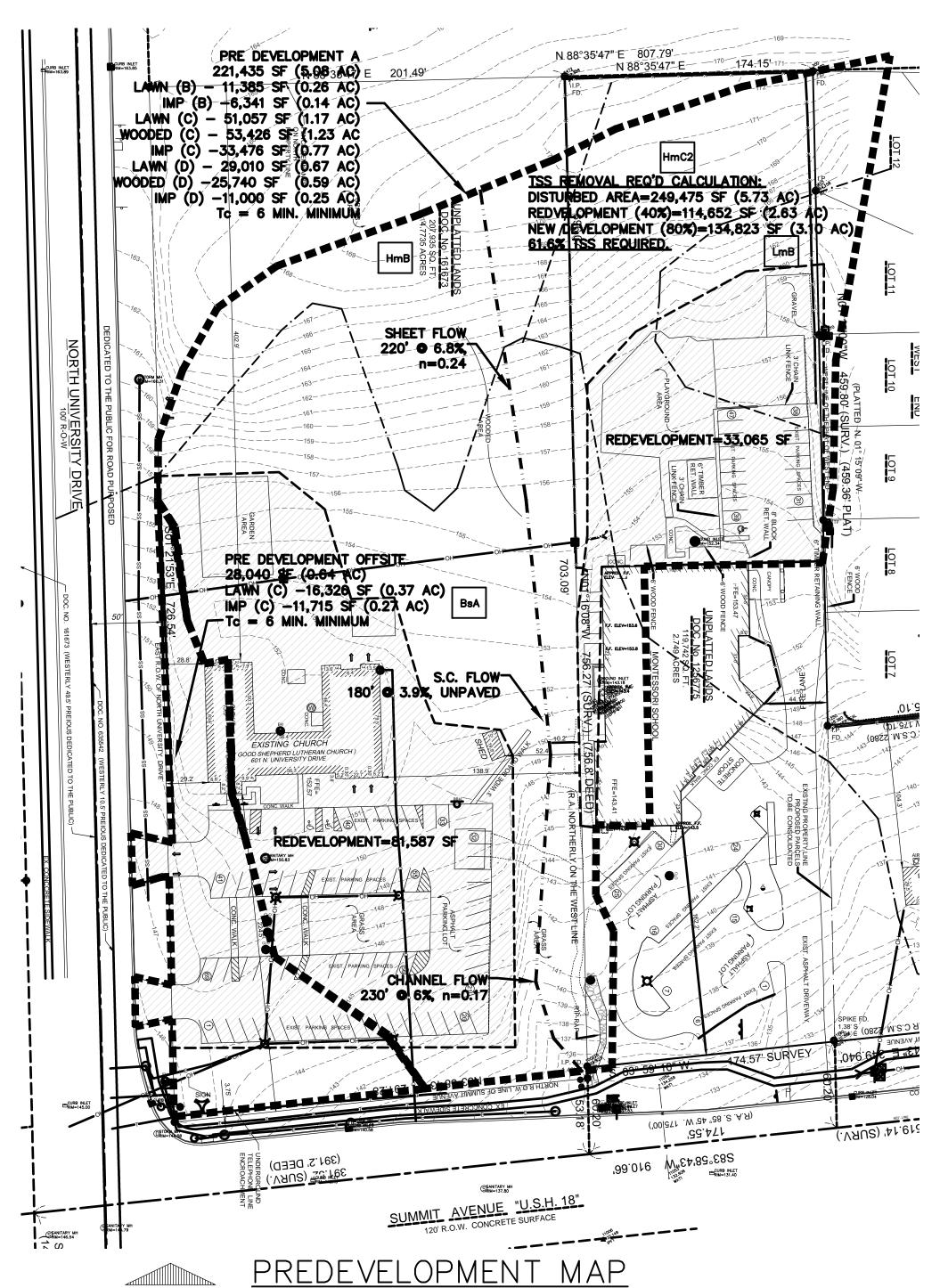
FAITH EVANGELICAL LUTHERAN CHURCH AND SCHOOL - 55 PRAIRIE ROAD

The owner of the property affected shall inspect and maintain the following stormwater management systems frequently, especially after heavy rainfalls, but at least on an annual basis

unless otherwise specifie	d.
STORMWATER	TYPE OF ACTION
FACILITY	
1. Lawn and Landscaped Areas	All lawn areas shall be kept clear of any materials that block the flow of stormwater. Rills and small gullies shall immediately be filled and seeded or have sod placed in them. The lawn shall be kept mowed, tree seedlings shall be removed, and litter shall be removed from landscaped areas.
2. Swales	All grassed swales showing signs of erosion, scour, or channelization shall be repaired, reinforced, and revegetated immediately. All swales shall be repaired to the original plan requirements. Mowing shall take place no less than twice per year at a height of no less than three inches. Grasses shall not be allowed to grow to a height that permits branching or bending. Mowing shall only take place when the ground is dry and able to support machinery.
3. Catch Basin Grates	The grate openings to these structures must be cleared of any clogging or the blocking of stormwater flow from getting into the stormwater conveyance system of any kind.
4. Catch Basin Sumps	Sumps shall visually be inspected every 3 months. Siltation shall be removed and disposed of offsite when the sump depth is within 3" of the outlet pipe invert elevation. The removal of siltation should occur a minimum of once per year.

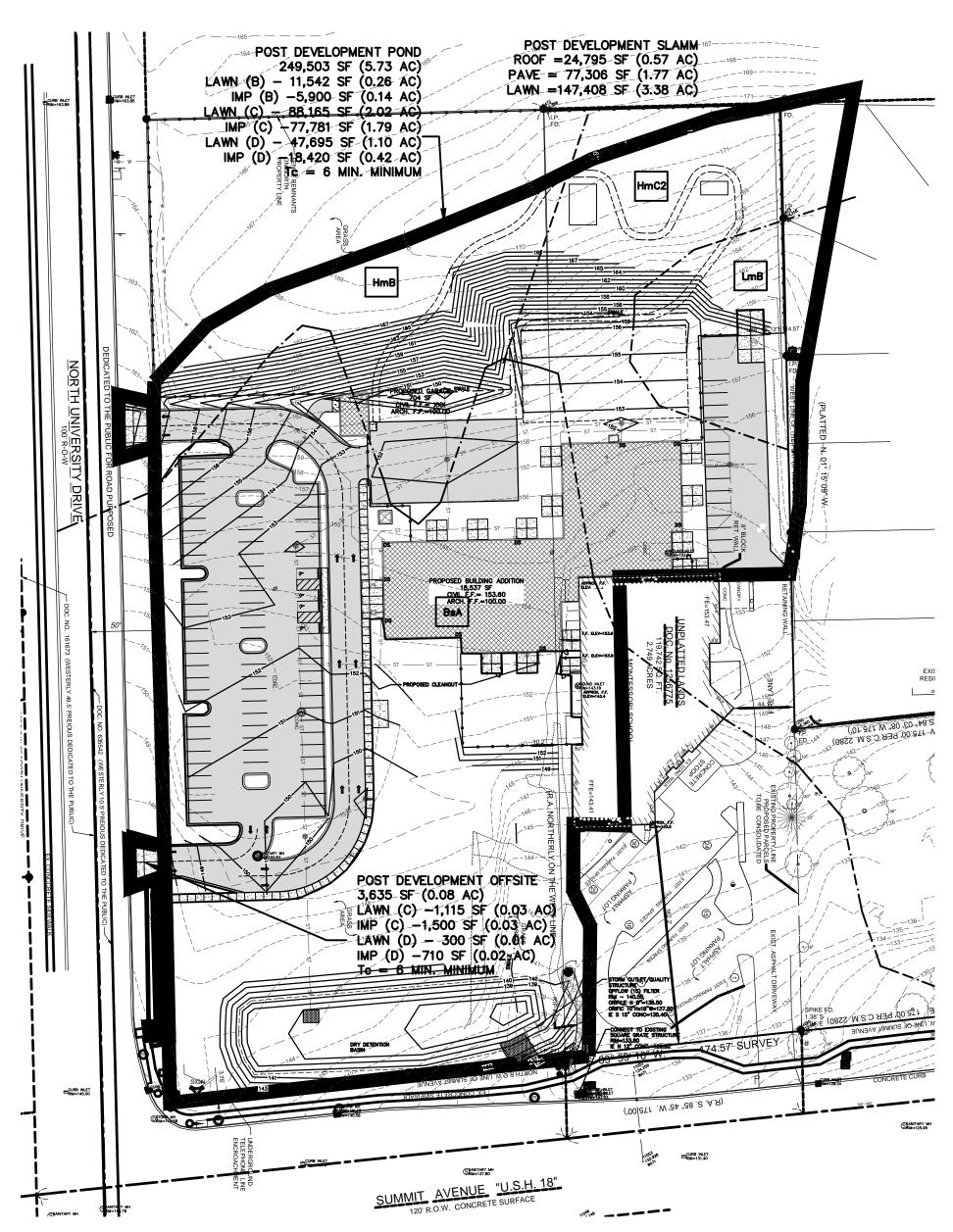
5. Detention Basin	Outlet structures, inlet and outlet pipes shall be kept clear of debris. Non-structurally sound devices shall be replaced. Floating litter and algae shall be removed monthly. All grassed areas, embankments, and flow control devices showing signs of erosion shall be repaired, reinforced, and revegetated immediately to the original plan requirements. Grasses shall not be allowed to grow to a height that permits branching or bending. Mowing shall only take place when the ground is dry and able to support machinery. Every 5 years, beginning in the first summer following completion of the basin (to be completed after detention basin is constructed), the elevations of the pond bottom shall be surveyed to determine the permanent pool depth and sediment depth in the pond. Cleaning, removal, and deposit of silt from the detention pond shall be done by means and methods acceptable to the Wisconsin Department of Natural Resources.
6. Hydro International Up-Flo Filter Quality Structures	Inspection of the structure shall be completed annually at a minimum by qualified maintenance personnel. Sediment in the bottom of the structure shall be inspected to verify sediment is less than 16" deep. If sediment is greater than 16" deep, the sediment shall be removed per Hydro International requirements. Qualified maintenance personnel shall enter structure to remove a Media Bag to be weighed. Media Bags weighing more than 40 lbs are an indication that the bag is full and need to be replaced. Replace per manufacturer specifications. Qualified maintenance personnel shall inspect the oil layer on the water surface to oil being entrained in the Media Bags. If the oil accumulation is greater than 1.5", the structure shall be pumped per manufacturer's specifications. After storm events of greater than 1" of rainfall, the structure shall be inspected 48 hours after the rainfall even to verify the water level inside the structure has dropped to below the base of the filter modules. If the water level has not dropped, the filters are considered to be clogged and shall be replaced per manufacturer's specifications. For further information, obtain Hydro International's Up-Flo Filter Operation and Maintenance Manual for details.
7. Record of	The operation and maintenance plan shall remain onsite and be
Maintenance	available for inspection when requested by WDNR and the City of
	Waukesha. When requested, the owner shall make available for inspection all maintenance records to the department or agent for the
	life of the system.
	ine of the system.

Appendix A Pre-Development Area(s):



NORTH SCALE (11"X17"): 1"=60'-0"

Appendix B Post Development Area(s):



NORTH POST DEVELOPMENT MAP

SCALE (11"X17"): 1"=60'-0"

Appendix C Soil Maps & Boring Data



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:15.800. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: Milwaukee and Waukesha Counties, Wisconsin C/D Survey Area Data: Version 13, Oct 6, 2017 Soil map units are labeled (as space allows) for map scales D 1:50,000 or larger. Not rated or not available Date(s) aerial images were photographed: Sep 7, 2014—Sep **Soil Rating Points** 22, 2014 The orthophoto or other base map on which the soil lines were A/D compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
BsA	Brookston silt loam, 0 to 2 percent slopes	C/D	5.9	41.0%
HmB	Hochheim loam, 2 to 6 percent slopes	D	2.7	18.8%
HmC2	Hochheim loam, 6 to 12 percent slopes, eroded	D	3.8	26.6%
KIA	Kendall silt loam, 1 to 3 percent slopes	С	0.6	4.4%
LmB	Lamartine silt loam, 0 to 3 percent slopes	B/D	1.3	9.2%
Totals for Area of Inter	rest	14.4	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

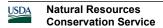
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

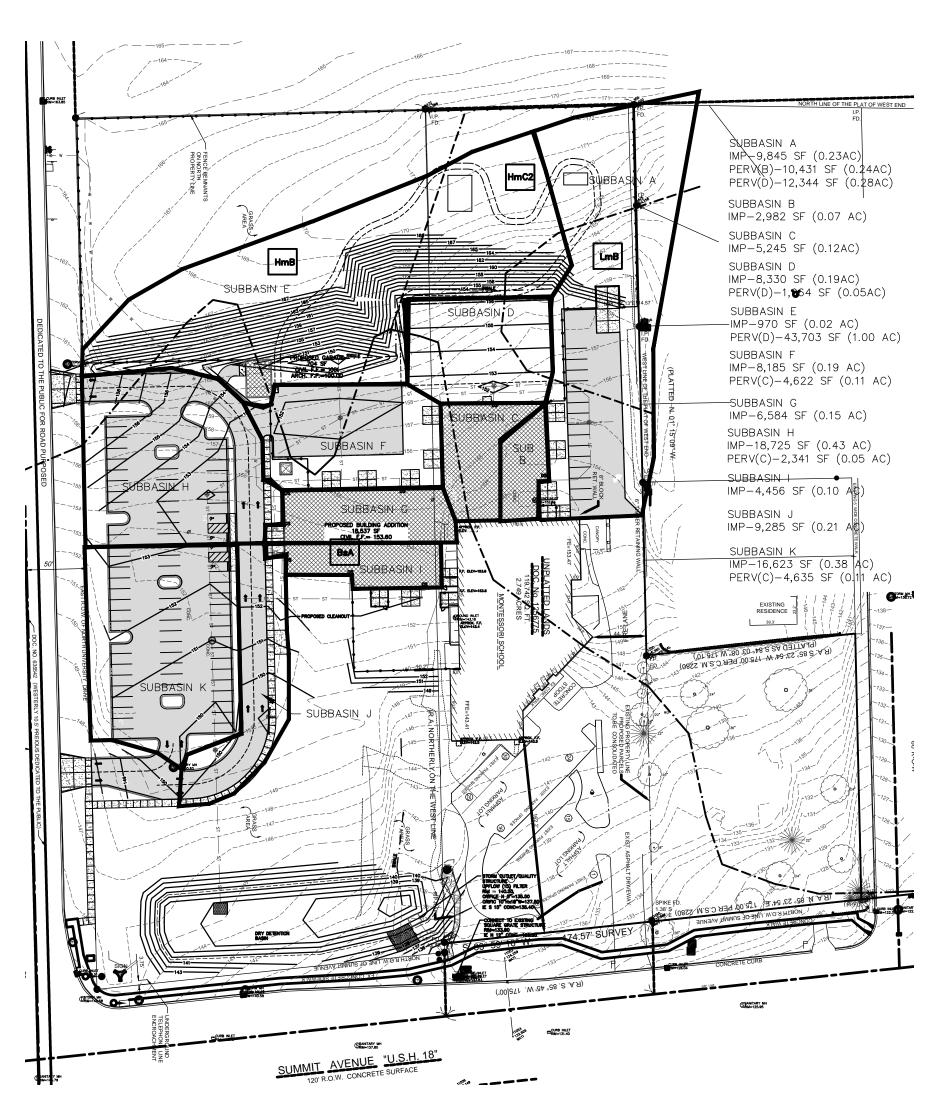
Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Appendix D Pipe Capacity Calculations







Excel Engineering Project No.

1818660

Project Name Montessori School - Waukesha

	Pi	pe Data		Pipe Capacity (100-yr)					
Pipe No.	Diameter (FT)	Slope (FT/FT)	Manning's n	Basin No.	Total Flow (cfs)	Total Flow (gpm)	Full Flow Capacity (cfs)	Full Flow Capacity (gpm)	
1	0.67	0.005	0.012	В	0.49	220	0.94	422	
2	1.25	0.005	0.012	А, В	4.23	1898	4.96	2227	
3	0.67	0.005	0.012	С	0.83	373	0.94	422	
4	1.5	0.005	0.012	A, B, C,D	6.67	2993	8.07	3621	
5	0.67	0.010	0.012	G	1.04	467	1.33	597	
6	1.25	0.015	0.012	Е	5.23	2347	8.59	3857	
7	2	0.005	0.012	A,B,C,D,E,F,G	14.82	6651	17.38	7798	
8	0.67	0.010	0.012	1	0.69	310	1.33	597	
9	2	0.008	0.012	A,B,C,D,E,F,G,I,H	18.80	8437	21.98	9864	
10	0.83	0.014	0.012	J	1.46	655	2.79	1250	
11	2	0.055	0.012	A,B,C,D,E,F,G,I,H,J,K	23.51	10551	57.63	25864	

Full Flow Capacity based off Manning's Equation

$$Q = \frac{1.49}{n} R^{2/3} S^{1/2} a$$

Where: Q = Full Flow Capacity of Pipe (cfs)

n = manning's roughness coefficient

R = hydraulic radius (ft) (D/4)

s = hydraulic gradient, slope (ft/ft)

a = flow area (sq. ft.)

Typical Manning's n

HDPE 0.012
PVC 0.012
Concrete 0.013
CMP 0.024

^{*}Total Flow calculated via TR-55 hydrologic calculations. Reference Storm Pipe Basin Map & TR-55 Calculations

Appendix E <u>SCS TR55</u> <u>Stormwater Management</u> <u>Calculations-Tail water:</u>

- o Hydrograph Return Period Recap
- o Hydrograph Summary Reports
- Hydrograph Plots
- o Hydrograph Tc Worksheets

Hydrograph Return Period Recap Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

-	Hydrograph							Hydrograph			
0.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff		3.370	4.778			9.980			17.03	Pre-Basin A
2	SCS Runoff		0.921	1.226			2.277			3.617	Pre-Offsite
3	Combine	1, 2	3.676	5.219			10.82			18.32	Total Predevelopment
5	SCS Runoff		8.247	10.98			20.39			32.38	Post- Pond
6	SCS Runoff		0.130	0.172			0.320			0.509	Post- Offsite
•	Reservoir	5	3.204	4.642			7.874			15.91	Pond Discharge
)	Combine	6, 7,	3.256	4.709			7.993			16.09	Total Post Discharge
2	SCS Runoff		0.780	1.083			2.218			3.742	SUBBASIN A
3	SCS Runoff		0.196	0.231			0.346			0.486	SUBBASIN B
4	SCS Runoff		0.336	0.396			0.592			0.833	SUBBASIN C
5	SCS Runoff		0.588	0.714			1.120			1.613	SUBBASIN D
6	SCS Runoff		1.135	1.558			3.138			5.227	SUBBASIN E
7	SCS Runoff		0.579	0.733			1.245			1.875	SUBBASIN F
8	SCS Runoff		0.419	0.495			0.741			1.041	SUBBASIN G
9	SCS Runoff		1.269	1.517			2.316			3.289	SUBBASIN H
0	SCS Runoff		0.280	0.330			0.494			0.694	SUBBASIN I
21	SCS Runoff		0.587	0.693			1.037			1.458	SUBBASIN J
2	SCS Runoff		1.150	1.408			2.241			3.254	SUBBASIN K

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Monday, 07 / 9 / 2018

Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	3.370	3	729	12,701				Pre-Basin A
2	SCS Runoff	0.921	3	717	2,098				Pre-Offsite
3	Combine	3.676	3	726	14,799	1, 2			Total Predevelopment
5	SCS Runoff	8.247	3	717	18,781				Post- Pond
6	SCS Runoff	0.130	3	717	295				Post- Offsite
7	Reservoir	3.204	3	726	18,780	5	137.88	4,778	Pond Discharge
9	Combine	3.256	3	726	19,075	6, 7,			Total Post Discharge
12	SCS Runoff	0.780	3	720	1,803				SUBBASIN A
13	SCS Runoff	0.196	3	717	494				SUBBASIN B
14	SCS Runoff	0.336	3	717	846				SUBBASIN C
15	SCS Runoff	0.588	3	717	1,371				SUBBASIN D
16	SCS Runoff	1.135	3	720	2,615				SUBBASIN E
17	SCS Runoff	0.579	3	717	1,308				SUBBASIN F
18	SCS Runoff	0.419	3	717	1,058				SUBBASIN G
19	SCS Runoff	1.269	3	717	3,048				SUBBASIN H
20	SCS Runoff	0.280	3	717	705				SUBBASIN I
21	SCS Runoff	0.587	3	717	1,481				SUBBASIN J
22	SCS Runoff	1.150	3	717	2,655				SUBBASIN K
181	8660STORN	1.gpw			Return I	Period: 1 Ye	ear	Monday, 0	7 / 9 / 2018

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

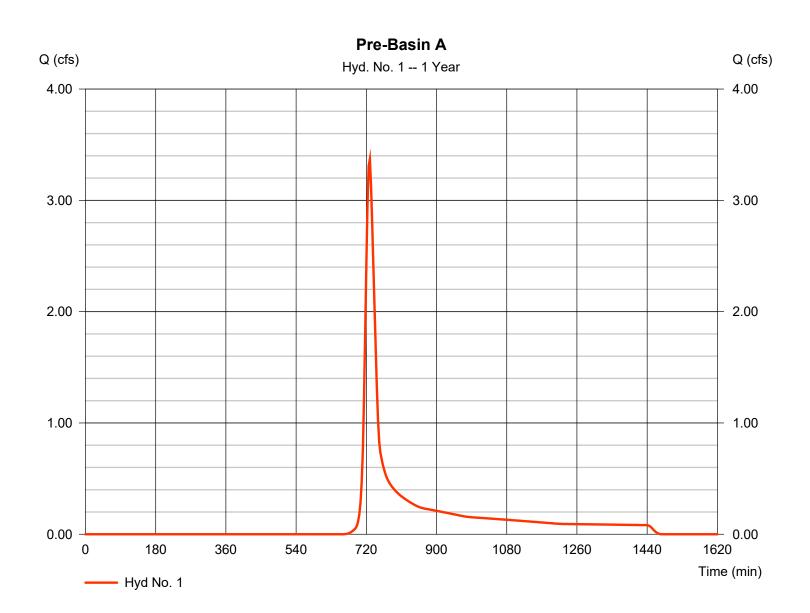
Monday, 07 / 9 / 2018

Hyd. No. 1

Pre-Basin A

Hydrograph type = SCS Runoff Peak discharge = 3.370 cfsStorm frequency Time to peak = 729 min = 1 yrsTime interval = 3 min Hyd. volume = 12.701 cuftCurve number Drainage area = 5.080 ac= 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.40 min = TR55 Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (1.160 \times 98) + (1.170 \times 74) + (1.230 \times 70) + (0.670 \times 80) + (0.590 \times 77)] / 5.080$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Hyd. No. 1

Pre-Basin A

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 220.0 = 2.54 = 6.80		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 18.45	+	0.00	+	0.00	=	18.45
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 180.00 = 3.90 = Unpaved =3.19	I	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.94	+	0.00	+	0.00	=	0.94
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 20.00 = 24.00 = 6.00 = 0.170 =1.90		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})230.0		0.0		0.0		
Travel Time (min)	= 2.02	+	0.00	+	0.00	=	2.02
Total Travel Time, Tc							

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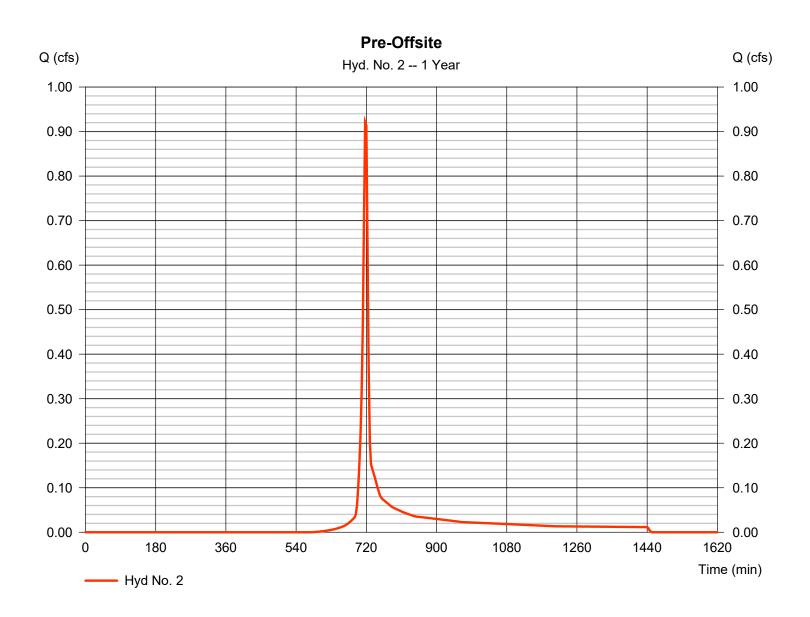
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Hyd. No. 2

Pre-Offsite

Hydrograph type = SCS Runoff Peak discharge = 0.921 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 2.098 cuft Drainage area Curve number = 0.640 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.370 x 74) + (0.270 x 98)] / 0.640



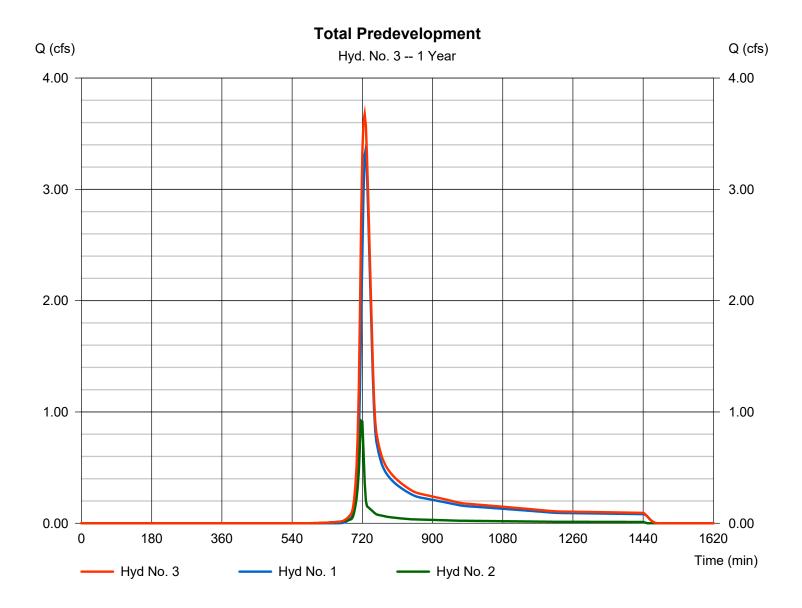
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Hyd. No. 3

Total Predevelopment

Hydrograph type = Combine Peak discharge = 3.676 cfsTime to peak Storm frequency = 1 yrs= 726 min Time interval = 3 min Hyd. volume = 14,799 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 5.720 ac



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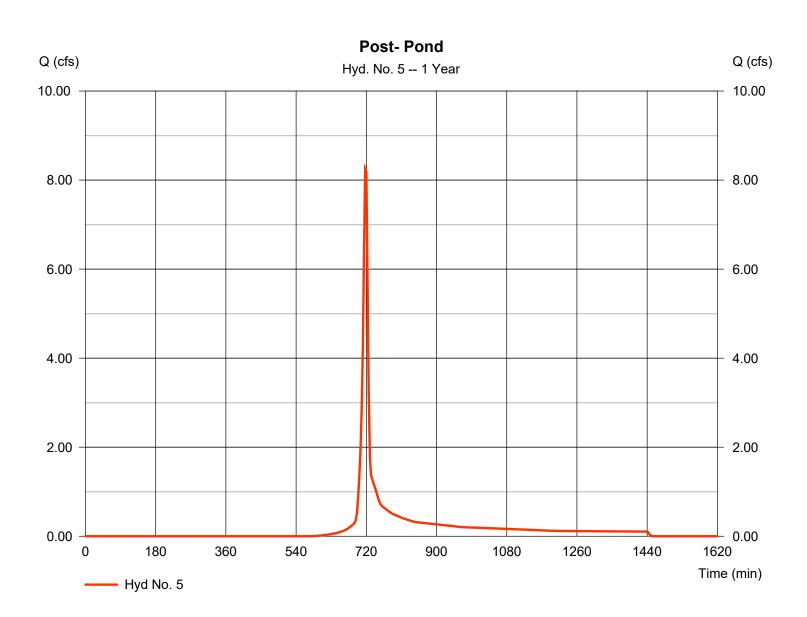
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Hyd. No. 5

Post-Pond

Hydrograph type = SCS Runoff Peak discharge = 8.247 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 18.781 cuft Curve number Drainage area = 5.730 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.30 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (2.350 \times 98) + (2.020 \times 74) + (1.100 \times 80)] / 5.730$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

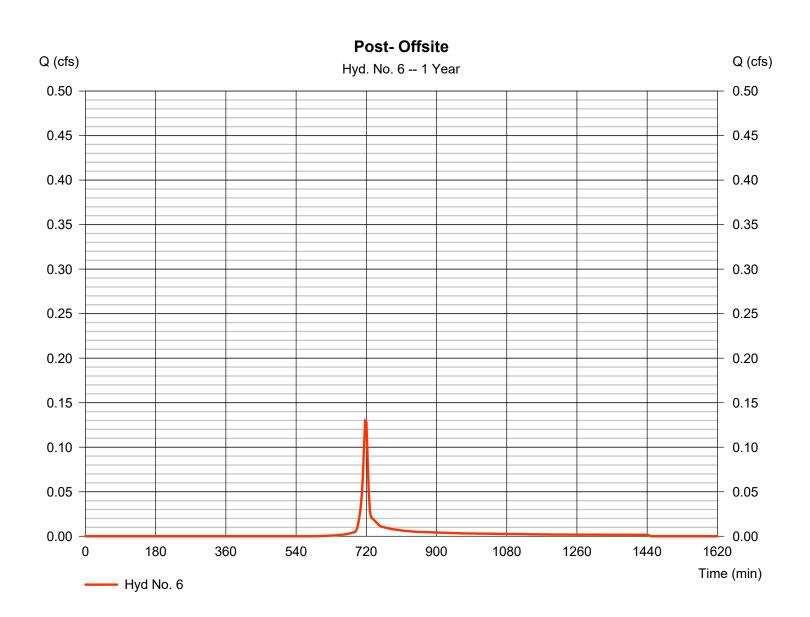
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Hyd. No. 6

Post- Offsite

Hydrograph type = SCS Runoff Peak discharge = 0.130 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 295 cuft Curve number Drainage area = 0.090 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.030 \times 61) + (0.050 \times 98) + (0.010 \times 80)] / 0.090$



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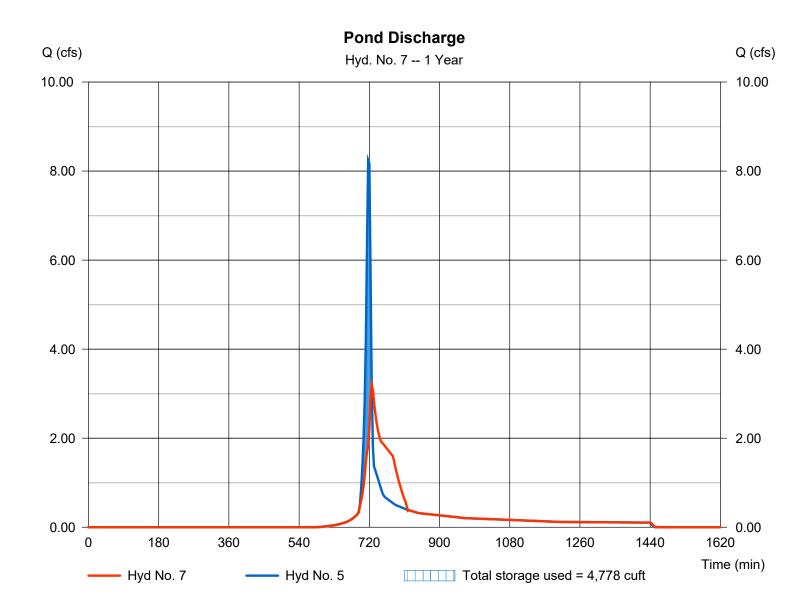
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Hyd. No. 7

Pond Discharge

Hydrograph type = Reservoir Peak discharge = 3.204 cfsStorm frequency Time to peak = 726 min = 1 yrsTime interval = 3 min Hyd. volume = 18,780 cuftInflow hyd. No. = 5 - Post- Pond Max. Elevation = 137.88 ft= South Detention Reservoir name Max. Storage = 4,778 cuft

Storage Indication method used.



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Monday, 07 / 9 / 2018

Pond No. 1 - South Detention

Pond Data

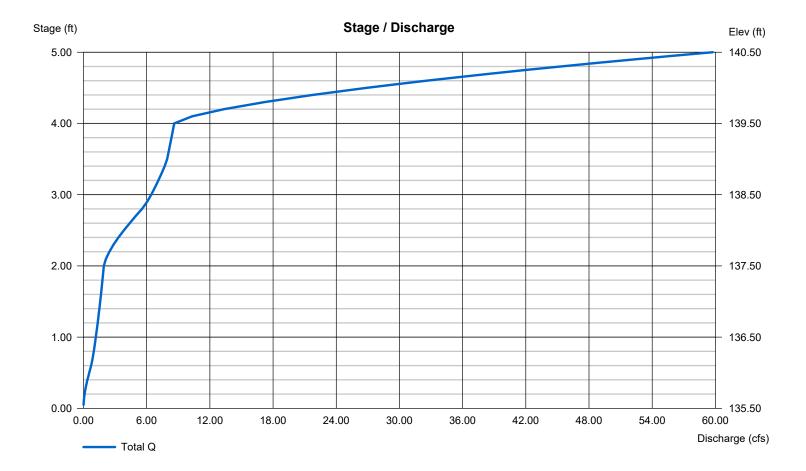
Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 135.50 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	135.50	10	0	0
0.50	136.00	188	40	40
1.50	137.00	2,340	1,064	1,104
2.50	138.00	6,390	4,199	5,302
3.50	139.00	9,411	7,851	13,154
4.50	140.00	11,707	10,537	23,691
5.00	140.50	13,070	6,191	29,881

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] 0.00 Rise (in) = 15.00 8.00 10.00 0.00 Crest Len (ft) = 15.00 0.00 0.00 Span (in) = 15.00 8.00 18.00 0.00 Crest El. (ft) = 139.50 0.00 0.00 0.00 3.33 No. Barrels = 1 0 Weir Coeff. = 3.333.33 3.33 135.50 Invert El. (ft) = 135.50 137.50 0.00 Weir Type = Rect Length (ft) = 55.00 0.00 0.00 0.00 Multi-Stage = No No No No = 11.00 0.00 Slope (%) 0.00 n/a = .013 N-Value .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Contour) = 0.00Multi-Stage = n/aYes Yes No TW Elev. (ft)

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



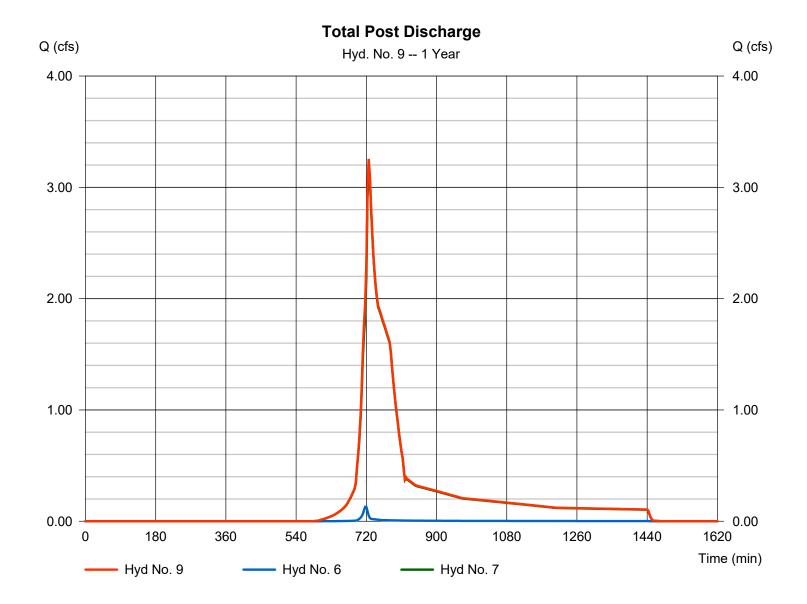
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Hyd. No. 9

Total Post Discharge

Hydrograph type = Combine Peak discharge = 3.256 cfsTime to peak Storm frequency = 1 yrs= 726 min Time interval = 3 min Hyd. volume = 19,075 cuft Inflow hyds. = 6, 7 = 0.090 ac Contrib. drain. area



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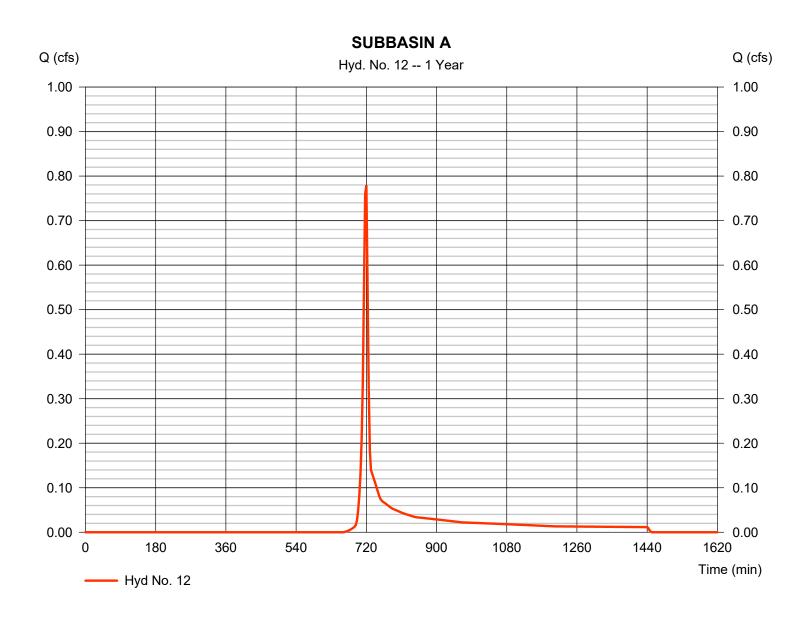
Monday, 07 / 9 / 2018

Hyd. No. 12

SUBBASIN A

Hydrograph type = SCS Runoff Peak discharge = 0.780 cfsStorm frequency Time to peak = 720 min = 1 yrsTime interval = 3 min Hyd. volume = 1.803 cuft Curve number Drainage area = 0.750 ac= 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.230 \times 98) + (0.240 \times 61) + (0.280 \times 80)] / 0.750$



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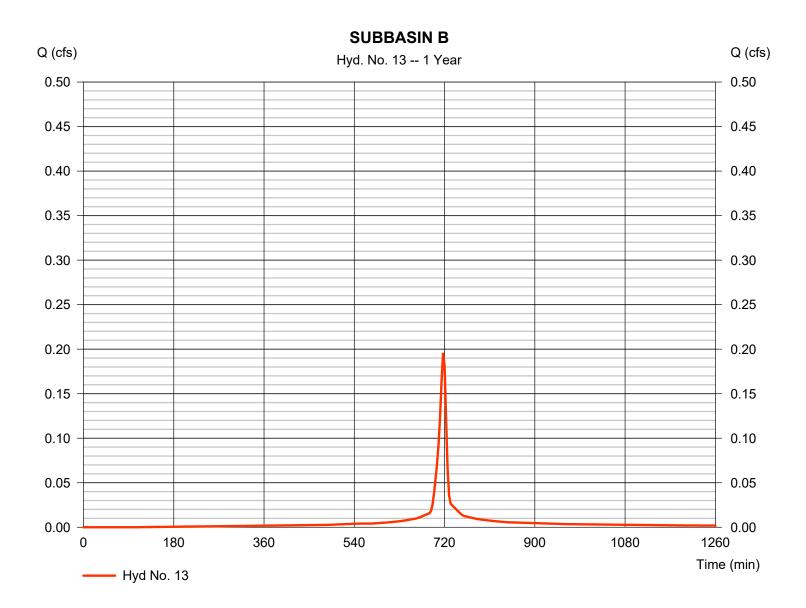
Monday, 07 / 9 / 2018

Hyd. No. 13

SUBBASIN B

Hydrograph type = SCS Runoff Peak discharge = 0.196 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 494 cuft Curve number Drainage area = 0.070 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.070 x 98)] / 0.070



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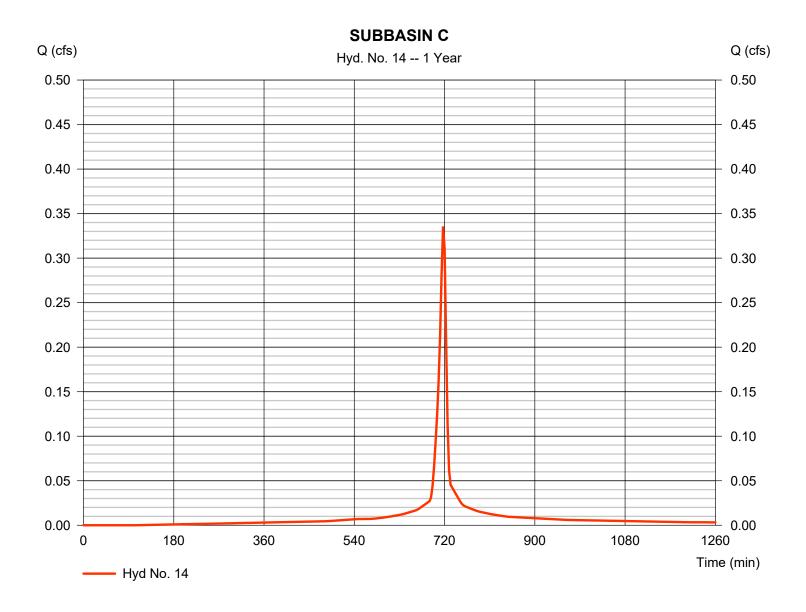
Monday, 07 / 9 / 2018

Hyd. No. 14

SUBBASIN C

Hydrograph type = SCS Runoff Peak discharge = 0.336 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 846 cuft Curve number Drainage area = 0.120 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.120 x 98)] / 0.120



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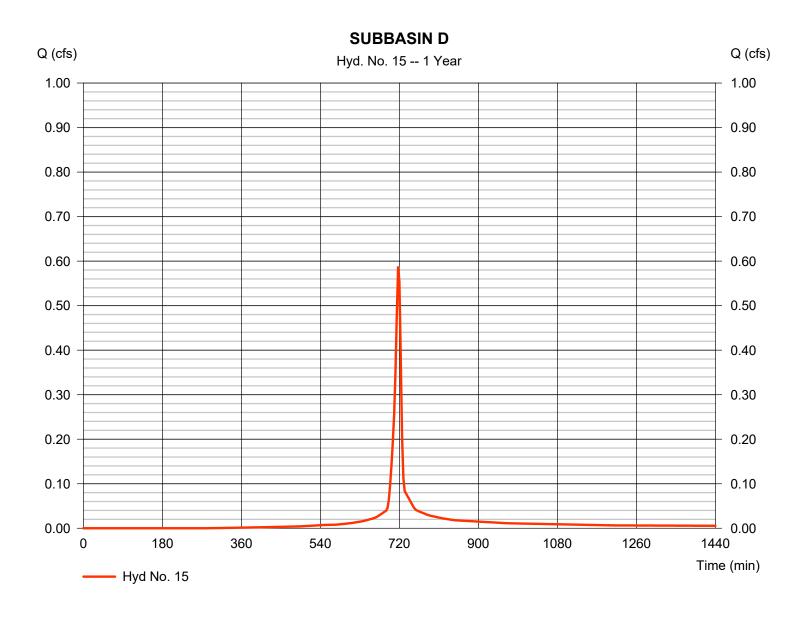
Monday, 07 / 9 / 2018

Hyd. No. 15

SUBBASIN D

Hydrograph type = SCS Runoff Peak discharge = 0.588 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 1.371 cuft Curve number Drainage area = 0.240 ac= 94* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.050 \times 80)] / 0.240$



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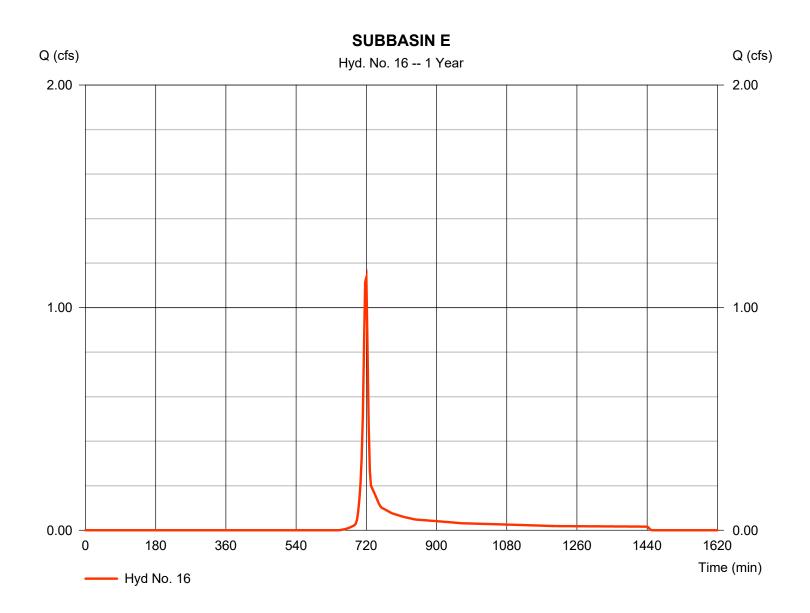
Monday, 07 / 9 / 2018

Hyd. No. 16

SUBBASIN E

Hydrograph type = SCS Runoff Peak discharge = 1.135 cfsStorm frequency Time to peak = 720 min = 1 yrsTime interval = 3 min Hyd. volume = 2,615 cuftCurve number Drainage area = 1.020 ac= 80* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.30 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.020 x 98) + (1.000 x 80)] / 1.020



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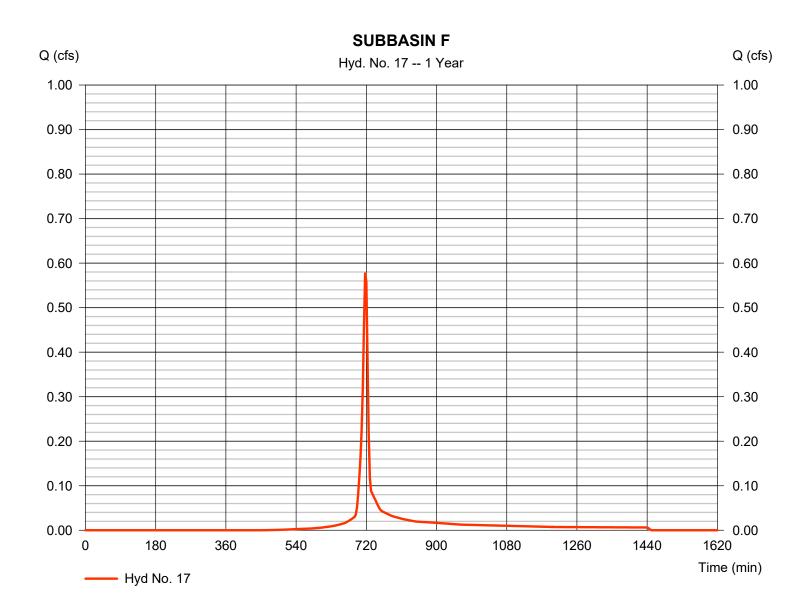
Monday, 07 / 9 / 2018

Hyd. No. 17

SUBBASIN F

Hydrograph type = SCS Runoff Peak discharge = 0.579 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 1.308 cuft Curve number Drainage area = 0.300 ac= 89* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.110 \times 74)] / 0.300$



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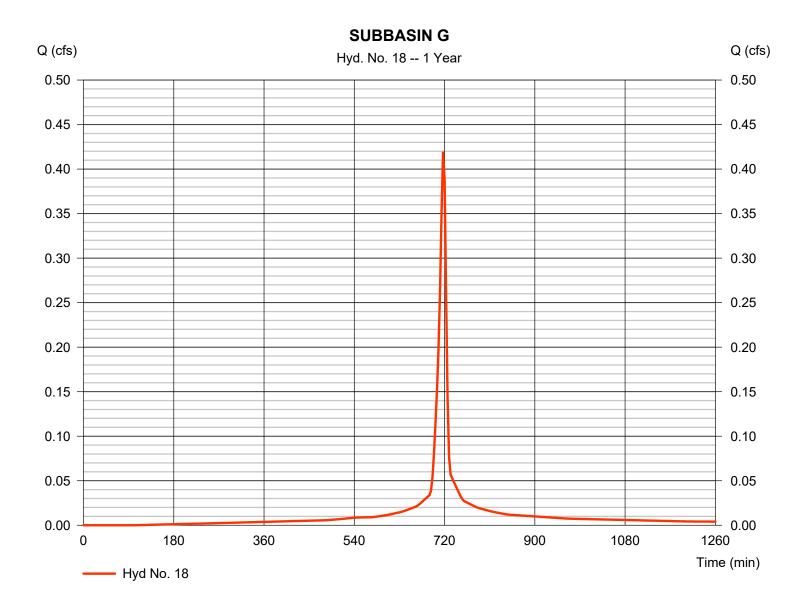
Monday, 07 / 9 / 2018

Hyd. No. 18

SUBBASIN G

Hydrograph type = SCS Runoff Peak discharge = 0.419 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 1.058 cuft Curve number Drainage area = 0.150 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.150 x 98)] / 0.150



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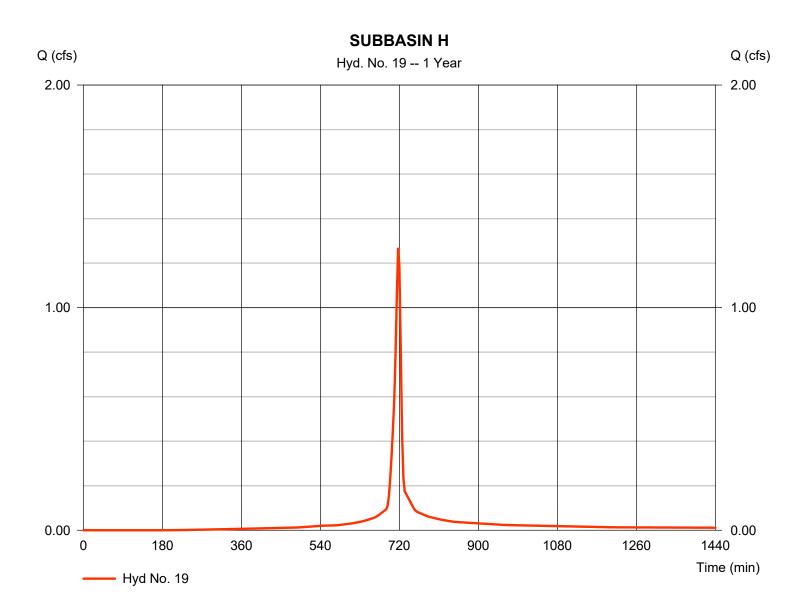
Monday, 07 / 9 / 2018

Hyd. No. 19

SUBBASIN H

Hydrograph type = SCS Runoff Peak discharge = 1.269 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 3,048 cuftCurve number Drainage area = 0.480 ac= 96* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.430 \times 98) + (0.050 \times 74)] / 0.480$



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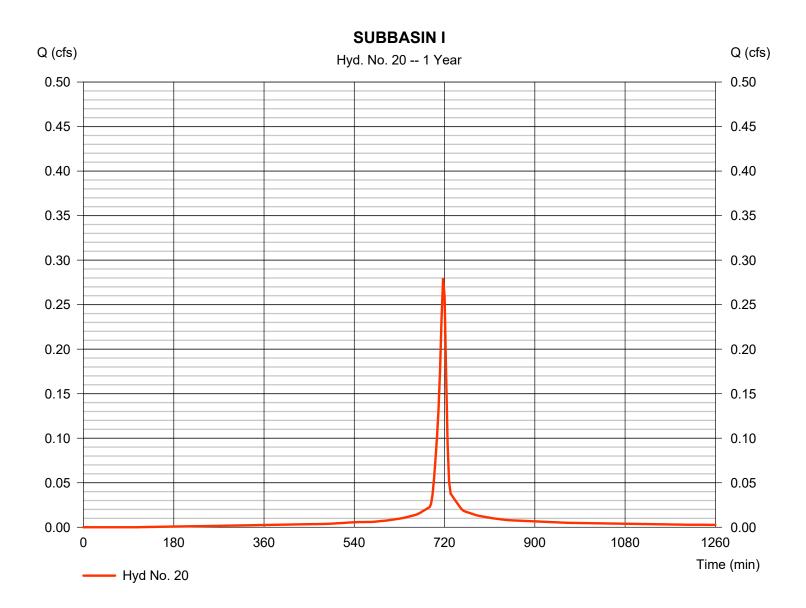
Monday, 07 / 9 / 2018

Hyd. No. 20

SUBBASIN I

Hydrograph type = SCS Runoff Peak discharge = 0.280 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 705 cuft Curve number Drainage area = 0.100 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.100 x 98)] / 0.100



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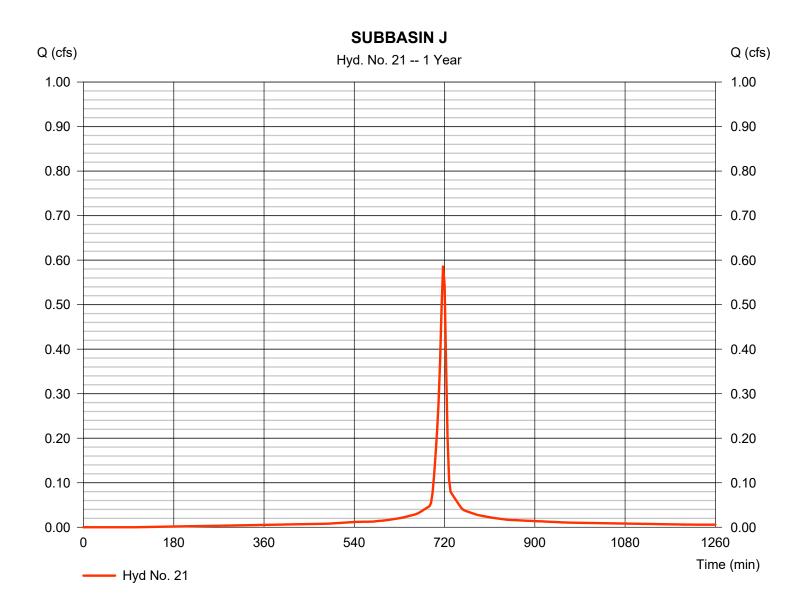
Monday, 07 / 9 / 2018

Hyd. No. 21

SUBBASIN J

Hydrograph type = SCS Runoff Peak discharge = 0.587 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 1.481 cuft Curve number Drainage area = 0.210 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.210 x 98)] / 0.210



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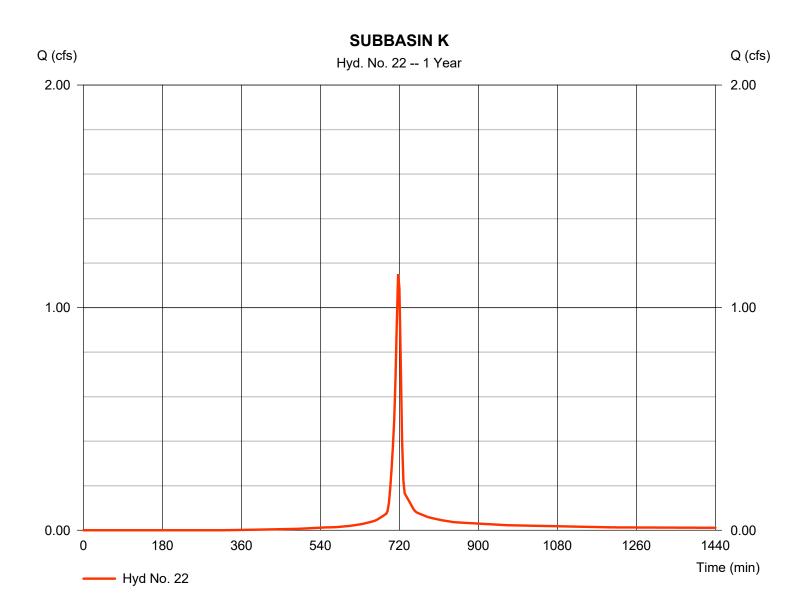
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Hyd. No. 22

SUBBASIN K

Hydrograph type = SCS Runoff Peak discharge = 1.150 cfsStorm frequency Time to peak = 717 min = 1 yrsTime interval = 3 min Hyd. volume = 2.655 cuftDrainage area = 0.490 acCurve number = 93* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.30 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.380 \times 98) + (0.110 \times 74)] / 0.490$



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

lyd. lo.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	4.778	3	729	17,514				Pre-Basin A	
2	SCS Runoff	1.226	3	717	2,773				Pre-Offsite	
3	Combine	5.219	3	726	20,288	1, 2			Total Predevelopment	
5	SCS Runoff	10.98	3	717	24,828				Post- Pond	
6	SCS Runoff	0.172	3	717	390				Post- Offsite	
7	Reservoir	4.642	3	726	24,828	5	138.15	6,438	Pond Discharge	
9	Combine	4.709	3	726	25,218	6, 7,			Total Post Discharge	
12	SCS Runoff	1.083	3	720	2,486				SUBBASIN A	
13	SCS Runoff	0.231	3	717	588				SUBBASIN B	
14	SCS Runoff	0.396	3	717	1,009				SUBBASIN C	
15	SCS Runoff	0.714	3	717	1,683				SUBBASIN D	
16	SCS Runoff	1.558	3	720	3,575				SUBBASIN E	
17	SCS Runoff	0.733	3	717	1,665				SUBBASIN F	
18	SCS Runoff	0.495	3	717	1,261				SUBBASIN G	
19	SCS Runoff	1.517	3	717	3,687				SUBBASIN H	
20	SCS Runoff	0.330	3	717	840				SUBBASIN I	
21	SCS Runoff	0.693	3	717	1,765				SUBBASIN J	
22	SCS Runoff	1.408	3	717	3,282				SUBBASIN K	
818660STORM.gpw					Return	Period: 2 Y	ear	Monday, 0	Monday, 07 / 9 / 2018	

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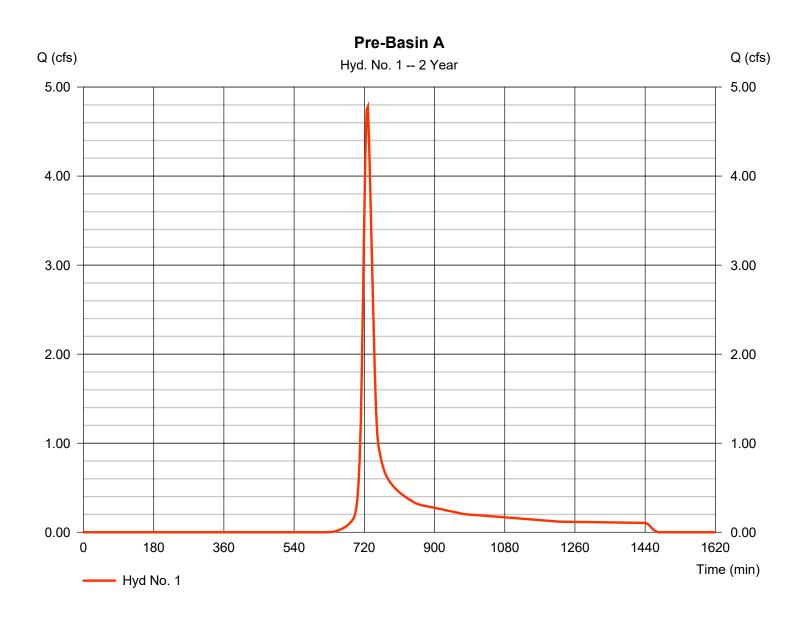
Monday, 07 / 9 / 2018

Hyd. No. 1

Pre-Basin A

Hydrograph type = SCS Runoff Peak discharge = 4.778 cfsStorm frequency = 2 yrsTime to peak = 729 min Time interval = 3 min Hyd. volume = 17.514 cuft Drainage area = 5.080 acCurve number = 79* Basin Slope = 0.0 % Hydraulic length = 0 ft= 21.40 min Tc method = TR55 Time of conc. (Tc) Total precip. Distribution = Type II = 2.70 inStorm duration = 24 hrs = 484 Shape factor

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (1.160 \times 98) + (1.170 \times 74) + (1.230 \times 70) + (0.670 \times 80) + (0.590 \times 77)] / 5.080$



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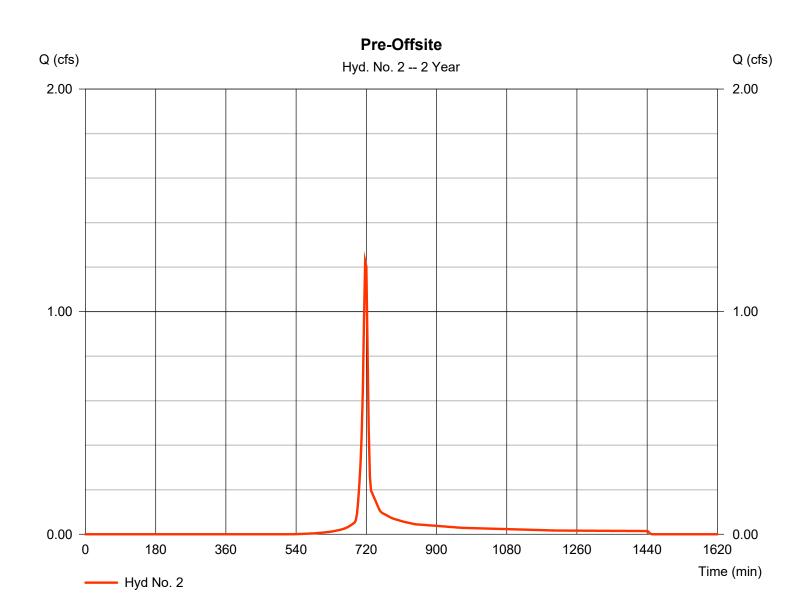
Monday, 07 / 9 / 2018

Hyd. No. 2

Pre-Offsite

Hydrograph type = 1.226 cfs= SCS Runoff Peak discharge Storm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2,773 cuftCurve number Drainage area = 0.640 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.70 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.370 x 74) + (0.270 x 98)] / 0.640



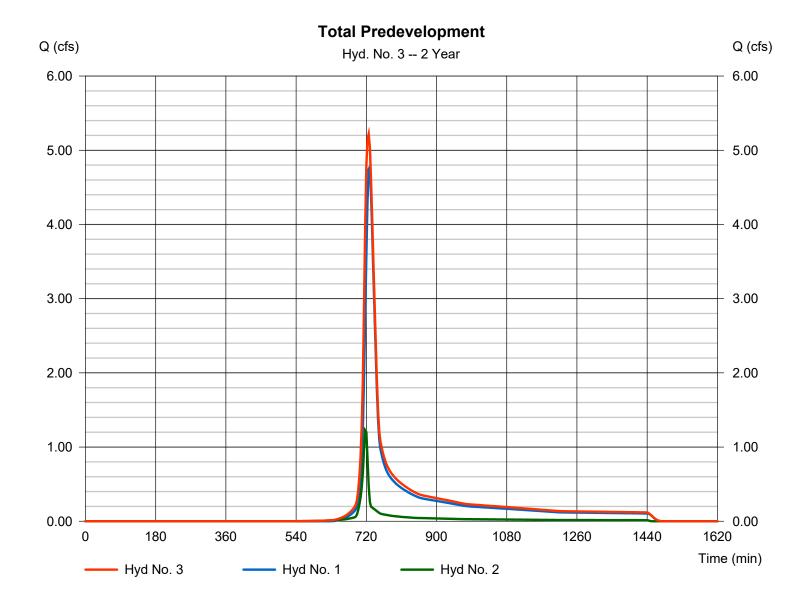
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Monday, 07 / 9 / 2018

Hyd. No. 3

Total Predevelopment

Hydrograph type = Combine Peak discharge = 5.219 cfsStorm frequency = 2 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 20,288 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 5.720 ac



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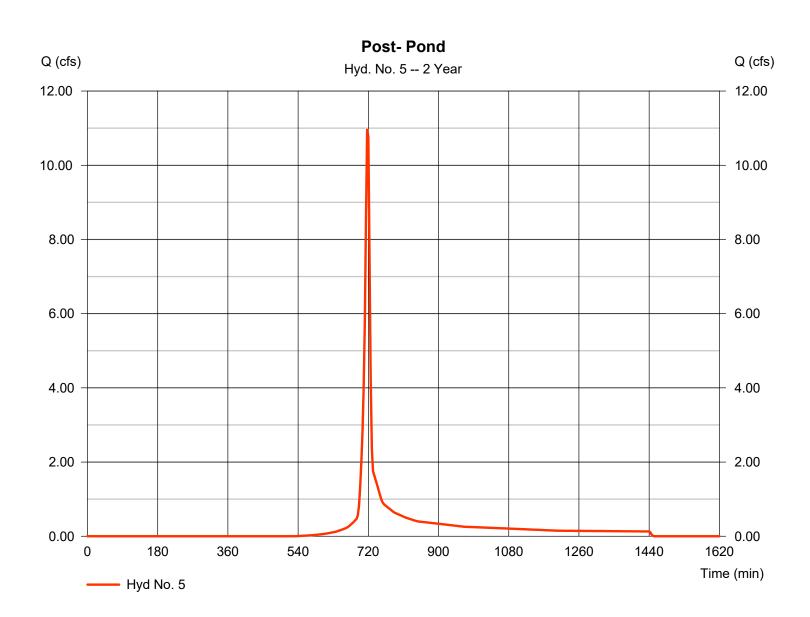
Monday, 07 / 9 / 2018

Hyd. No. 5

Post-Pond

Hydrograph type = SCS Runoff Peak discharge = 10.98 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 24.828 cuft Curve number Drainage area = 5.730 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.70 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (2.350 \times 98) + (2.020 \times 74) + (1.100 \times 80)] / 5.730$



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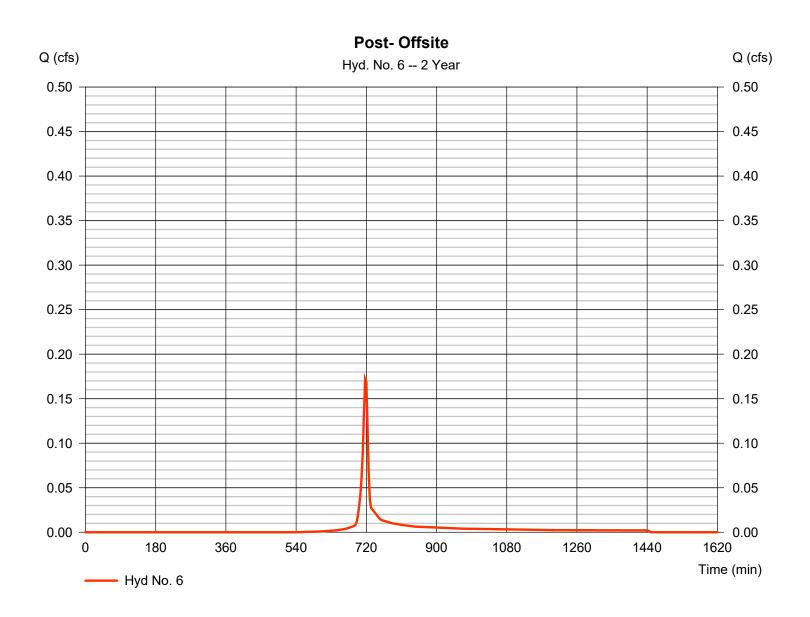
Monday, 07 / 9 / 2018

Hyd. No. 6

Post- Offsite

Hydrograph type = SCS Runoff Peak discharge = 0.172 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 390 cuft Curve number Drainage area = 0.090 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.030 \times 61) + (0.050 \times 98) + (0.010 \times 80)] / 0.090$



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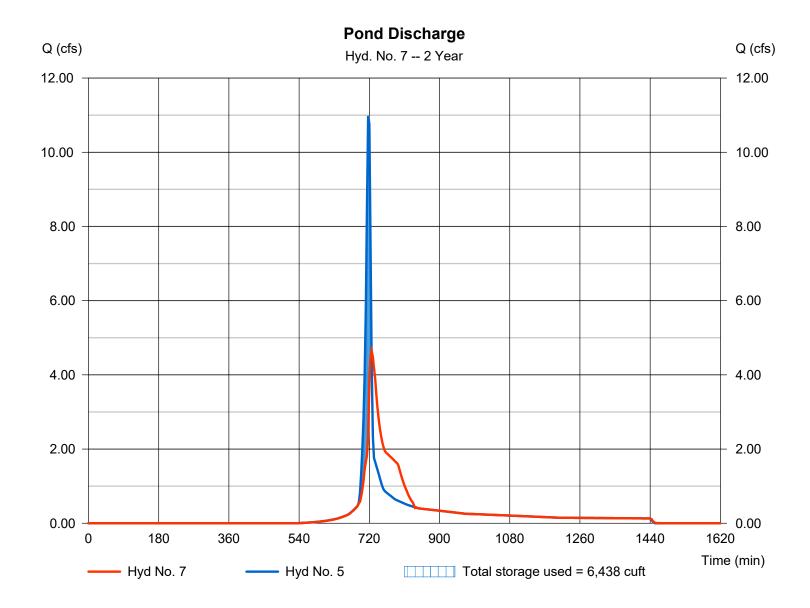
Monday, 07 / 9 / 2018

Hyd. No. 7

Pond Discharge

Hydrograph type = Reservoir Peak discharge = 4.642 cfsStorm frequency = 2 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 24,828 cuft = 5 - Post- Pond Max. Elevation = 138.15 ft Inflow hyd. No. Reservoir name = South Detention Max. Storage = 6,438 cuft

Storage Indication method used.



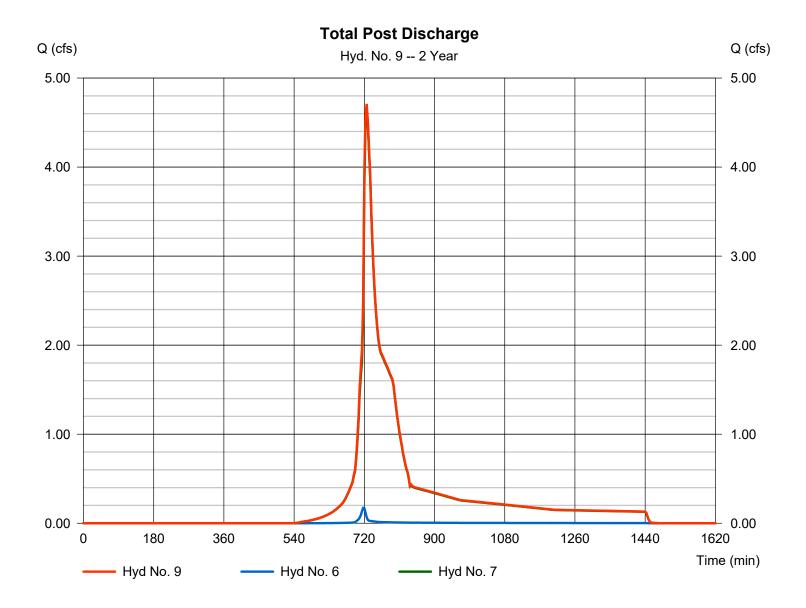
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Hyd. No. 9

Total Post Discharge

Hydrograph type = Combine = 4.709 cfsPeak discharge Storm frequency = 2 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 25,218 cuft Inflow hyds. = 6, 7 Contrib. drain. area = 0.090 ac



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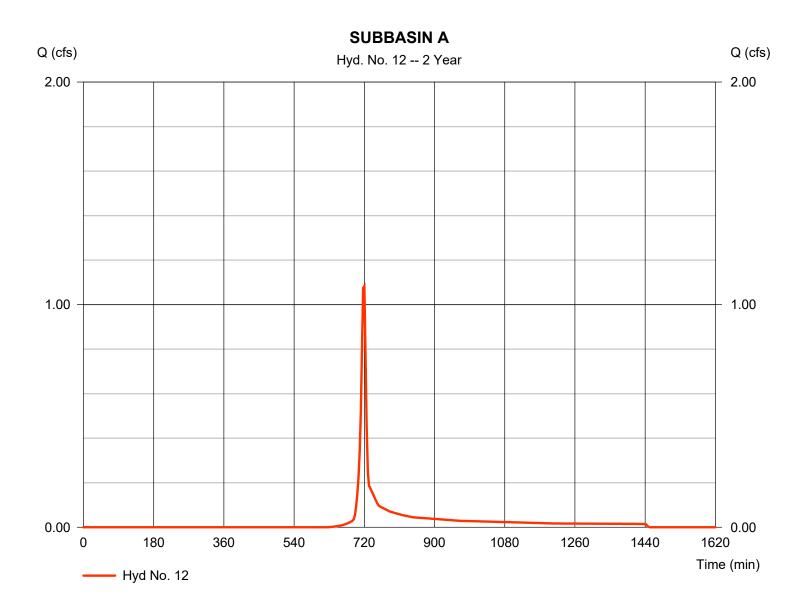
Monday, 07 / 9 / 2018

Hyd. No. 12

SUBBASIN A

Hydrograph type = SCS Runoff Peak discharge = 1.083 cfsStorm frequency = 2 yrsTime to peak = 720 min Time interval = 3 min Hyd. volume = 2.486 cuft Curve number = 79* Drainage area = 0.750 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.230 \times 98) + (0.240 \times 61) + (0.280 \times 80)] / 0.750$



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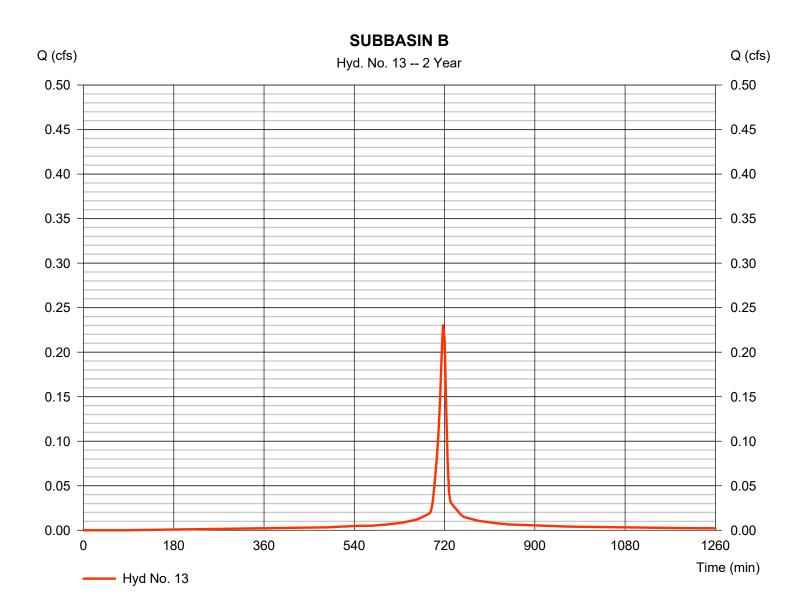
Monday, 07 / 9 / 2018

Hyd. No. 13

SUBBASIN B

Hydrograph type = SCS Runoff Peak discharge = 0.231 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 588 cuft Curve number Drainage area = 0.070 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.070 x 98)] / 0.070



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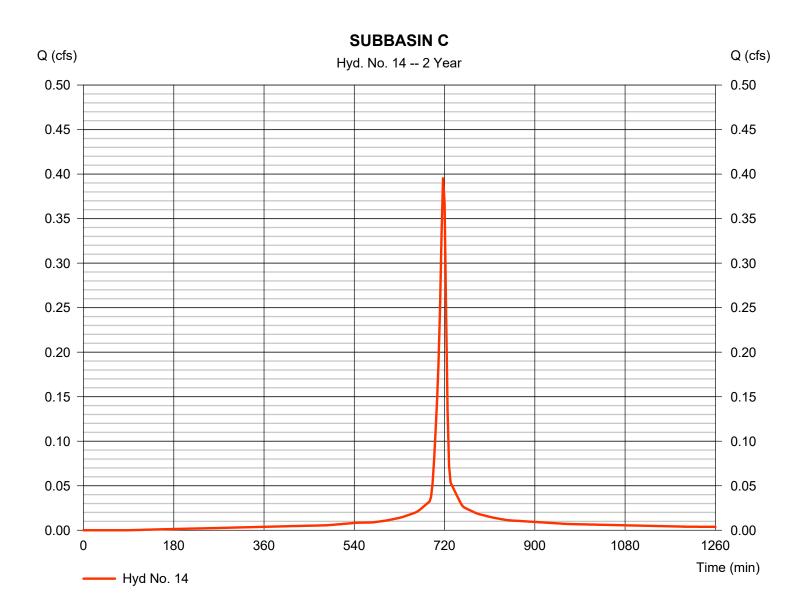
Monday, 07 / 9 / 2018

Hyd. No. 14

SUBBASIN C

Hydrograph type = SCS Runoff Peak discharge = 0.396 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.009 cuftCurve number Drainage area = 0.120 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.120 x 98)] / 0.120



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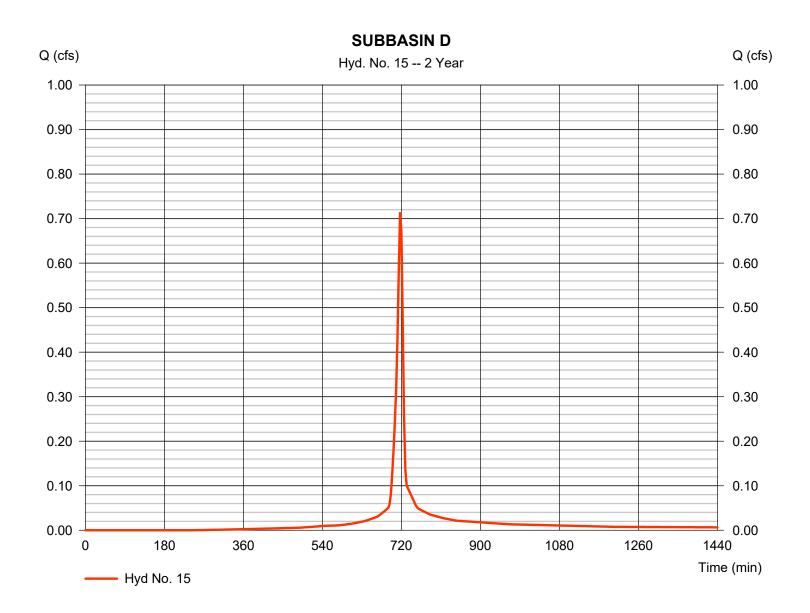
Monday, 07 / 9 / 2018

Hyd. No. 15

SUBBASIN D

Hydrograph type = SCS Runoff Peak discharge = 0.714 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1,683 cuft Drainage area = 0.240 acCurve number = 94* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.050 \times 80)] / 0.240$



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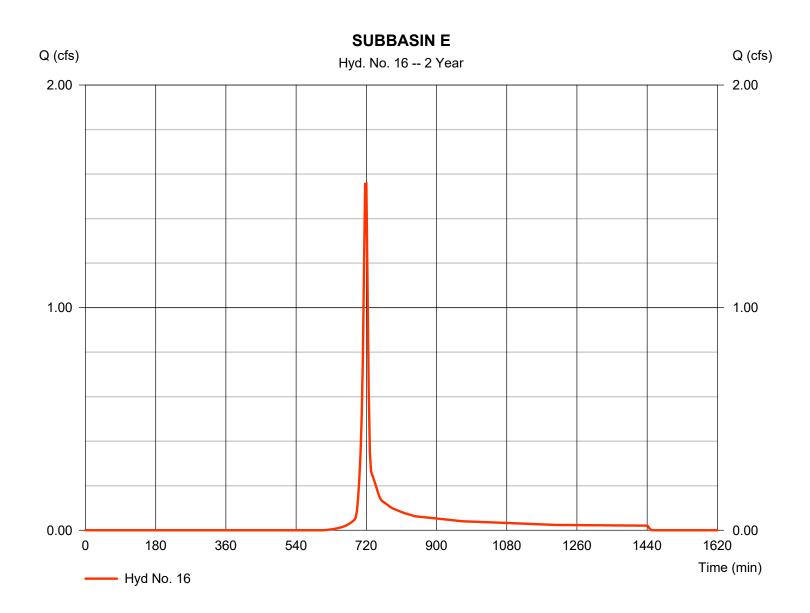
Monday, 07 / 9 / 2018

Hyd. No. 16

SUBBASIN E

Hydrograph type = SCS Runoff Peak discharge = 1.558 cfsStorm frequency = 2 yrsTime to peak = 720 min Time interval = 3 min Hyd. volume = 3,575 cuftDrainage area = 1.020 acCurve number = 80* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.020 x 98) + (1.000 x 80)] / 1.020



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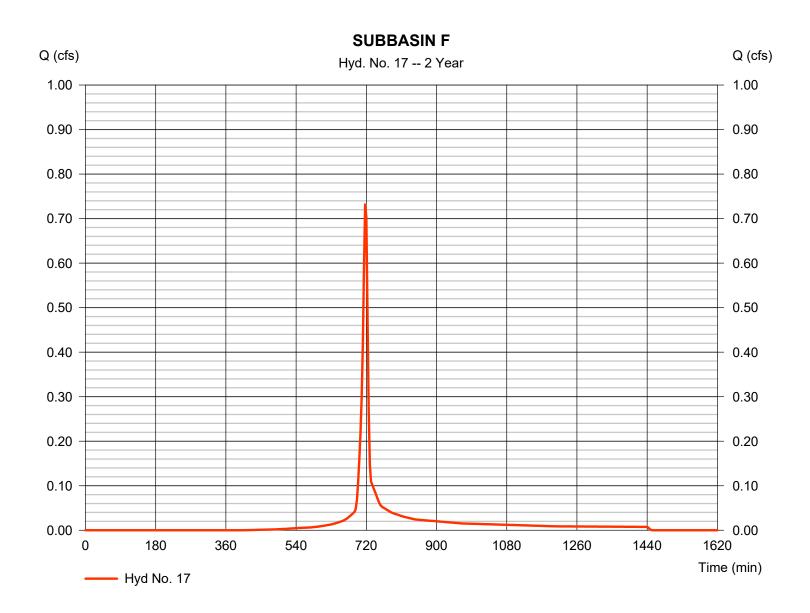
Monday, 07 / 9 / 2018

Hyd. No. 17

SUBBASIN F

Hydrograph type = SCS Runoff Peak discharge = 0.733 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.665 cuft Curve number Drainage area = 0.300 ac= 89* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.110 \times 74)] / 0.300$



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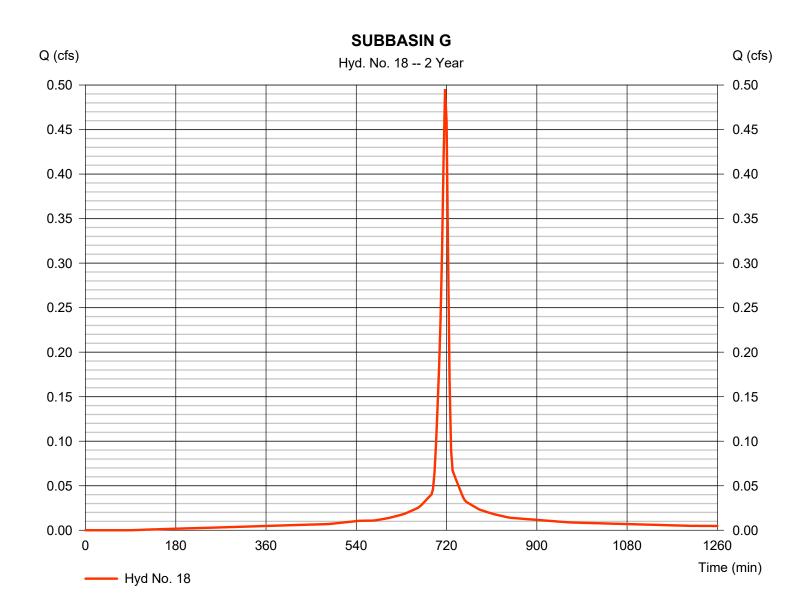
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Hyd. No. 18

SUBBASIN G

Hydrograph type = SCS Runoff Peak discharge = 0.495 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.261 cuft Curve number Drainage area = 0.150 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.150 x 98)] / 0.150



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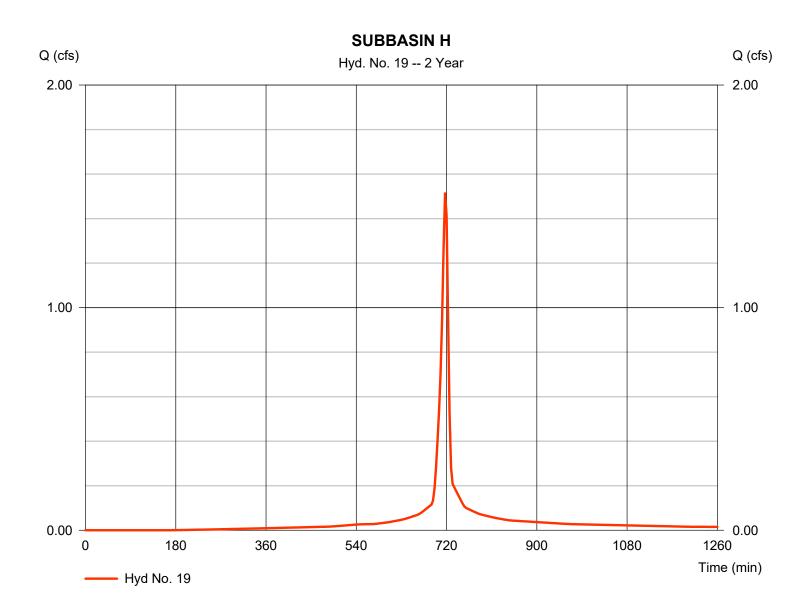
Monday, 07 / 9 / 2018

Hyd. No. 19

SUBBASIN H

Hydrograph type = SCS Runoff Peak discharge = 1.517 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 3.687 cuft Drainage area = 0.480 acCurve number = 96* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = 6.00 min = User Time of conc. (Tc) Total precip. = 2.70 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.430 \times 98) + (0.050 \times 74)] / 0.480$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

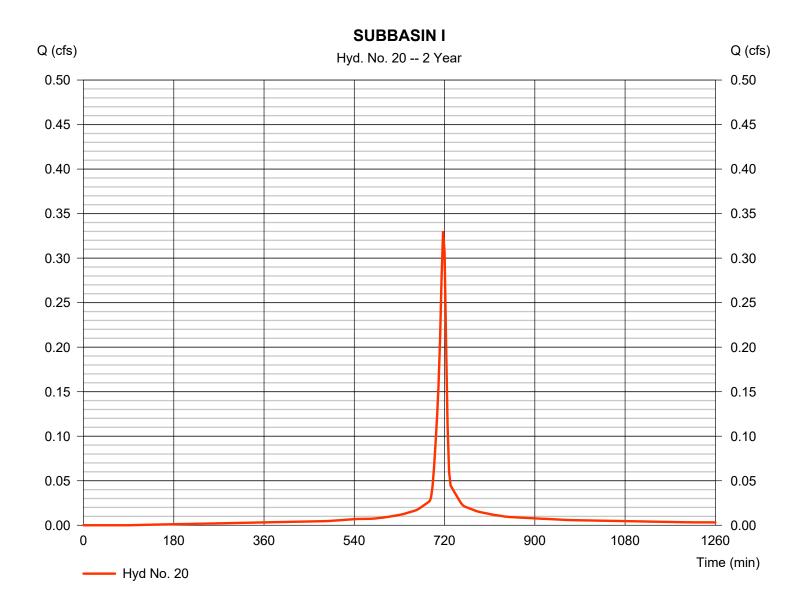
Monday, 07 / 9 / 2018

Hyd. No. 20

SUBBASIN I

Hydrograph type = SCS Runoff Peak discharge = 0.330 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 840 cuft Curve number Drainage area = 0.100 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.100 x 98)] / 0.100



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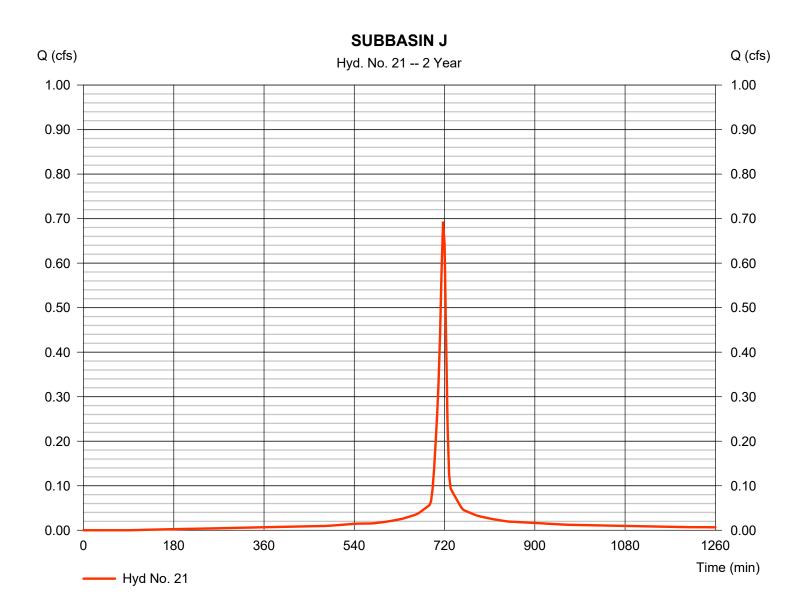
Monday, 07 / 9 / 2018

Hyd. No. 21

SUBBASIN J

Hydrograph type = SCS Runoff Peak discharge = 0.693 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1,765 cuftCurve number Drainage area = 0.210 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 2.70 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.210 x 98)] / 0.210



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

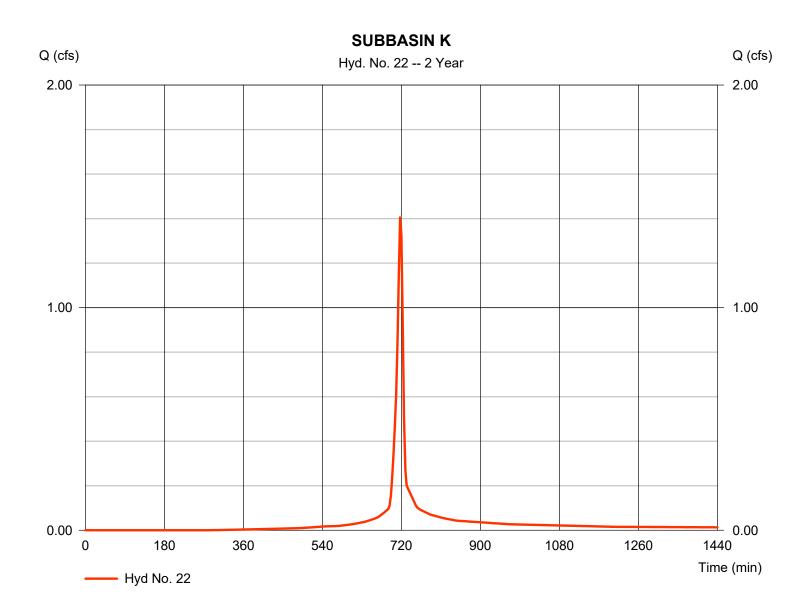
Monday, 07 / 9 / 2018

Hyd. No. 22

SUBBASIN K

Hydrograph type = SCS Runoff Peak discharge = 1.408 cfsStorm frequency = 2 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 3.282 cuft Drainage area = 0.490 acCurve number = 93* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 2.70 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.380 \times 98) + (0.110 \times 74)] / 0.490$



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	9.980	3	726	35,302				Pre-Basin A	
2	SCS Runoff	2.277	3	717	5,164				Pre-Offsite	
3	Combine	10.82	3	726	40,467	1, 2			Total Predevelopment	
5	SCS Runoff	20.39	3	717	46,236				Post- Pond	
6	SCS Runoff	0.320	3	717	726				Post- Offsite	
7	Reservoir	7.874	3	726	46,236	5	138.97	12,912	Pond Discharge	
9	Combine	7.993	3	726	46,962	6, 7,			Total Post Discharge	
12	SCS Runoff	2.218	3	717	5,011				SUBBASIN A	
13	SCS Runoff	0.346	3	717	897				SUBBASIN B	
14	SCS Runoff	0.592	3	717	1,538				SUBBASIN C	
15	SCS Runoff	1.120	3	717	2,715				SUBBASIN D	
16	SCS Runoff	3.138	3	717	7,087				SUBBASIN E	
17	SCS Runoff	1.245	3	717	2,882				SUBBASIN F	
18	SCS Runoff	0.741	3	717	1,922				SUBBASIN G	
19	SCS Runoff	2.316	3	717	5,783				SUBBASIN H	
20	SCS Runoff	0.494	3	717	1,281				SUBBASIN I	
21	SCS Runoff	1.037	3	717	2,691				SUBBASIN J	
22	SCS Runoff	2.241	3	717	5,369				SUBBASIN K	
181	818660STORM.gpw					Return Period: 10 Year			Monday, 07 / 9 / 2018	

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

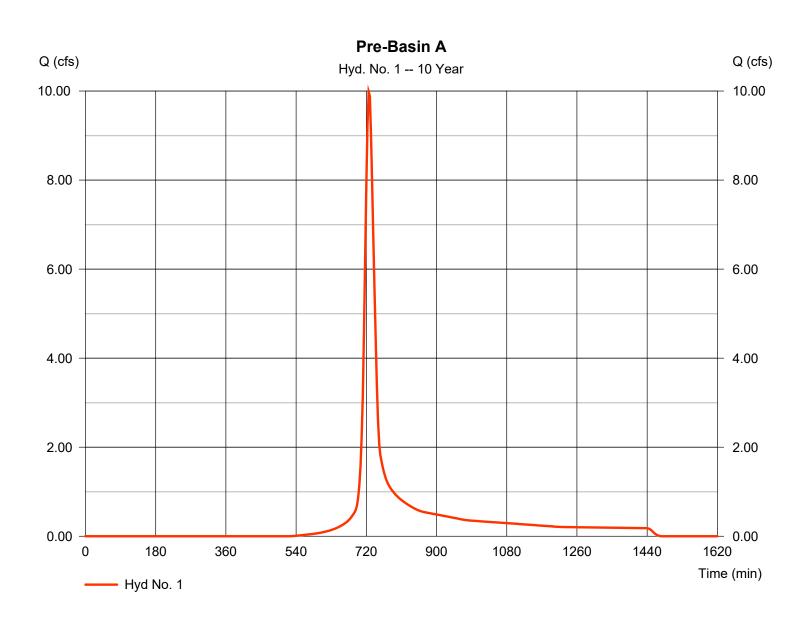
Monday, 07 / 9 / 2018

Hyd. No. 1

Pre-Basin A

Hydrograph type = SCS Runoff Peak discharge = 9.980 cfsStorm frequency = 10 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 35.302 cuft Curve number Drainage area = 5.080 ac= 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.40 min = TR55 Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (1.160 \times 98) + (1.170 \times 74) + (1.230 \times 70) + (0.670 \times 80) + (0.590 \times 77)] / 5.080$



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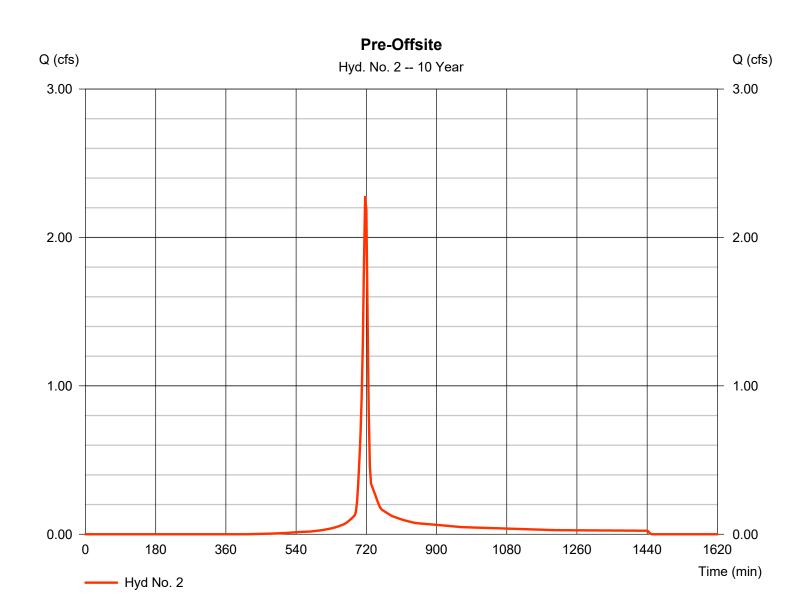
Monday, 07 / 9 / 2018

Hyd. No. 2

Pre-Offsite

Hydrograph type = SCS Runoff Peak discharge = 2.277 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 5,164 cuftDrainage area = 0.640 acCurve number = 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 6.00 \, \text{min}$ = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.370 x 74) + (0.270 x 98)] / 0.640



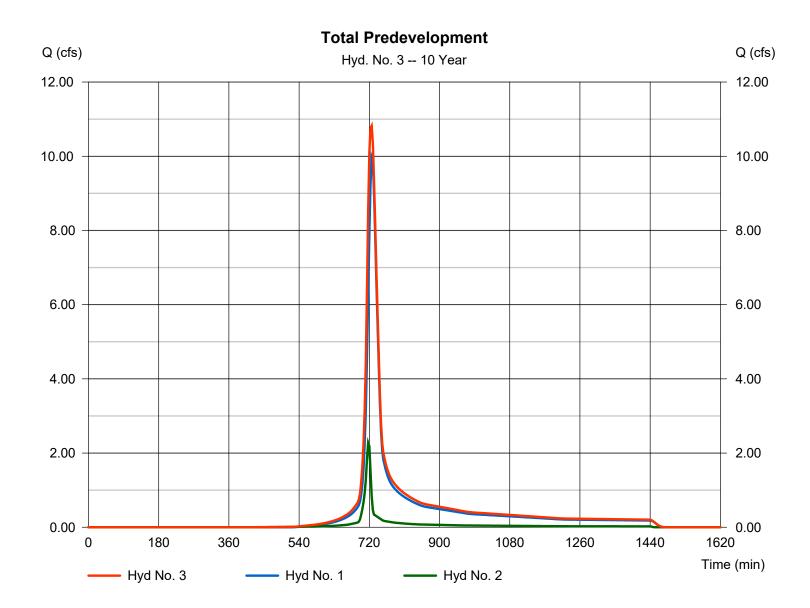
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Hyd. No. 3

Total Predevelopment

Hydrograph type = Combine Peak discharge = 10.82 cfsStorm frequency = 10 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 40,467 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 5.720 ac



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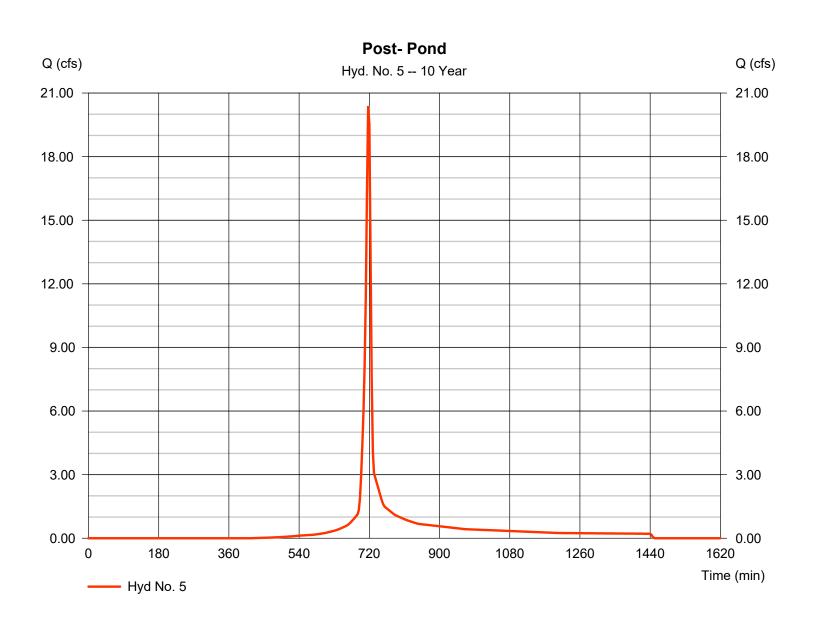
Monday, 07 / 9 / 2018

Hyd. No. 5

Post-Pond

Hydrograph type = SCS Runoff Peak discharge = 20.39 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 46.236 cuft Curve number Drainage area = 5.730 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.260 x 61) + (2.350 x 98) + (2.020 x 74) + (1.100 x 80)] / 5.730



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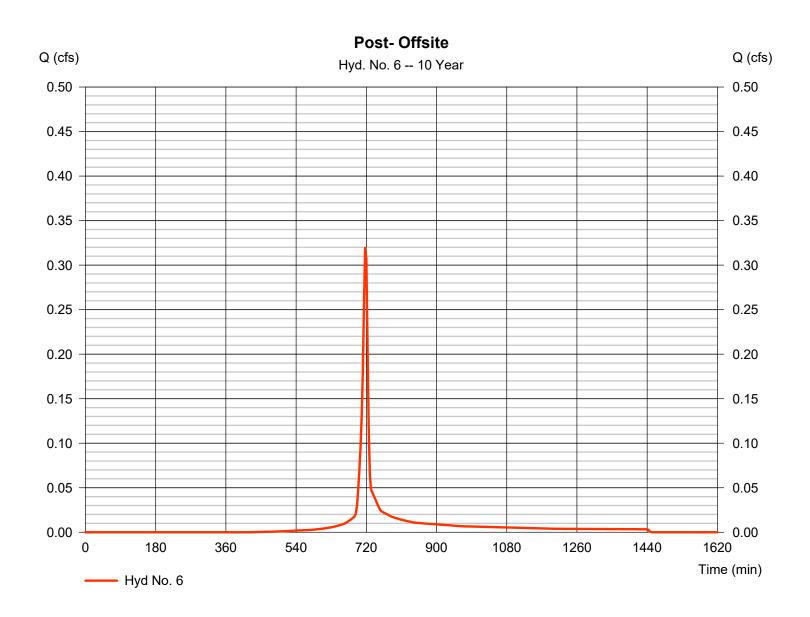
Monday, 07 / 9 / 2018

Hyd. No. 6

Post- Offsite

Hydrograph type = SCS Runoff Peak discharge = 0.320 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 726 cuft Curve number Drainage area = 0.090 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 484 = 24 hrs

^{*} Composite (Area/CN) = $[(0.030 \times 61) + (0.050 \times 98) + (0.010 \times 80)] / 0.090$



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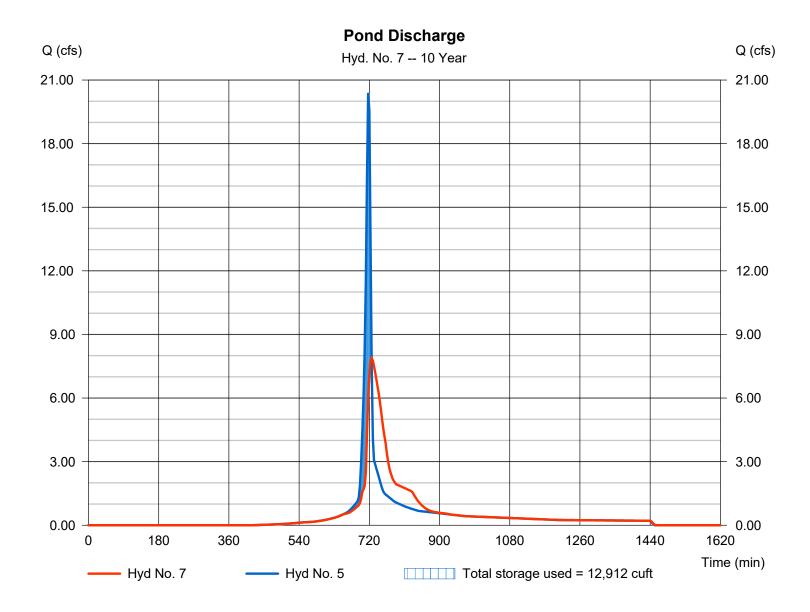
Monday, 07 / 9 / 2018

Hyd. No. 7

Pond Discharge

Hydrograph type = Reservoir Peak discharge = 7.874 cfsStorm frequency = 10 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 46,236 cuft = 5 - Post- Pond Max. Elevation Inflow hyd. No. = 138.97 ftReservoir name = South Detention Max. Storage = 12,912 cuft

Storage Indication method used.



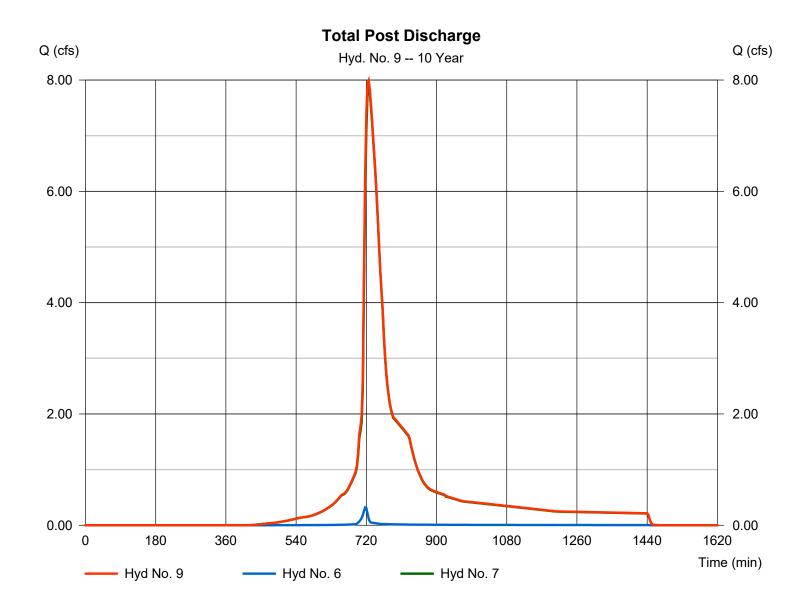
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Monday, 07 / 9 / 2018

Hyd. No. 9

Total Post Discharge

Hydrograph type = Combine Peak discharge = 7.993 cfsStorm frequency = 10 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 46,962 cuft Inflow hyds. = 6, 7 Contrib. drain. area = 0.090 ac



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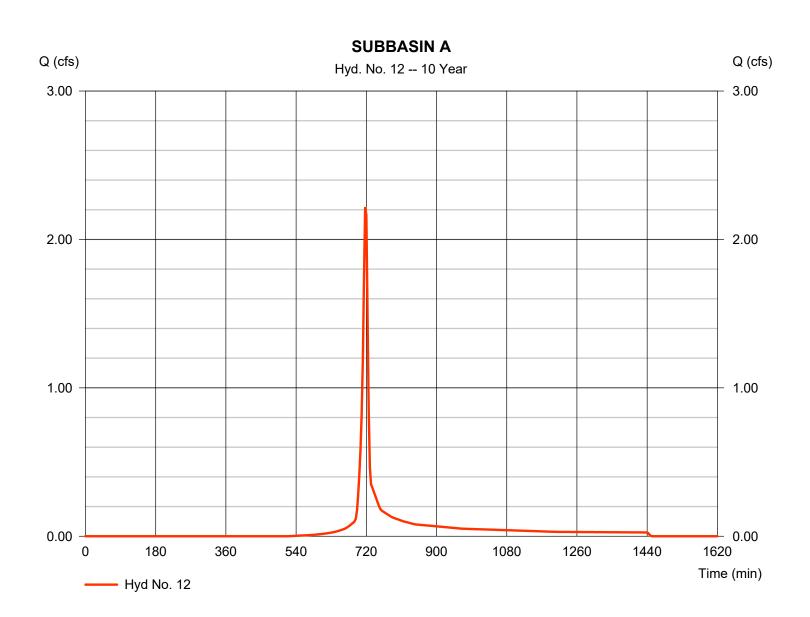
Monday, 07 / 9 / 2018

Hyd. No. 12

SUBBASIN A

Hydrograph type = SCS Runoff Peak discharge = 2.218 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 5.011 cuftCurve number = 79* Drainage area = 0.750 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.230 \times 98) + (0.240 \times 61) + (0.280 \times 80)] / 0.750$



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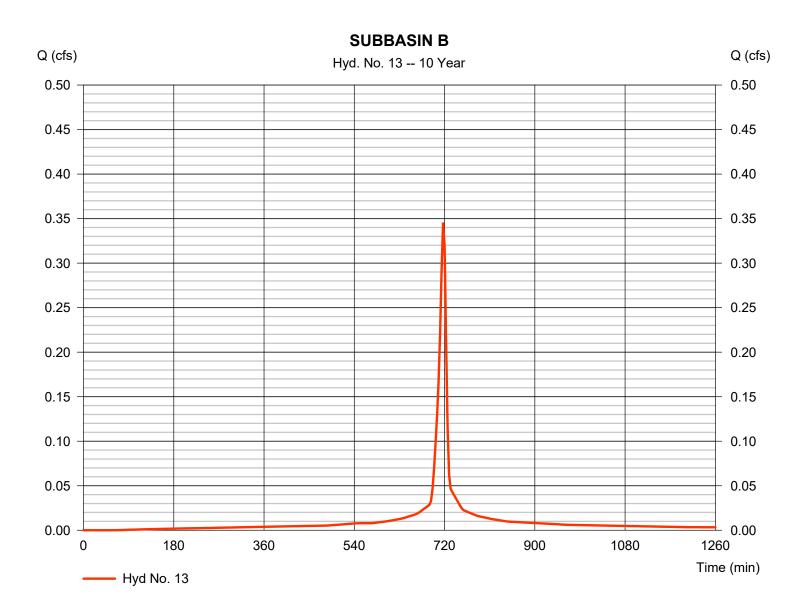
Monday, 07 / 9 / 2018

Hyd. No. 13

SUBBASIN B

Hydrograph type = SCS Runoff Peak discharge = 0.346 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 897 cuft Curve number Drainage area = 0.070 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.070 x 98)] / 0.070



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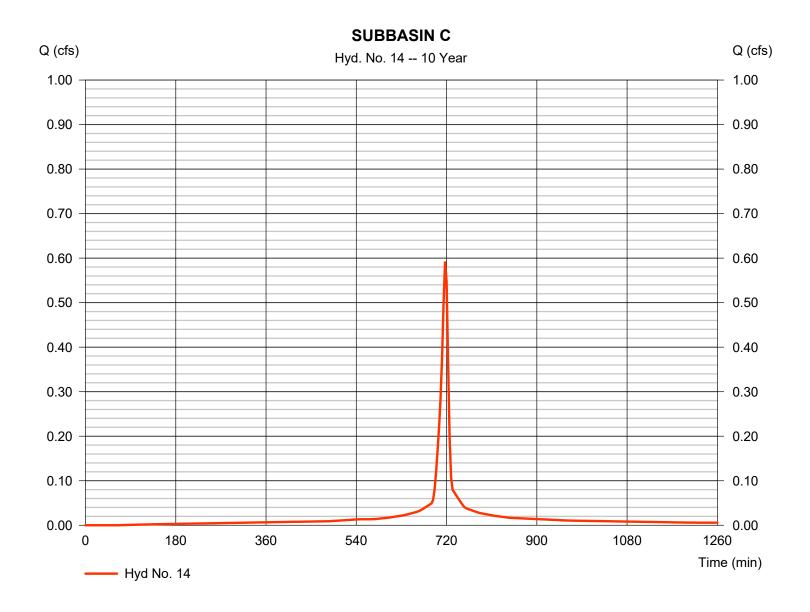
Monday, 07 / 9 / 2018

Hyd. No. 14

SUBBASIN C

Hydrograph type = SCS Runoff Peak discharge = 0.592 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.538 cuft Curve number Drainage area = 0.120 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.120 x 98)] / 0.120



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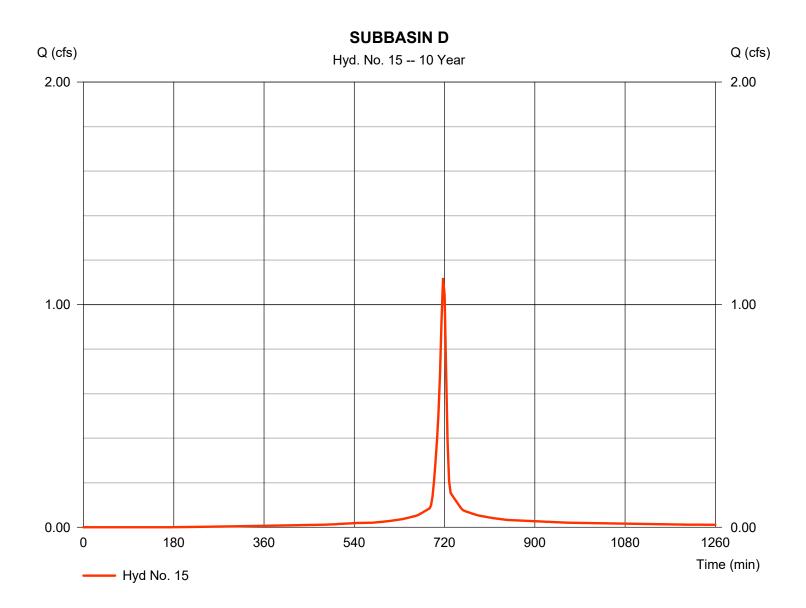
Monday, 07 / 9 / 2018

Hyd. No. 15

SUBBASIN D

Hydrograph type = SCS Runoff Peak discharge = 1.120 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2,715 cuftDrainage area = 0.240 acCurve number = 94* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.050 \times 80)] / 0.240$



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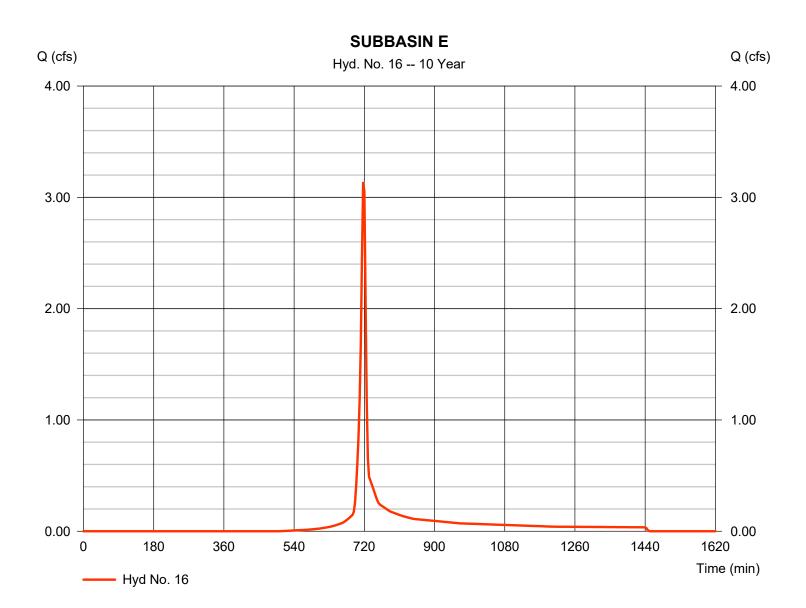
Monday, 07 / 9 / 2018

Hyd. No. 16

SUBBASIN E

Hydrograph type = SCS Runoff Peak discharge = 3.138 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 7.087 cuftCurve number Drainage area = 1.020 ac= 80* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.020 x 98) + (1.000 x 80)] / 1.020



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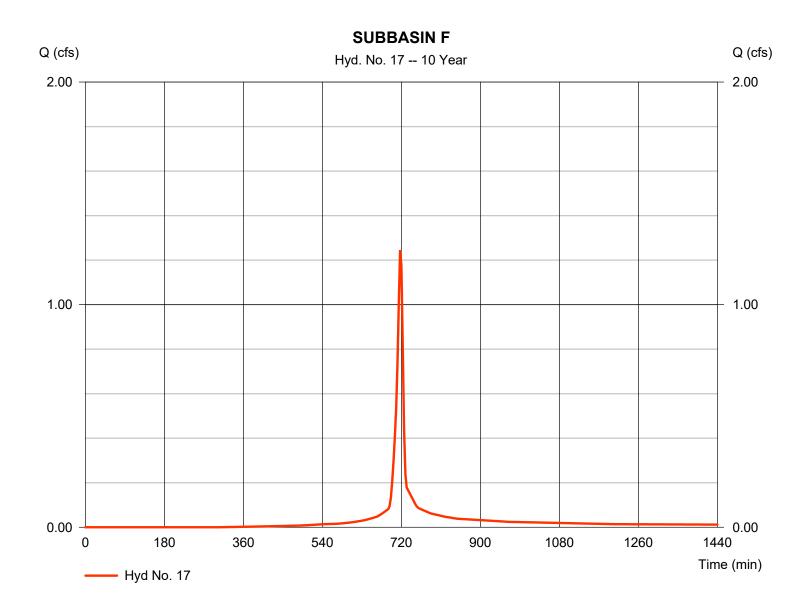
Monday, 07 / 9 / 2018

Hyd. No. 17

SUBBASIN F

Hydrograph type = SCS Runoff Peak discharge = 1.245 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2.882 cuft Drainage area = 0.300 acCurve number = 89* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.110 \times 74)] / 0.300$



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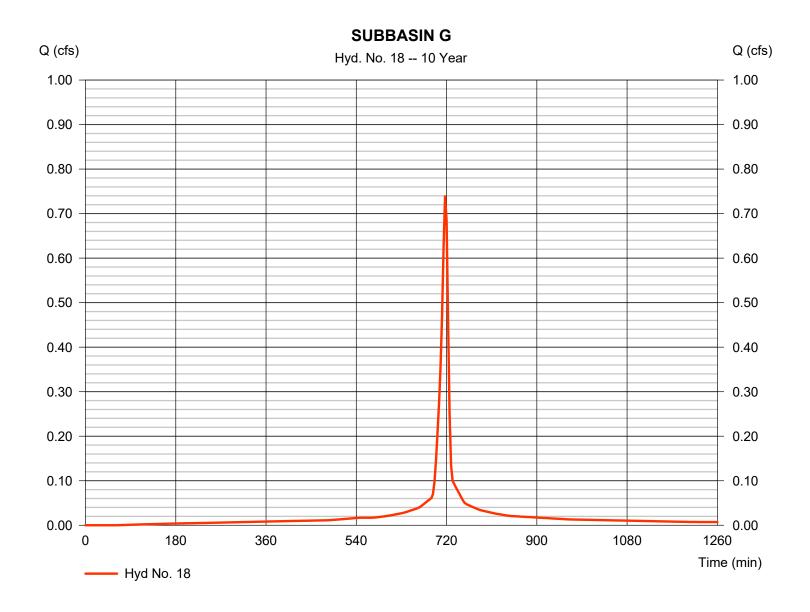
Monday, 07 / 9 / 2018

Hyd. No. 18

SUBBASIN G

Hydrograph type = SCS Runoff Peak discharge = 0.741 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1,922 cuft Curve number Drainage area = 0.150 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.150 x 98)] / 0.150



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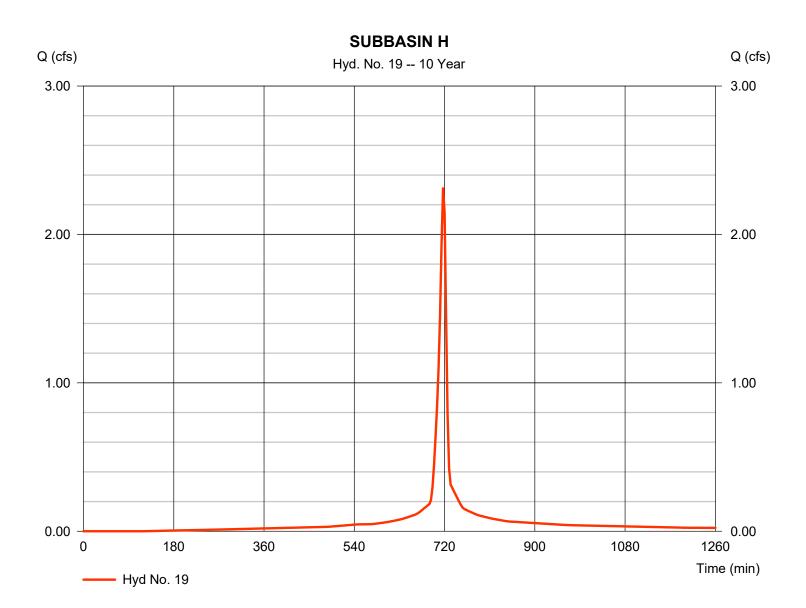
Monday, 07 / 9 / 2018

Hyd. No. 19

SUBBASIN H

Hydrograph type = SCS Runoff Peak discharge = 2.316 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 5,783 cuftCurve number Drainage area = 0.480 ac= 96* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 6.00 \, \text{min}$ = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.430 \times 98) + (0.050 \times 74)] / 0.480$



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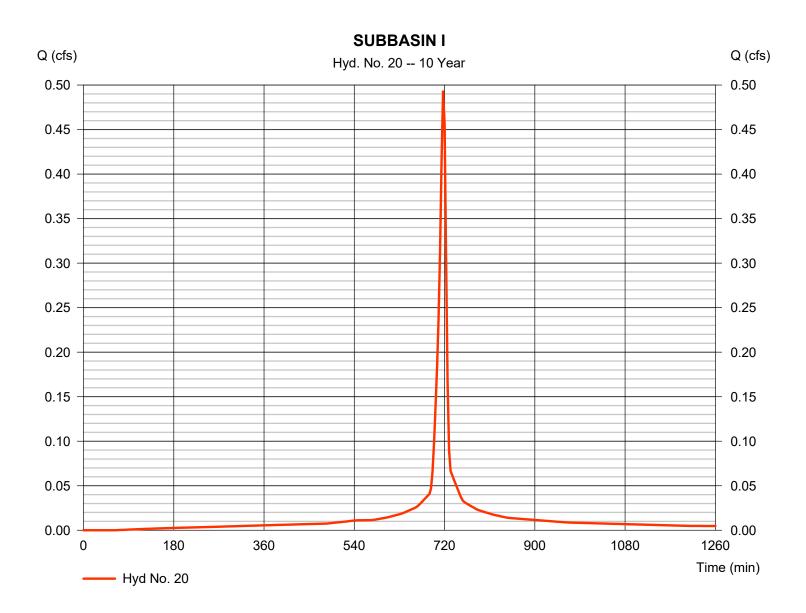
Monday, 07 / 9 / 2018

Hyd. No. 20

SUBBASIN I

Hydrograph type = SCS Runoff Peak discharge = 0.494 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.281 cuft Curve number Drainage area = 0.100 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.100 x 98)] / 0.100



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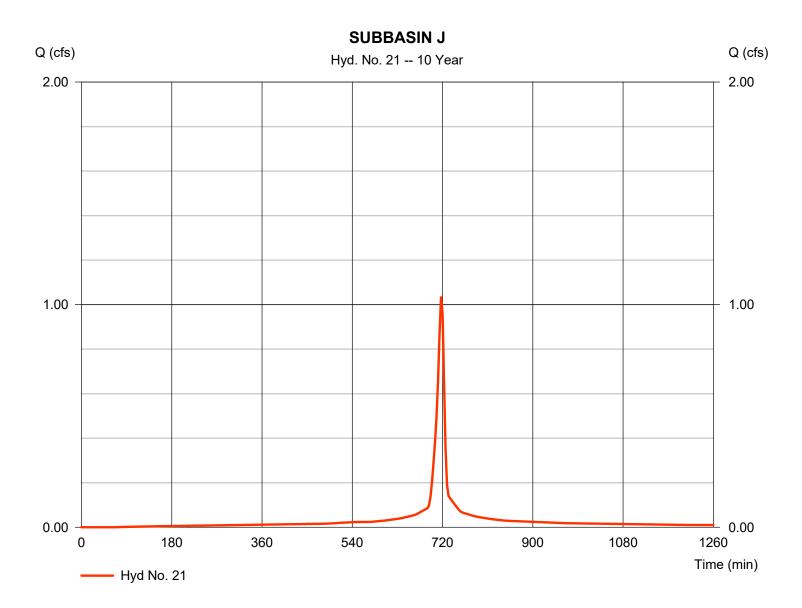
Monday, 07 / 9 / 2018

Hyd. No. 21

SUBBASIN J

Hydrograph type = SCS Runoff Peak discharge = 1.037 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2.691 cuftCurve number = 98* Drainage area = 0.210 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.210 x 98)] / 0.210



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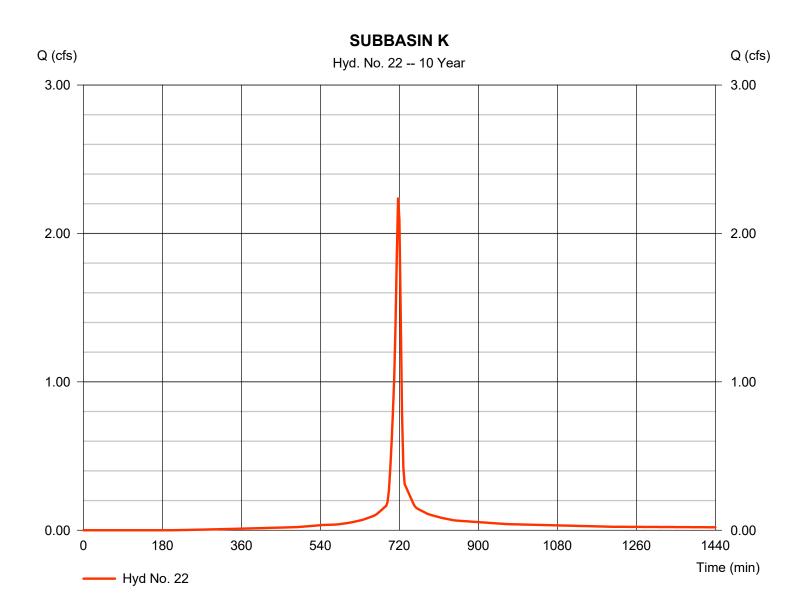
Monday, 07 / 9 / 2018

Hyd. No. 22

SUBBASIN K

Hydrograph type = SCS Runoff Peak discharge = 2.241 cfsStorm frequency = 10 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 5.369 cuftDrainage area = 0.490 acCurve number = 93* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 4.00 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.380 \times 98) + (0.110 \times 74)] / 0.490$



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	17.03	3	726	59,775				Pre-Basin A	
2	SCS Runoff	3.617	3	717	8,328				Pre-Offsite	
3	Combine	18.32	3	726	68,103	1, 2			Total Predevelopment	
5	SCS Runoff	32.38	3	717	74,559				Post- Pond	
6	SCS Runoff	0.509	3	717	1,171				Post- Offsite	
7	Reservoir	15.91	3	726	74,559	5	139.80	21,233	Pond Discharge	
9	Combine	16.09	3	726	75,730	6, 7,			Total Post Discharge	
12	SCS Runoff	3.742	3	717	8,486				SUBBASIN A	
13	SCS Runoff	0.486	3	717	1,277				SUBBASIN B	
14	SCS Runoff	0.833	3	717	2,190				SUBBASIN C	
15	SCS Runoff	1.613	3	717	4,003				SUBBASIN D	
16	SCS Runoff	5.227	3	717	11,880				SUBBASIN E	
17	SCS Runoff	1.875	3	717	4,440				SUBBASIN F	
18	SCS Runoff	1.041	3	717	2,737				SUBBASIN G	
19	SCS Runoff	3.289	3	717	8,379				SUBBASIN H	
20	SCS Runoff	0.694	3	717	1,825				SUBBASIN I	
21	SCS Runoff	1.458	3	717	3,832				SUBBASIN J	
22	SCS Runoff	3.254	3	717	7,984				SUBBASIN K	
181	818660STORM.gpw				Return Period: 100 Year			Monday, 0	Monday, 07 / 9 / 2018	

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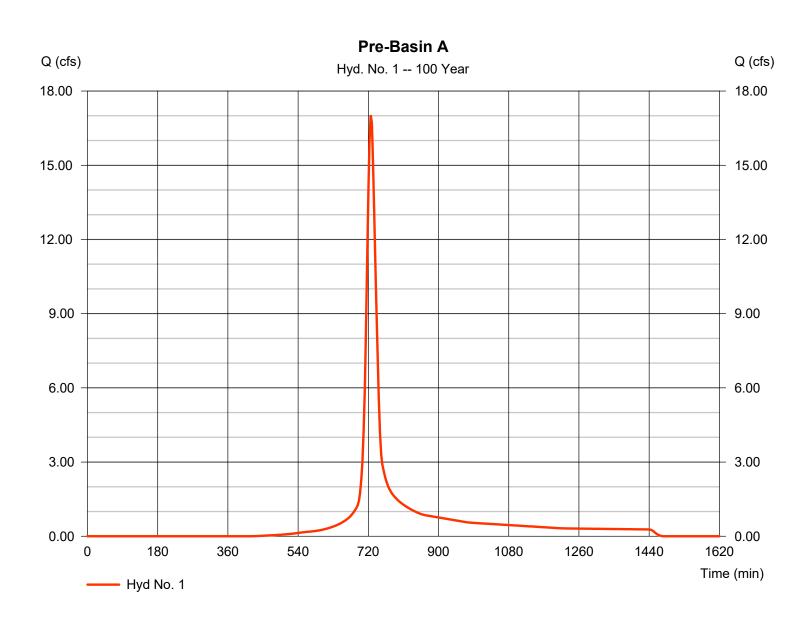
Monday, 07 / 9 / 2018

Hyd. No. 1

Pre-Basin A

Hydrograph type = SCS Runoff Peak discharge = 17.03 cfsStorm frequency = 100 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 59.775 cuftCurve number Drainage area = 5.080 ac= 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.40 min = TR55 Total precip. Distribution = Type II = 5.60 inShape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.260 \times 61) + (1.160 \times 98) + (1.170 \times 74) + (1.230 \times 70) + (0.670 \times 80) + (0.590 \times 77)] / 5.080$



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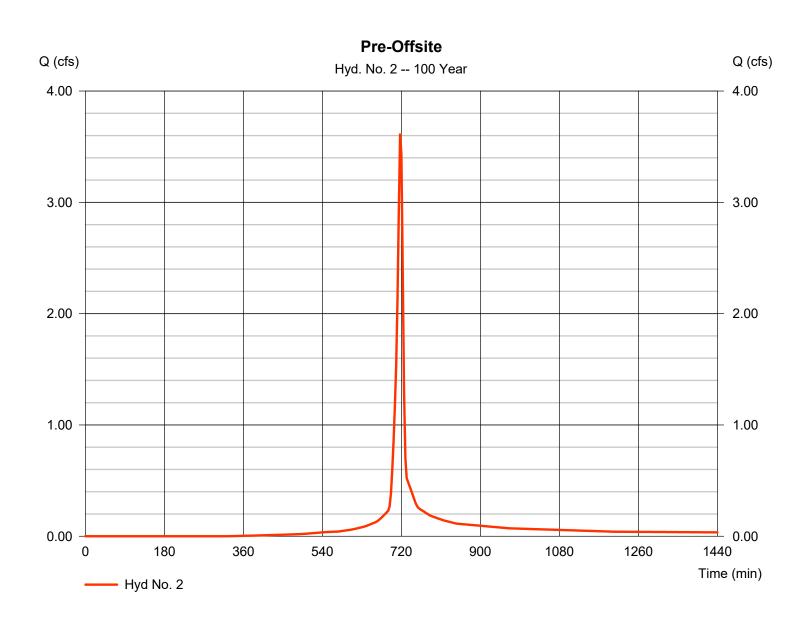
Monday, 07 / 9 / 2018

Hyd. No. 2

Pre-Offsite

Hydrograph type = SCS Runoff Peak discharge = 3.617 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 8.328 cuft Curve number Drainage area = 0.640 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.370 x 74) + (0.270 x 98)] / 0.640



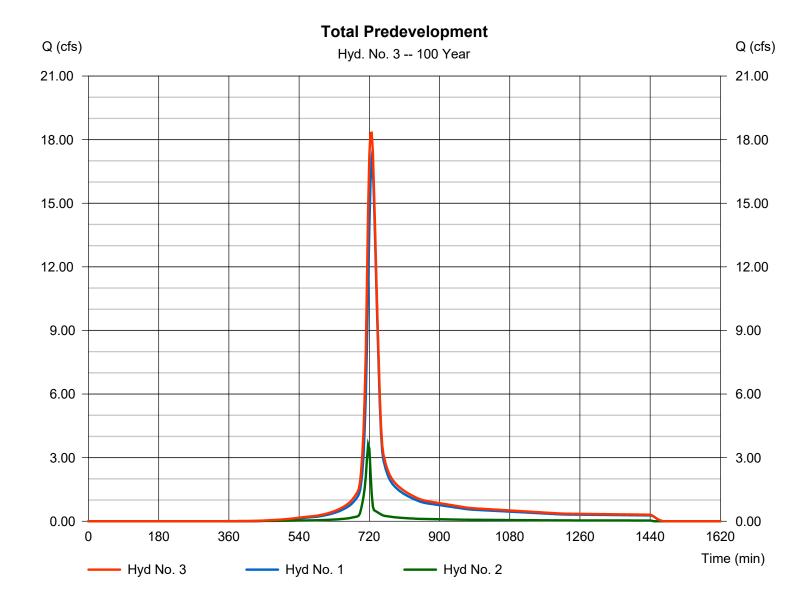
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Hyd. No. 3

Total Predevelopment

Hydrograph type = Combine Peak discharge = 18.32 cfsStorm frequency = 100 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 68,103 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 5.720 ac



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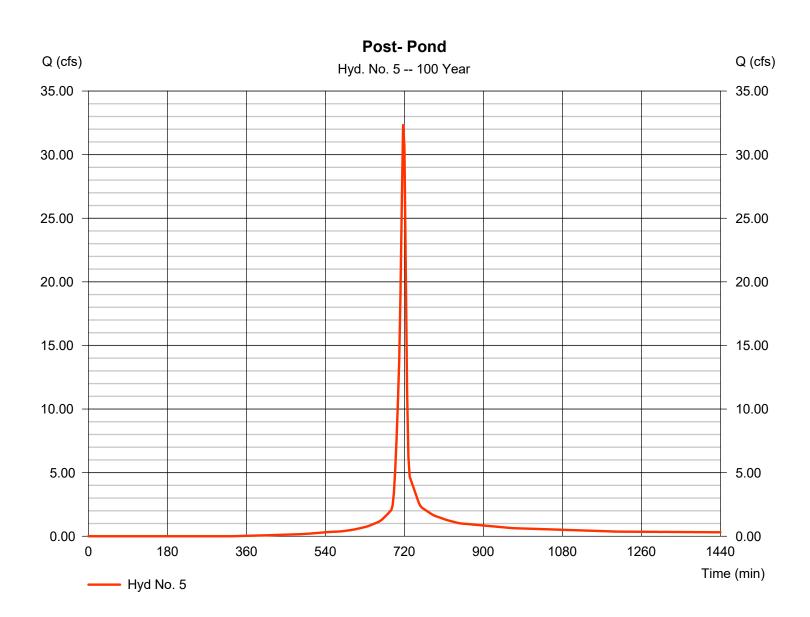
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Hyd. No. 5

Post-Pond

Hydrograph type = SCS Runoff Peak discharge = 32.38 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 74.559 cuftCurve number Drainage area = 5.730 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.260 x 61) + (2.350 x 98) + (2.020 x 74) + (1.100 x 80)] / 5.730



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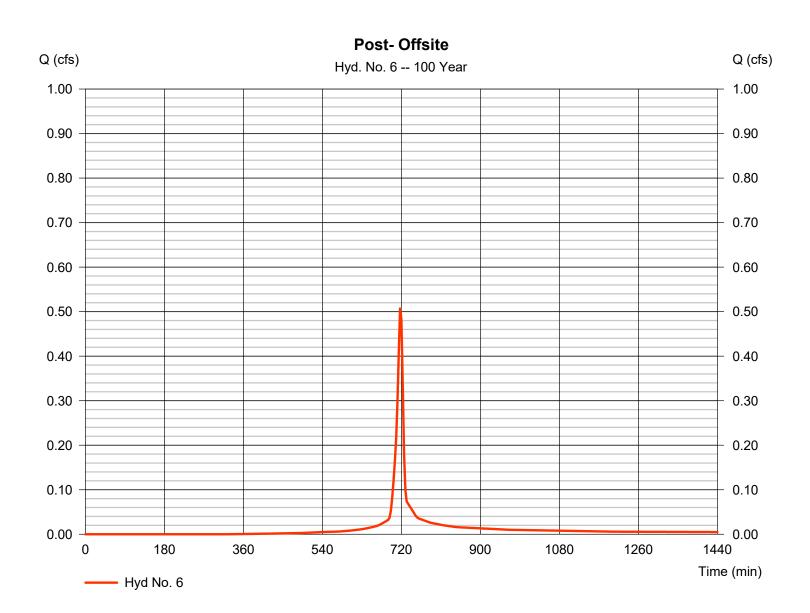
Monday, 07 / 9 / 2018

Hyd. No. 6

Post- Offsite

Hydrograph type = SCS Runoff Peak discharge = 0.509 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1,171 cuftCurve number Drainage area = 0.090 ac= 84* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. Distribution = Type II = 5.60 inShape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.030 \times 61) + (0.050 \times 98) + (0.010 \times 80)] / 0.090$



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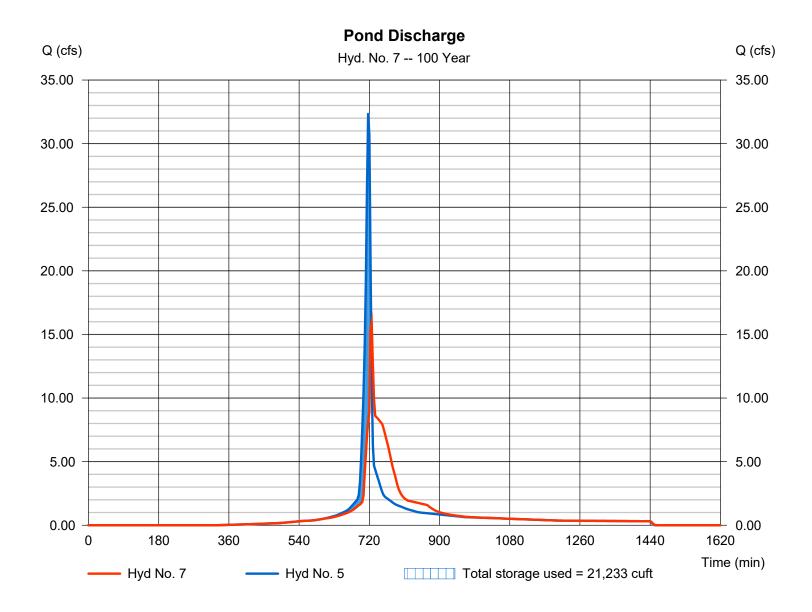
Monday, 07 / 9 / 2018

Hyd. No. 7

Pond Discharge

Hydrograph type = Reservoir Peak discharge = 15.91 cfsStorm frequency = 100 yrsTime to peak = 726 min Time interval = 3 min Hyd. volume = 74,559 cuft Inflow hyd. No. Max. Elevation = 139.80 ft= 5 - Post- Pond = South Detention = 21,233 cuft Reservoir name Max. Storage

Storage Indication method used.



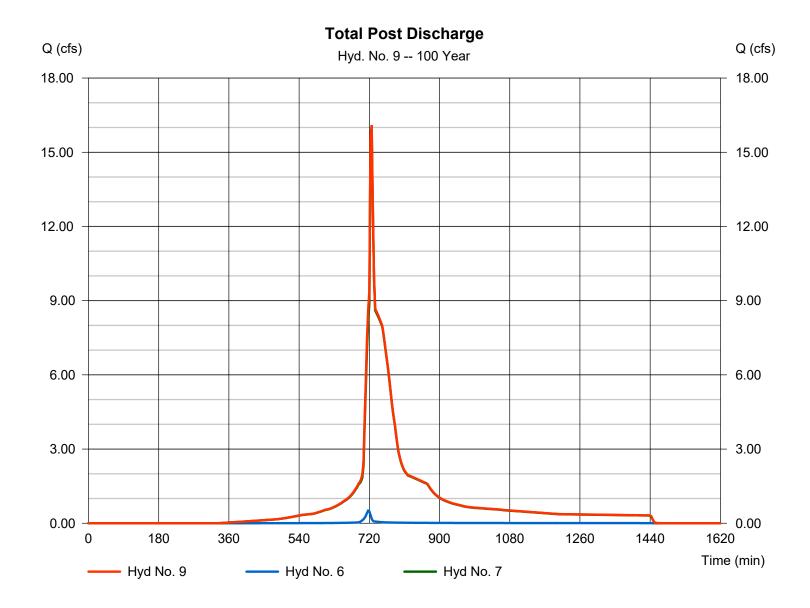
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Monday, 07 / 9 / 2018

Hyd. No. 9

Total Post Discharge

Hydrograph type = Combine Peak discharge = 16.09 cfsStorm frequency Time to peak = 100 yrs= 726 min Time interval = 3 min Hyd. volume = 75,730 cuftInflow hyds. = 6, 7 Contrib. drain. area = 0.090 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

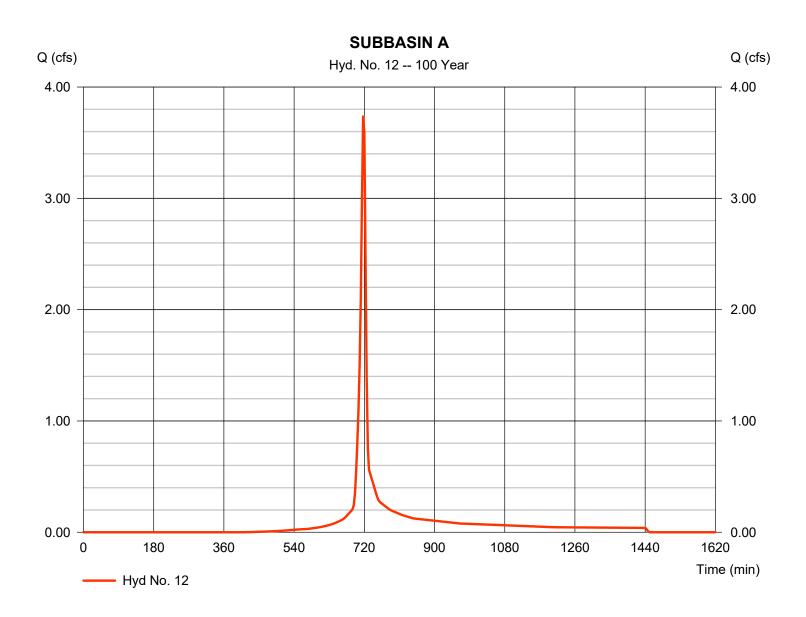
Monday, 07 / 9 / 2018

Hyd. No. 12

SUBBASIN A

Hydrograph type = SCS Runoff Peak discharge = 3.742 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 8.486 cuft Curve number Drainage area = 0.750 ac= 79* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.230 \times 98) + (0.240 \times 61) + (0.280 \times 80)] / 0.750$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

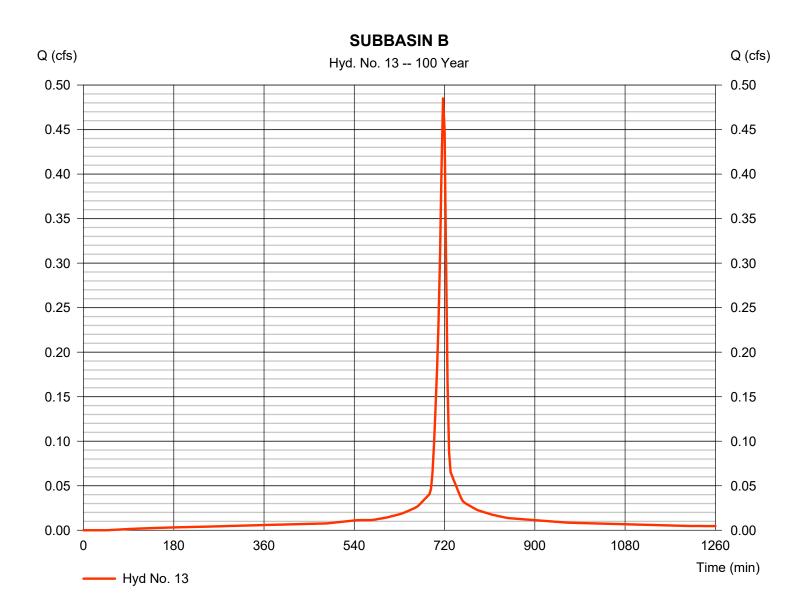
Monday, 07 / 9 / 2018

Hyd. No. 13

SUBBASIN B

Hydrograph type = SCS Runoff Peak discharge = 0.486 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.277 cuft Curve number Drainage area = 0.070 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.070 x 98)] / 0.070



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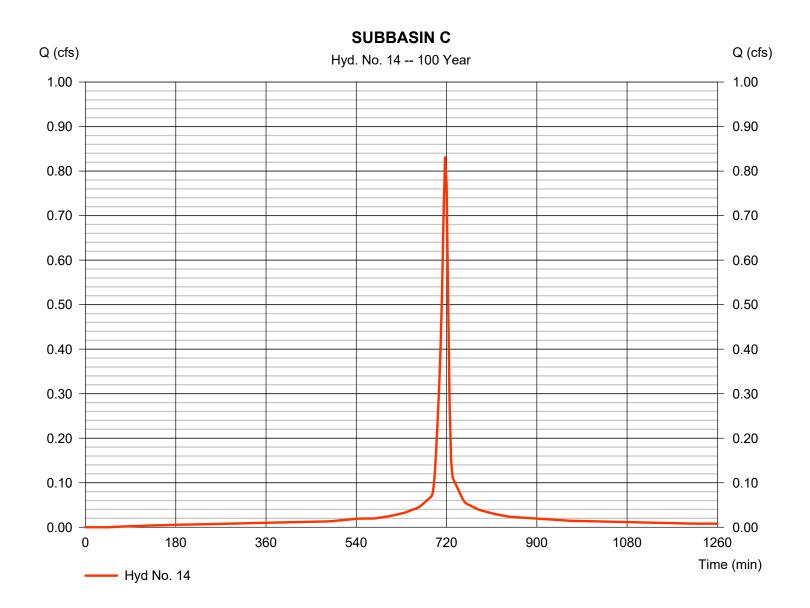
Monday, 07 / 9 / 2018

Hyd. No. 14

SUBBASIN C

Hydrograph type = SCS Runoff Peak discharge = 0.833 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2.190 cuftCurve number Drainage area = 0.120 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.120 x 98)] / 0.120



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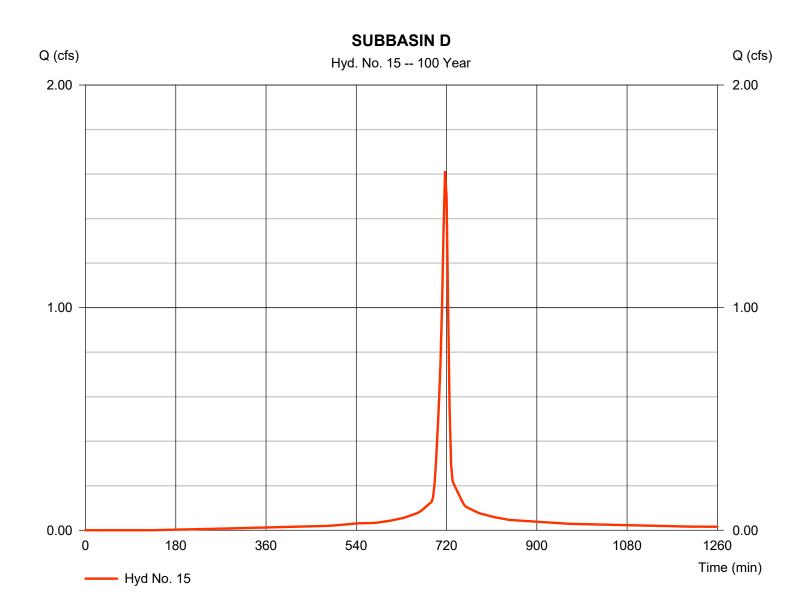
Monday, 07 / 9 / 2018

Hyd. No. 15

SUBBASIN D

Hydrograph type = SCS Runoff Peak discharge = 1.613 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 4,003 cuftCurve number Drainage area = 0.240 ac= 94* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.050 \times 80)] / 0.240$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

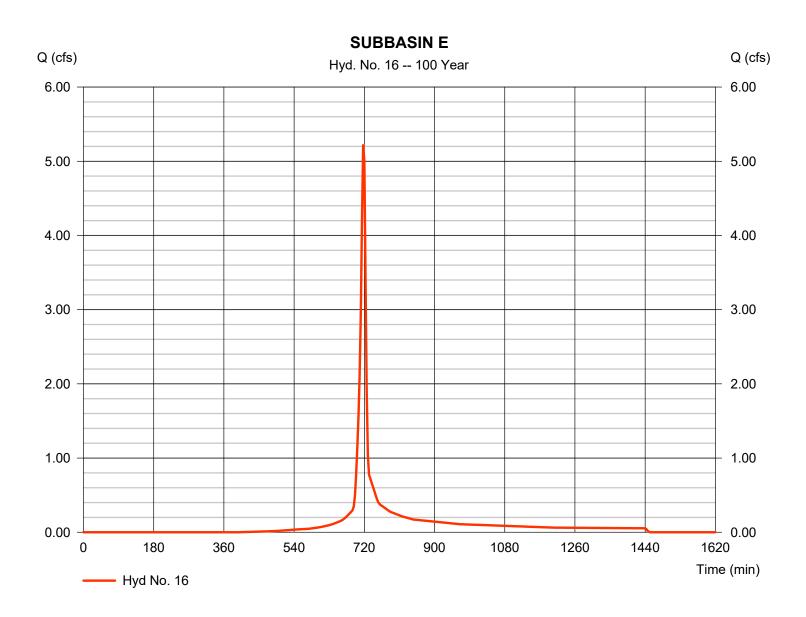
Monday, 07 / 9 / 2018

Hyd. No. 16

SUBBASIN E

Hydrograph type = SCS Runoff Peak discharge = 5.227 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 11.880 cuft Curve number Drainage area = 1.020 ac= 80* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = [(0.020 x 98) + (1.000 x 80)] / 1.020



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

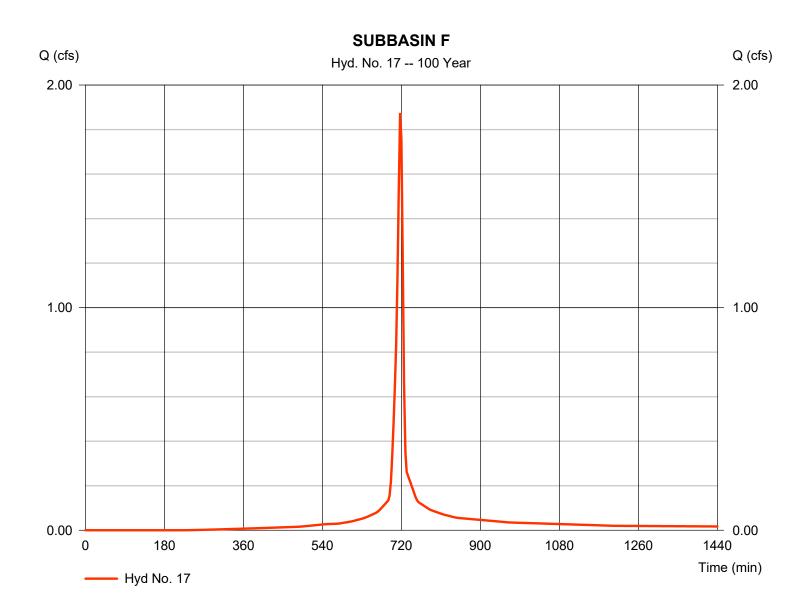
Monday, 07 / 9 / 2018

Hyd. No. 17

SUBBASIN F

Hydrograph type = SCS Runoff Peak discharge = 1.875 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 4,440 cuftCurve number Drainage area = 0.300 ac= 89* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.190 \times 98) + (0.110 \times 74)] / 0.300$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

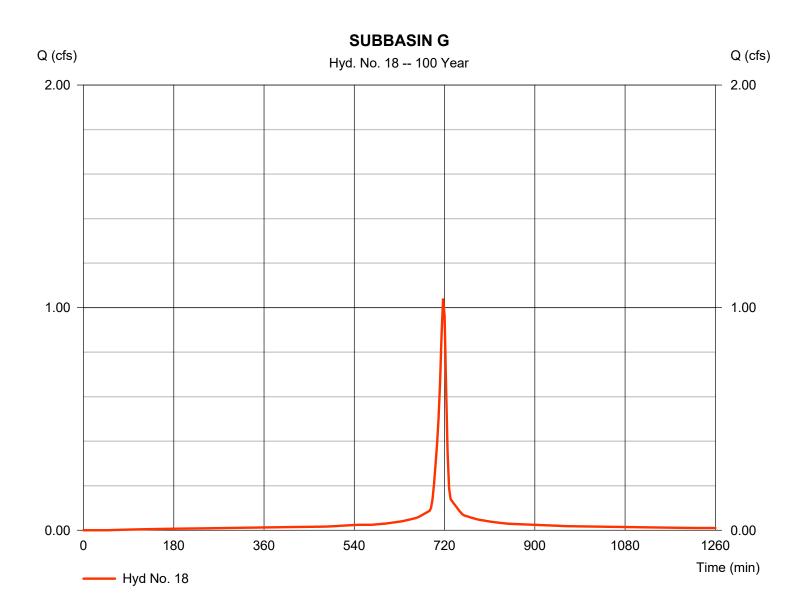
Monday, 07 / 9 / 2018

Hyd. No. 18

SUBBASIN G

Hydrograph type = SCS Runoff Peak discharge = 1.041 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 2.737 cuftCurve number Drainage area = 0.150 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.150 x 98)] / 0.150



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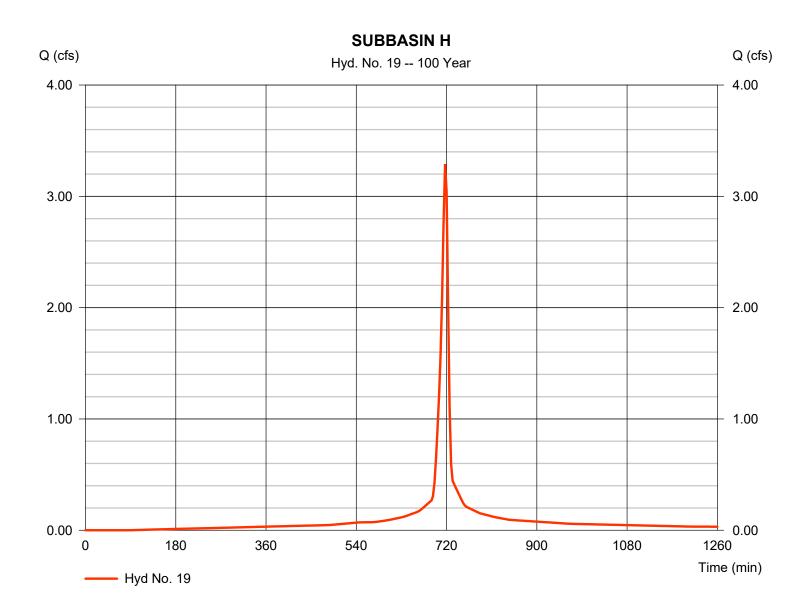
Monday, 07 / 9 / 2018

Hyd. No. 19

SUBBASIN H

Hydrograph type = SCS Runoff Peak discharge = 3.289 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 8,379 cuftCurve number Drainage area = 0.480 ac= 96* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.430 \times 98) + (0.050 \times 74)] / 0.480$



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

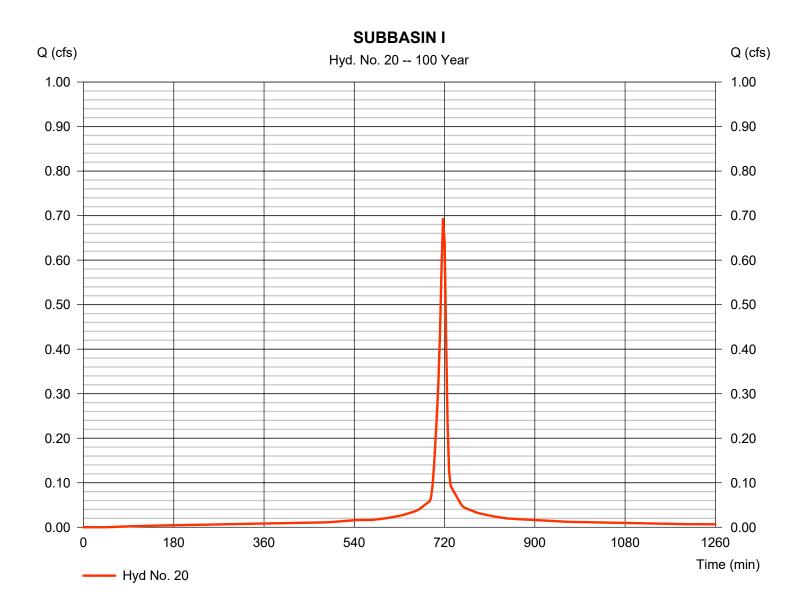
Monday, 07 / 9 / 2018

Hyd. No. 20

SUBBASIN I

Hydrograph type = SCS Runoff Peak discharge = 0.694 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 1.825 cuft Drainage area Curve number = 0.100 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 6.00 \, \text{min}$ Total precip. = 5.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.100 x 98)] / 0.100



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

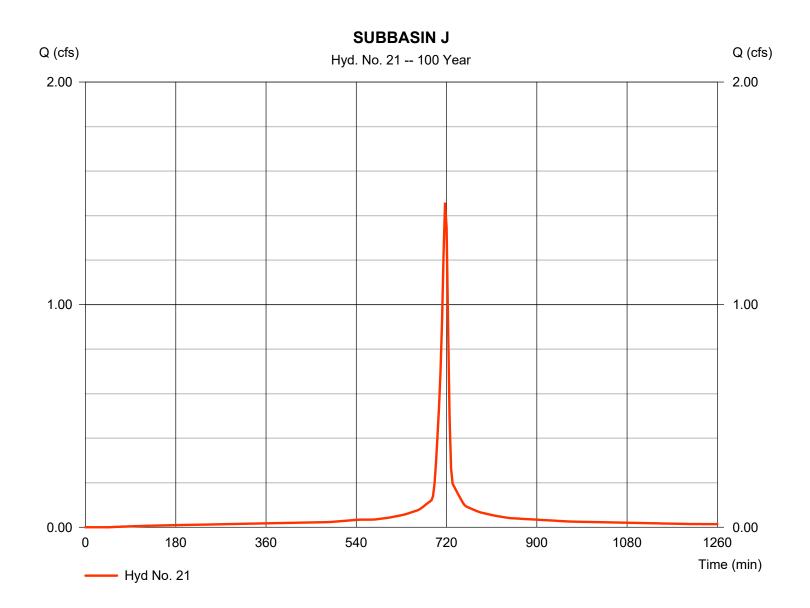
Monday, 07 / 9 / 2018

Hyd. No. 21

SUBBASIN J

Hydrograph type = SCS Runoff Peak discharge = 1.458 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 3.832 cuft Curve number Drainage area = 0.210 ac= 98* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(0.210 x 98)] / 0.210



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

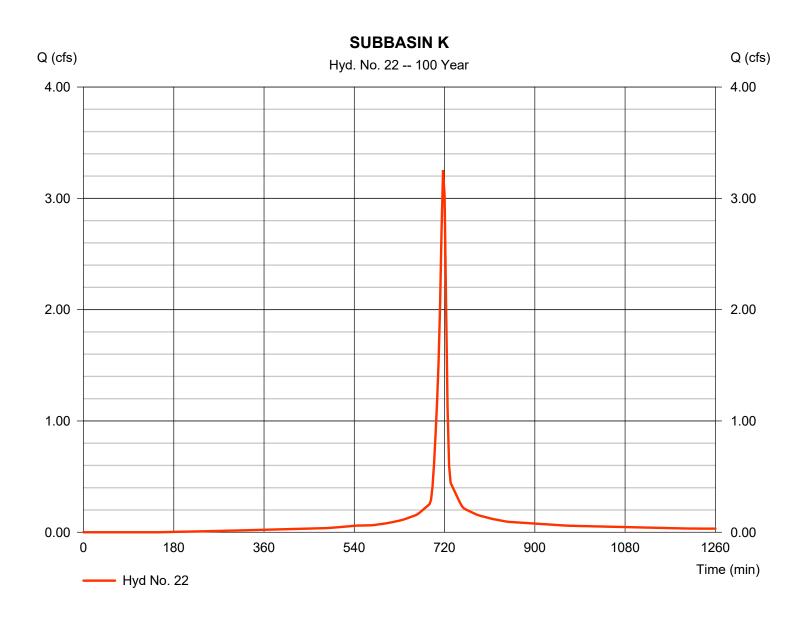
Monday, 07 / 9 / 2018

Hyd. No. 22

SUBBASIN K

Hydrograph type = SCS Runoff Peak discharge = 3.254 cfsStorm frequency = 100 yrsTime to peak = 717 min Time interval = 3 min Hyd. volume = 7.984 cuft Curve number Drainage area = 0.490 ac= 93* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 6.00 min = User Total precip. = 5.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

^{*} Composite (Area/CN) = $[(0.380 \times 98) + (0.110 \times 74)] / 0.490$



Appendix F SLAMM Input / output Information:

slamm - InputData.txt

Data file name: F:\Job Files\1818660 Montessori School of Waukesha-Waukesha,

WI\1818664 Civil\storm water report and calculations\slamm.mdb

WinSLAMM Version 10.3.2

Rain file name: F:\Programs\civil\WinSLAMM\v10.3.2\Parameter Files\WisReg - Milwaukee WI 1969.RAN

Particulate Solids Concentration file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\v10.1 WI_AVG01.pscx
Runoff Coefficient file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter
Files\WI SL06 Dec06.rsvx

Residential Street Delivery file name:

 $F:\Pr{ograms\Civil\WinSLAMM\v10.3.2\Parameter\ Files\WI_Res\ and\ Other\ Urban\ Dec06.std}\\ Institutional\ Street\ Delivery\ file\ name:$

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI_Com Inst Indust Dec06.std Commercial Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI Com Inst Indust Dec06.std

Industrial Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter
Files\WI Com Inst Indust Dec06.std

Other Urban Street Delivery file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI_Res and Other Urban Dec06.std Freeway Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\Freeway Dec06.std

Apply Street Delivery Files to Adjust the After Event Load Street Dirt Mass Balance: False

Pollutant Relative Concentration file name:

F:\Programs\civil\WinSLAMM\v10.3.2\Parameter Files\WI GE003.ppdx

Source Area PSD and Peak to Average Flow Ratio File:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\NURP Source Area PSD Files.csv Cost Data file name:

Seed for random number generator: -42

Study period starting date: 01/05/69 Study period ending date: 12/31/69

Start of Winter Season: 12/06 End of Winter Season: 03/28

Date: 07-05-2018 Time: 15:19:50

Site information:

- LU# 1 Institutional: Filter Total area (ac): 5.720
- 1 Roofs 1: 0.570 ac. Flat Connected Source Area PSD File:

C:\WinSLAMM Files\NURP.cpz

- 13 Paved Parking 1: 1.770 ac. Connected Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
- 45 Large Landscaped Areas 1: 3.380 ac. Normal Clayey Low Density Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
- LU# 2 Institutional: Offsite Total area (ac): 0.090
- 13 Paved Parking 1: 0.050 ac. Connected Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
- 45 Large Landscaped Areas 1: 0.040 ac. Normal Clayey Low Density Source Area PSD File: C:\WinSLAMM Files\NURP.cpz

slamm - InputData.txt

Control Practice 1: Upflo Filter CP# 1 (DS) - DS UpfloFilter # 1

Media Type: CPZ

Fraction of Area Served by Upflo Filters (0-1): 1.0 Height from Outlet Invert to Structure Top (ft): 4.0

Sump Depth (ft): 2.00

Sump Cleaning/Filter Replacement is not considered during the model run

Solve for Given Conditions Number of filters: 15

Upflo Filter particle size distribution file name: Not needed -

calculated by program

slamm - Output Summary.txt

SLAMM for Windows Version 10.3.2

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Data file name: F:\Job Files\1818660 Montessori School of Waukesha-Waukesha,

WI\1818664 Civil\storm water report and calculations\slamm.mdb

Data file description:

Rain file name: F:\Programs\civil\WinSLAMM\v10.3.2\Parameter Files\WisReg -

Milwaukee WI 1969.RAN

Particulate Solids Concentration file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\v10.1 WI_AVG01.pscx

 $\label{lem:coefficient} Runoff \ \ Coefficient \ file \ name: \ F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter$

Files\WI_SL06 Dec06.rsvx

Residential Street Delivery file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI_Res and Other Urban Dec06.std Institutional Street Delivery file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI_Com Inst Indust Dec06.std Commercial Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter

Files\WI_Com Inst Indust Dec06.std

Industrial Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter
Files\WI Com Inst Indust Dec06.std

Other Urban Street Delivery file name:

F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\WI_Res and Other Urban Dec06.std Freeway Street Delivery file name: F:\Programs\Civil\WinSLAMM\v10.3.2\Parameter Files\Freeway Dec06.std

Pollutant Relative Concentration file name:

F:\Programs\civil\WinSLAMM\v10.3.2\Parameter Files\WI_GE003.ppdx

Start of Winter Season: 12/06 End of Winter Season: 03/28

Model Run Start Date: 01/05/69 Model Run End Date: 12/31/69

Date of run: 07-05-2018 Time of run: 15:19:36

Total Area Modeled (acres): 5.810

Years in Model Run: 0.99

				Runoff	Percent			
Particulate	Particula	ate Per	cent					
				Volume	Runoff			
Solids								
				(cu ft)	Volume			
Conc.	Yield	Solids			Dad. attau			
(mg/L)	(1hc)	Doduction			Reduction			
(mg/L)	(lbs)	Reduction						
Total of al	-							
120.5	1595	-						
Outfall Tot	-0.11%							
43.27	573.2	64.06%						
Annualized	Total Afte	er Outfall	Controls:	215158				
581.	2							