

OLLMANN ERNEST MARTIN ARCHITECTS

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February 19, 2016

Mr. Randall R. Dahmen, P.E.
Engineering Consultant, WI Division of Industry Services

Transaction ID No. 2662586
Site ID No. 803873
RE: Culvers of Waukesha
840 W. Sunset Dr.
Waukesha, WI 53189
Review Comments: 02/11/2016

Mr. Dahmen:

We have responded to your review comments as follows; item numbers correspond to the numbered items in the review.

- Item 1 SPS 361.31(2): *See attached stamped/signed structural calculation.*
- Item 2 SPS 361.31(2): *See attached stamped/signed HVAC Load Analysis.*
- Item 3 SPS 361.31(2)(e): *See attached stamped/signed structural calculation.*
- Item 4 SPS 361.31(2)(e): *See attached stamped/signed structural calculation.*
- Item 5 SPS 361.31(2) & IBC 1608: *See attached stamped/signed structural calculation. There is a little step between the existing and the new addition; however, the tapered insulation makes up for this step. We have revised the spacing of the joists for the addition. See attached sheet S102 to show the 2x12s are at 12" o.c.*
- Item 6 IBC 715.4.10: *As indicated in Specification section 083400 Overhead Coiling Fire Doors, the coiling door is a 1.5 hour rated door with self resetting test operation. Per 2.01:F: the door has an automatic closing operation at 165 degree thermal (fusible) link positioned at each side of wall, with manual over ride release.*
- Item 7 IBC 703.6: *Per Specification section 083400 Overhead Coiling Fire Doors:2.01:K: the fire shutter is to be provided with a permanently affixed UL label indicating class of door.*
- Item 8 IBC 716.4: *Note has been added to keynote #4 on attached sheet M101.*
- Item 9 IFGC 401/SPS 365.0400: *Note has been added to General Note #13 on attached sheet M101.*
- Item 10 IECC 403.2.2/IECC 503.2.7/IMC 603.9: *Note has been added to Specification section 233113 Ductwork:3:A on page 3.*
- Item 11 IBC 1101.2/ANSI A117.1-308.2 & 3: *Note has been added at Stat locations on attached sheet M101.*

Additional Documents:

Structural Calculations, HVAC Load Analysis, Spec Section 233113, S102 and M101.

Please feel free to contact me with any questions or comments.

Sincerely,

Todd William Ost, AIA
Ollmann Ernest Martin Architects

Cc: File

Ollmann Ernest Martin Architects

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JOB TITLE Waukesha Culvers

1 of 19

JOB NO. 2015-093

SHEET NO.

CALCULATED BY _____

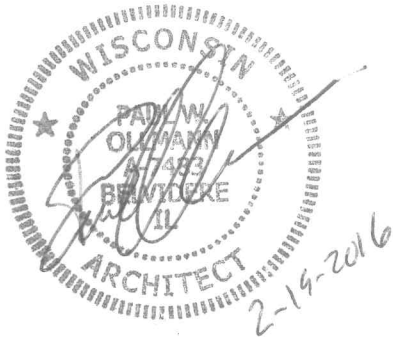
DATE 2/4/16

CHECKED BY _____

DATE _____

CS12 Ver 2013.07.01

www.struware.com



STRUCTURAL CALCULATIONS

FOR

Waukesha Culvers

Waukesha, Wisconsin

Code Search**Code:** Wisconsin Bldg Code**Occupancy:**

Occupancy Group = A Assembly

Occupancy Category & Importance Factors:

Occupancy Category =	II
Wind factor =	1.00
Snow factor =	1.00
Seismic factor =	1.00

Type of Construction:

Fire Rating:	
Roof =	0.0 hr
Floor =	0.0 hr

Building Geometry:

Roof angle (θ)	0.25 / 12	1.2 deg
Building length (L)	26.0 ft	
Least width (B)	25.0 ft	
Mean Roof Ht (h)	12.0 ft	
Parapet ht above grd	16.0 ft	
Minimum parapet ht	4.0 ft	

Live Loads:

Roof	0 to 200 sf: 20 psf
	200 to 600 sf: 24 - 0.02Area, but not less than 12 psf
	over 600 sf: 12 psf

Floor:

Typical Floor	50 psf
Partitions	15 psf
Corridors above first floor	80 psf
Lobbies & first floor corridors	100 psf
Balconies (exterior) - same as occup:	50 psf

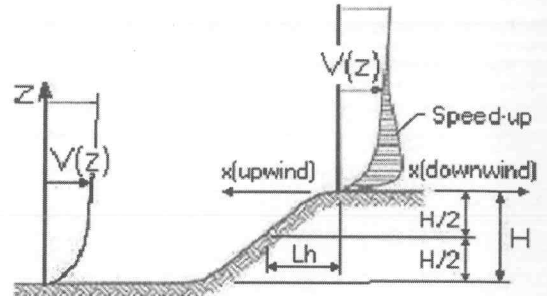
Wind Loads :

ASCE 7 - 05

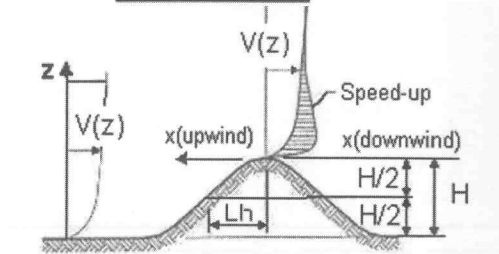
Basic Wind Speed	90 mph
Importance Factor	1.00
Occupancy Category	II
Exposure Category	B
Enclosure Classif.	Enclosed Building
Internal pressure	+/-0.18
Directionality (Kd)	0.85
Kh case 1	0.701
Kh case 2	0.575
Type of roof	Monoslope

Topographic Factor (Kzt)

Topography	Flat
Hill Height (H)	80.0 ft
Half Hill Length (Lh)	100.0 ft
Actual H/Lh =	0.80
Use H/Lh =	0.50
Modified Lh =	160.0 ft
From top of crest: x =	50.0 ft
Bldg up/down wind?	downwind
H/Lh = 0.50	K ₁ = 0.000
x/Lh = 0.31	K ₂ = 0.792
z/Lh = 0.09	K ₃ = 1.000
At Mean Roof Ht:	
Kzt = (1+K ₁ K ₂ K ₃) ² =	1.00



ESCARPMENT



2D RIDGE or 3D AXISYMMETRICAL HILL

Gust Effect Factor

h =	12.0 ft
B =	25.0 ft
/z (0.6h) =	30.0 ft

Flexible structure if natural frequency < 1 Hz (T > 1 second).

However, if building h/B < 4 then probably rigid structure (rule of thumb).

h/B = 0.48 Rigid structure

G = 0.85 Using rigid structure default

Rigid Structure

e-bar =	0.33
l =	320 ft
Z _{min} =	30 ft
c =	0.30
g _Q , g _v =	3.4
L _z =	310.0 ft
Q =	0.93
I _z =	0.30
G =	0.88 use G = 0.85

Flexible or Dynamically Sensitive Structure

Natural Frequency (η ₁) =	0.0 Hz		
Damping ratio (β) =	0		
/b =	0.45		
/α =	0.25		
V _z =	58.0		
N ₁ =	0.00		
K _n =	0.000		
R _h =	28.282	η =	0.000
R _B =	28.282	η =	0.000
R _L =	28.282	η =	0.000
g _R =	0.000		
R =	0.000		
G =	0.000		
		h =	12.0 ft

Enclosure Classification

Test for Enclosed Building: A building that does not qualify as open or partially enclosed.

Test for Open Building: All walls are at least 80% open.
 $A_o \geq 0.8A_g$

Test for Partially Enclosed Building:

Input		Test	
Ao	0.0 sf	$A_o \geq 1.1A_{oi}$	YES
Ag	0.0 sf	$A_o > 4'$ or $0.01A_g$	NO
Aoi	0.0 sf	$A_{oi} / A_{gi} \leq 0.20$	NO
Agi	0.0 sf		

Building is NOT Partially Enclosed

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

- $A_o \geq 1.1A_{oi}$
- $A_o >$ smaller of 4' or $0.01 A_g$
- $A_{oi} / A_{gi} \leq 0.20$

Where:

- Ao = the total area of openings in a wall that receives positive external pressure.
- Ag = the gross area of that wall in which Ao is identified.
- Aoi = the sum of the areas of openings in the building envelope (walls and roof) not including Ao.
- Agi = the sum of the gross surface areas of the building envelope (walls and roof) not including Ag.

Reduction Factor for large volume partially enclosed buildings (Ri) :

If the partially enclosed building contains a single room that is unpartitioned , the internal pressure coefficient may be multiplied by the reduction factor Ri.

Total area of all wall & roof openings (Aog): 0 sf
 Unpartitioned internal volume (Vi) : 0 cf
 Ri = 1.00

Altitude adjustment to constant 0.00256 (caution - see code) :

Altitude = 0 feet Average Air Density = 0.0765 lbm/ft³
 Constant = 0.00256

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Altitude = 0 feet Average Air Density = 0.0765 lbm/ft³
 Constant = 0.00256

Wind Loads - MWFRS all h (Enclosed/partially enclosed only)

Kh (case 2) = 0.57	h = 12.0 ft	GCpi = +/-0.18
Base pressure (qh) = 10.1 psf	ridge ht = 12.3 ft	G = 0.85
Roof Angle (θ) = 1.2 deg	L = 26.0 ft	qi = qh
Roof tributary area - (h/2)*L: 156 sf	B = 25.0 ft	
(h/2)*B: 150 sf		

Nominal Wind Surface Pressures (psf)

Surface	Wind Normal to Ridge				Wind Parallel to Ridge				
	B/L = 0.96		h/L = 0.48		L/B = 1.04		h/L = 0.46		
	Cp	qhGCp	w/+qiGCpi	w/-qhGCpi	Dist.*	Cp	qhGCp	w/+qiGCpi	w/-qhGCpi
Windward Wall (WW)	0.80	6.9	see table below			0.80	6.9	see table below	
Leeward Wall (LW)	-0.50	-4.3	-6.1	-2.5		-0.49	-4.2	-6.1	-2.4
Side Wall (SW)	-0.70	-6.0	-7.9	-4.2		-0.70	-6.0	-7.9	-4.2
Leeward Roof (LR)	**				Included in windward roof				
Windward Roof: 0 to h/2*	-0.90	-7.7	-9.6	-5.9	0 to h/2*	-0.90	-7.7	-9.6	-5.9
h/2 to h*	-0.90	-7.7	-9.6	-5.9	h/2 to h*	-0.90	-7.7	-9.6	-5.9
h to 2h*	-0.50	-4.31	-6.13	-2.48	h to 2h*	-0.50	-4.3	-6.1	-2.5
> 2h*	-0.30	-2.58	-4.41	-0.76	> 2h*	-0.30	-2.6	-4.4	-0.8

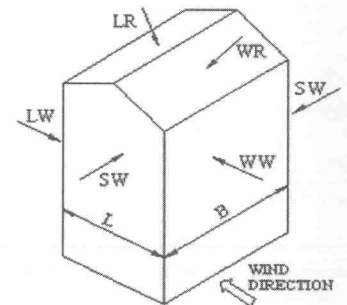
**Roof angle < 10 degrees. Therefore, leeward roof is included in windward roof pressure zones.

*Horizontal distance from windward edge

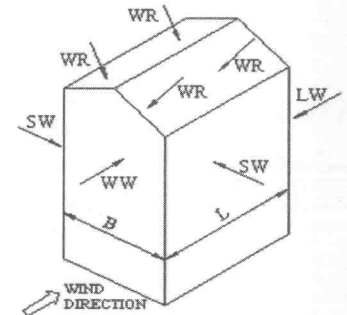
For monoslope roofs, entire roof surface is either windward or leeward surface.

Windward Wall Pressures at "z" (psf)

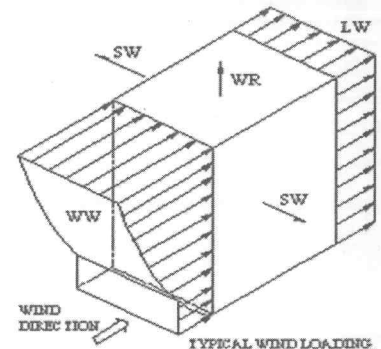
z	Kz	Kzt	qzGCp	Windward Wall		Combined WW + LW	
				w/+qiGCpi	w/-qhGCpi	Normal to Ridge	Parallel to Ridge
h= 0 to 15'	0.57	1.00	6.9	5.1	8.7	11.2	11.1



WIND NORMAL TO RIDGE



WIND PARALLEL TO RIDGE



TYPICAL WIND LOADING

NOTE:
 See figure in ASCE7 for the application of full and partial loading of the above wind pressures. There are 4 different loading cases.

Parapet

z	Kz	Kzt	qp (psf)
16.0 ft	0.59	1.00	10.3

Windward parapet: 15.5 psf (GCpn = +1.5)
 Leeward parapet: -10.3 psf (GCpn = -1.0)

Windward roof overhangs (add to windward roof pressure) : 6.9 psf (upward)

Wind Loads - MWFRS $h \leq 60'$ (Low-rise Buildings) Enclosed/partially enclosed only

$K_z = K_h$ (case 1) = 0.70
 Base pressure (qh) = **12.3 psf**
 $G_{Cpi} = +/-0.18$

Edge Strip (a) = 3.0 ft
 End Zone (2a) = 6.0 ft
 Zone 2 length = 12.5 ft

Wind Pressure Coefficients

Surface	Transverse Direction			Longitudinal Direction		
	Perpendicular $\theta = 1.2$ deg			Parallel $\theta = 0.0$		
	GCpf	w/-GCpi	w/+GCpi	GCpf	w/-GCpi	w/+GCpi
1	0.40	0.58	0.22	0.40	0.58	0.22
2	-0.69	-0.51	-0.87	-0.69	-0.51	-0.87
3	-0.37	-0.19	-0.55	-0.37	-0.19	-0.55
4	-0.29	-0.11	-0.47	-0.29	-0.11	-0.47
5	-0.45	-0.27	-0.63	-0.45	-0.27	-0.63
6	-0.45	-0.27	-0.63	-0.45	-0.27	-0.63
1E	0.61	0.79	0.43	0.61	0.79	0.43
2E	-1.07	-0.89	-1.25	-1.07	-0.89	-1.25
3E	-0.53	-0.35	-0.71	-0.53	-0.35	-0.71
4E	-0.43	-0.25	-0.61	-0.43	-0.25	-0.61

Nominal Wind Surface Pressures (psf)

1	7.2	2.7	7.2	2.7
2	-6.3	-10.7	-6.3	-10.7
3	-2.3	-6.8	-2.3	-6.8
4	-1.4	-5.8	-1.4	-5.8
5	-3.3	-7.8	-3.3	-7.8
6	-3.3	-7.8	-3.3	-7.8
1E	9.8	5.3	9.8	5.3
2E	-11.0	-15.4	-11.0	-15.4
3E	-4.3	-8.8	-4.3	-8.8
4E	-3.1	-7.5	-3.1	-7.5

Parapet

Windward parapet = 18.5 psf (GCpn = +1.5)
 Leeward parapet = -12.3 psf (GCpn = -1.0)

Windward roof overhangs = 8.4 psf (upward) add to windward roof pressure

Horizontal MWFRS Simple Diaphragm Pressures (psf)

Transverse direction (normal to L)

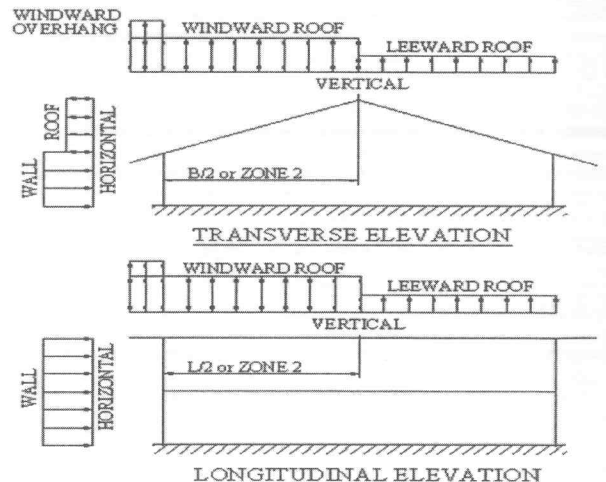
Interior Zone: Wall 8.5 psf
 Roof -4.0 psf **
 End Zone: Wall 12.8 psf
 Roof -6.7 psf **

Longitudinal direction (parallel to L)

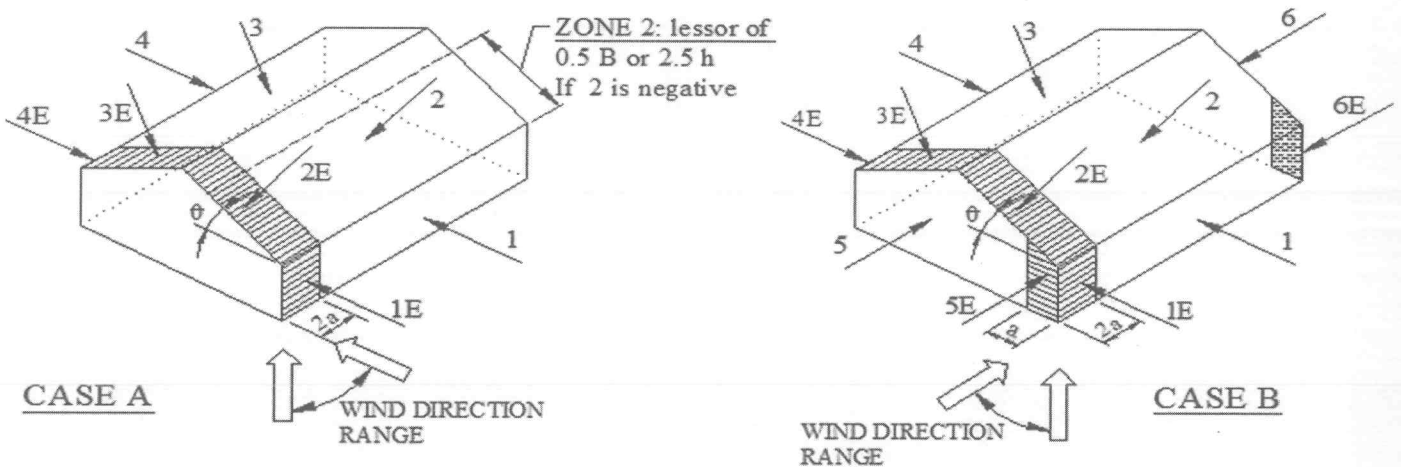
Interior Zone: Wall 8.5 psf
 End Zone: Wall 12.8 psf

** NOTE: Total horiz force shall not be less than that determined by neglecting roof forces (except for MWFRS moment frames).

The code requires the MWFRS as a minimum be designed for a 10 psf force applied to the vertical projection of the structure.

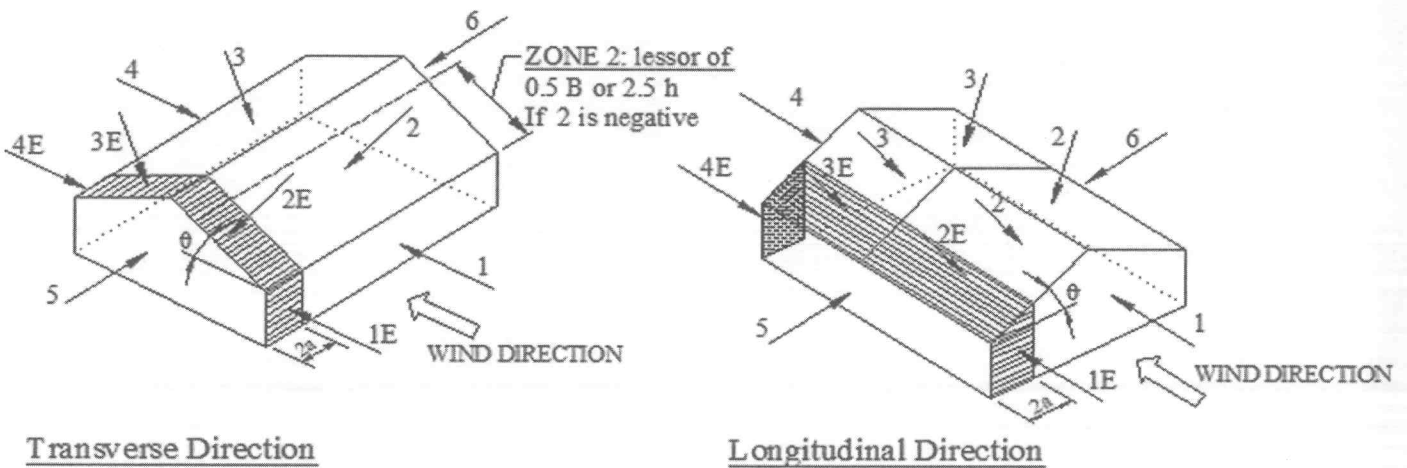


Location of MWFRS Wind Pressure Zones



NOTE: Torsional loads are 25% of zones 1 - 6. See code for loading diagram.

ASCE 7 -99 and ASCE 7-10 (& later)



NOTE: Torsional loads are 25% of zones 1 - 4. See code for loading diagram.

ASCE 7 -02 and ASCE 7-05

Nominal Wind Pressures

Wind Loads - Components & Cladding : h <= 60'

Kh (case 1) = 0.70 h = 12.0 ft
Base pressure (qh) = 12.3 psf a = 3.0 ft
Minimum parapet ht = 4.0 ft GCpi = +/-0.18
Roof Angle (θ) = 1.2 deg
Type of roof = Monoslope

Roof Area	GCp +/- GCpi			Surface Pressure (psf)			User input	
	10 sf	50 sf	100 sf	10 sf	50 sf	100 sf	75 sf	500 sf
Negative Zone 1	-1.18	-1.11	-1.08	-14.6	-13.7	-13.3	-13.5	-13.3
Negative Zone 2	-1.98	-1.49	-1.28	-24.4	-18.4	-15.8	-16.9	-15.8
Negative Zone 3	-1.98	-1.49	-1.28	-24.4	-18.4	-15.8	-16.9	-15.8
Positive Zone 1	0.48	0.41	0.38	10.0	10.0	10.0	10.0	10.0
Positive Zones 2 & 3	1.08	0.97	0.92	13.3	12.0	11.4	11.6	10.0
Overhang Zone 1&2	-1.70	-1.63	-1.60	-21.0	-20.1	-19.8	-19.9	-13.6
Overhang Zone 3	-1.70	-1.63	-1.60	-21.0	-20.1	-19.8	-19.9	-13.6

Negative zone 3 = zone 2, since parapet >= 3ft.

Overhang pressures in the table above assume an internal pressure coefficient (Gcpi) of 0.0

Parapet

qp = 12.3 psf

CASE A = pressure towards building (pos)
CASE B = pressure away from bldg (neg)

Solid Parapet Pressure	Surface Pressure (psf)			User input
	10 sf	100 sf	500 sf	40 sf
CASE A : Interior zone:	33.3	22.7	21.4	27.0
Corner zone:	33.3	22.7	21.4	27.0
CASE B : Interior zone:	-23.3	-19.4	-16.7	-21.0
Corner zone:	-26.7	-20.8	-16.7	-23.1

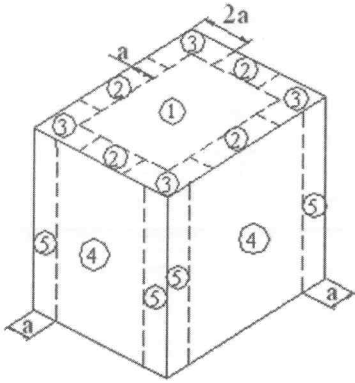
Walls

Area	GCp +/- GCpi			Surface Pressure (psf)			User input	
	10 sf	100 sf	500 sf	10 sf	100 sf	500 sf	50 sf	200 sf
Negative Zone 4	-1.17	-1.01	-0.90	-14.4	-12.5	-11.1	-13.1	-11.9
Negative Zone 5	-1.44	-1.12	-0.90	-17.8	-13.9	-11.1	-15.0	-12.7
Positive Zone 4 & 5	1.08	0.92	0.81	13.3	11.4	10.0	12.0	10.8

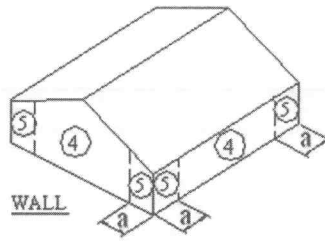
Note: GCp reduced by 10% due to roof angle <= 10 deg.

Nominal Wind Pressures

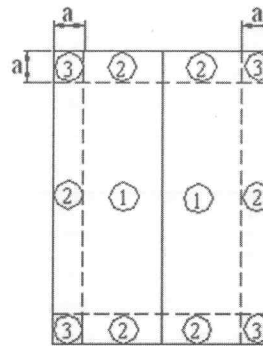
Location of C&C Wind Pressure Zones



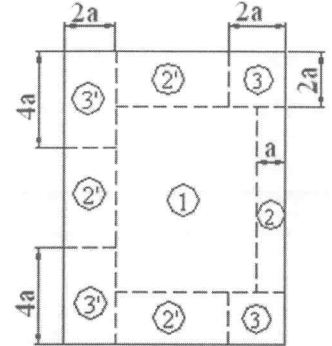
Roofs w/ $\theta \leq 10^\circ$
 and all walls
 $h > 60'$



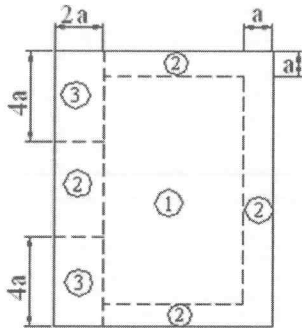
Walls $h \leq 60'$
 & alt design $h < 90'$



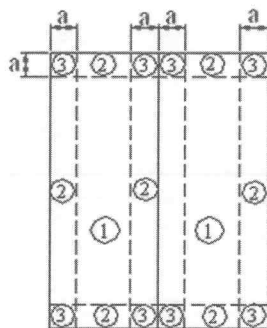
Gable, Sawtooth and
 Multispan Gable $\theta \leq 7$ degrees &
 Monoslope ≤ 3 degrees
 $h \leq 60'$ & alt design $h < 90'$



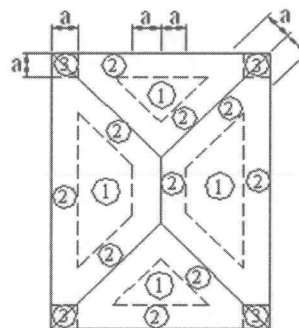
Monoslope roofs
 $3^\circ < \theta \leq 10^\circ$
 $h \leq 60'$ & alt design $h < 90'$



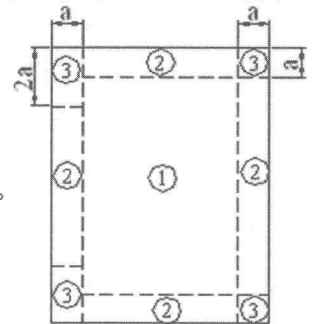
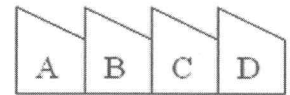
Monoslope roofs
 $10^\circ < \theta \leq 30^\circ$
 $h \leq 60'$ & alt design $h < 90'$



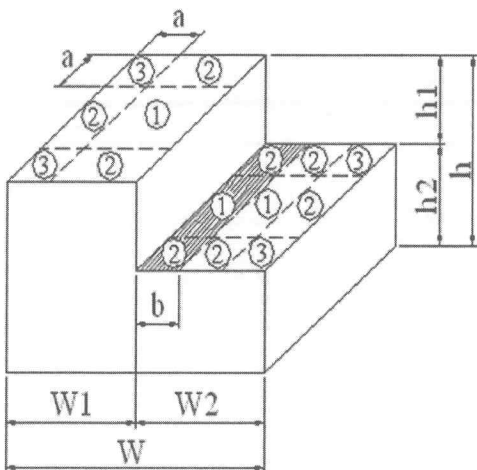
Multispan Gable &
 Gable $7^\circ < \theta \leq 45^\circ$



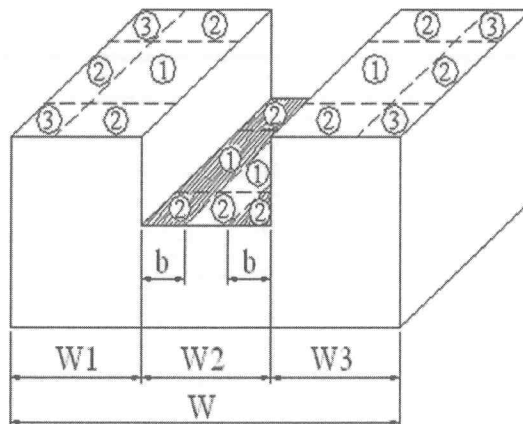
Hip $7^\circ < \theta \leq 27^\circ$



Sawtooth $10^\circ < \theta \leq 45^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Stepped roofs $\theta \leq 3^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Snow Loads : ASCE 7-05

Nominal Snow Forces

Roof slope = 1.2 deg
 Horiz. eave to ridge dist (W) = 25.0 ft
 Roof length parallel to ridge (L) = 26.0 ft

Type of Roof Monoslope
 Ground Snow Load $P_g = 30.0$ psf
 Occupancy Category = II
 Importance Factor $I = 1.0$
 Thermal Factor $C_t = 1.00$
 Exposure Factor $C_e = 1.0$

$P_f = 0.7 * C_e * C_t * I * P_g = 21.0$ psf
 Unobstructed Slippery Surface yes

Sloped-roof Factor $C_s = 1.00$
 Balanced Snow Load $P_s = 21.0$ psf

Rain on Snow Surcharge Angle 0.50 deg
 Code Maximum Rain Surcharge 5.0 psf
 Rain on Snow Surcharge = 0.0 psf
 P_s plus rain surcharge = 21.0 psf
 Minimum Snow Load $P_{fmin} = 20.0$ psf

Uniform Roof Design Snow Load = 21.0 psf

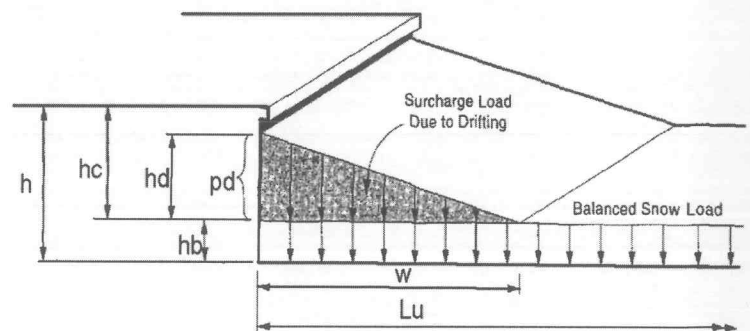
NOTE: Alternate spans of continuous beams and other areas shall be loaded with half the design roof snow load so as to produce the greatest possible effect - see code.

Windward Snow Drifts 1 - Against walls, parapets, etc more than 15' long

Upwind fetch $l_u = 26.0$ ft
 Projection height $h = 4.0$ ft
 Snow density $g = 17.9$ pcf
 Balanced snow height $h_b = 1.17$ ft
 $h_c = 2.83$ ft
 $h_c/h_b > 0.2 = 2.4$ Therefore, design for drift
 Drift height (h_d) = 1.28 ft
 Drift width $w = 5.11$ ft
 Surcharge load: $pd = \gamma * h_d = 22.9$ psf
 Balanced Snow load: = 21.0 psf
 43.9 psf

Windward Snow Drifts 2 - Against walls, parapets, etc > 15'

Upwind fetch $l_u = 116.0$ ft
 Projection height $h = 4.0$ ft
 Snow density $g = 17.9$ pcf
 Balanced snow height $h_b = 1.17$ ft
 $h_c = 2.83$ ft
 $h_c/h_b > 0.2 = 2.4$ Therefore, design for drift
 Drift height (h_c) = 2.83 ft
 Drift width $w = 11.34$ ft
 Surcharge load: $pd = \gamma * h_d = 50.6$ psf



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JOB TITLE Waukesha Culvers

12 of 19

JOB NO. 2015-093

SHEET NO.

CALCULATED BY

DATE

2/4/16

CHECKED BY

DATE

Seismic Loads:

IBC 2009

Strength Level Forces

Occupancy Category : II
 Importance Factor (I) : 1.00
 Site Class : D

Ss (0.2 sec) = 11.20 %g
 S1 (1.0 sec) = 4.50 %g

Fa = 1.600
 Fv = 2.400

Sms = 0.179
 Sm1 = 0.108

S_{DS} = 0.119
 S_{D1} = 0.072

Design Category = A
 Design Category = B

Seismic Design Category = **B**

Number of Stories: 1

Structure Type: All other building systems

Horizontal Struct Irregularities: No plan Irregularity

Vertical Structural Irregularities: No vertical Irregularity

Flexible Diaphragms: Yes

Building System: **Bearing Wall Systems**Seismic resisting system: **Light frame (wood) walls with structural wood shear panels**System Structural Height Limit: **Height not limited**

Actual Structural Height (hn) = 12.3 ft

DESIGN COEFFICIENTS AND FACTORS

Response Modification Coefficient (R) = 6.5
 Over-Strength Factor (Ω_0) = 2.5
 Deflection Amplification Factor (Cd) = 4
 S_{DS} = 0.119
 S_{D1} = 0.072

Seismic Load Effect (E) = $\rho Q_E \pm 0.2S_{DS} D$ = $\rho Q_E \pm 0.024D$
 Special Seismic Load Effect (Em) = $\Omega_0 Q_E \pm 0.2S_{DS} D$ = $2.5 Q_E \pm 0.024D$

ρ = redundancy coefficient
 Q_E = horizontal seismic force
 D = dead load

PERMITTED ANALYTICAL PROCEDURES**Simplified Analysis** - Use Equivalent Lateral Force Analysis**Equivalent Lateral-Force Analysis** - Permitted

Building period coef. (C_T) = 0.020 $C_u = 1.70$
 Approx fundamental period (T_a) = $C_T h_n^x = 0.131$ sec $x = 0.75$ $T_{max} = C_u T_a = 0.223$
 User calculated fundamental period (T) = 0 sec Use T = 0.131
 Long Period Transition Period (TL) = ASCE7 map = 12
 Seismic response coef. (C_s) = $S_{DS}/R = 0.018$
 need not exceed $C_s = S_{d1} I / RT = 0.084$
 but not less than $C_s = 0.010$
 USE $C_s = 0.018$
 Design Base Shear V = 0.018W

Model & Seismic Response Analysis

- Permitted (see code for procedure)

ALLOWABLE STORY DRIFT

Structure Type: All other structures

Allowable story drift = 0.020hsx where hsx is the story height below level x

CODE SUMMARY

Code: Wisconsin Bldg Code

Live Loads:

Roof 0 to 200 sf: 20 psf
 200 to 600 sf: 24 - 0.02Area, but not less than 12 psf
 over 600 sf: 12 psf

Typical Floor 50 psf
 Partitions 15 psf
 Corridors above first floor 80 psf
 Lobbies & first floor corridors 100 psf
 Balconies (exterior) - same as occup 50 psf

Dead Loads:

Floor 100.0 psf
 Roof 20.0 psf

Wind Design Data:

Basic Wind Speed 90 mph
 Importance Factor 1.00
 Occupancy Category II
 Mean Roof Ht (h) 12.0 ft
 Exposure Category B
 Enclosure Classif. Enclosed Building
 Internal pressure Coef. +/-0.18
 Directionality (Kd) 0.85

Roof Snow Loads:

Design Uniform Roof Snow load = 21.0 psf
 Flat Roof Snow Load Pf = 21.0 psf
 Balanced Snow Load Ps = 21.0 psf
 Ground Snow Load Pg = 30.0 psf
 Importance Factor I = 1.00
 Snow Exposure Factor Ce = 1.00
 Thermal Factor Ct = 1.00
 Sloped-roof Factor Cs = 1.00

Earthquake Design Data:

Occupancy Category = II
 Importance Factor I = 1.00
 Mapped spectral response acceleratic Ss = 11.20 %g
 S1 = 4.50 %g
 Site Class = D
 Spectral Response Coef. Sds = 0.119
 Sd1 = 0.072
 Seismic Design Category = B
 Basic Structural System = Bearing Wall Systems
 Seismic Resisting System = Light frame (wood) walls with structural wood shear panels
 Design Base Shear V = 0.018W
 Seismic Response Coef. Cs = 0.018
 Response Modification Factor R = 6.5
 Analysis Procedure = Equivalent Lateral-Force Analysis

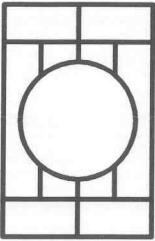
CODE SUMMARY- continued

Component and cladding wind pressures

Roof	Area	Surface Pressure (psf)		
		10 sf	50 sf	100 sf
Negative Zone 1		-14.6	-13.7	-13.3
Negative Zone 2		-24.4	-18.4	-15.8
Negative Zone 3		-24.4	-18.4	-15.8
Positive Zone 1		10.0	10.0	10.0
Positive Zones 2 & 3		13.3	12.0	11.4
Overhang Zone 1&2		-21.0	-20.1	-19.8
Overhang Zone 3		-21.0	-20.1	-19.8

Parapet	Area	Solid Parapet Pressure (psf)		
		10 sf	100 sf	500 sf
CASE A: Interior zone		33.3	22.7	21.4
Corner zone		33.3	22.7	21.4
CASE B: Interior zone		-23.3	-19.4	-16.7
Corner zone		-26.7	-20.8	-16.7

Wall	Area	Surface Pressure (psf)		
		10 sf	100 sf	500 sf
Negative Zone 4		-14.4	-12.5	-11.1
Negative Zone 5		-17.8	-13.9	-11.1
Positive Zone 4 & 5		13.3	11.4	10.0

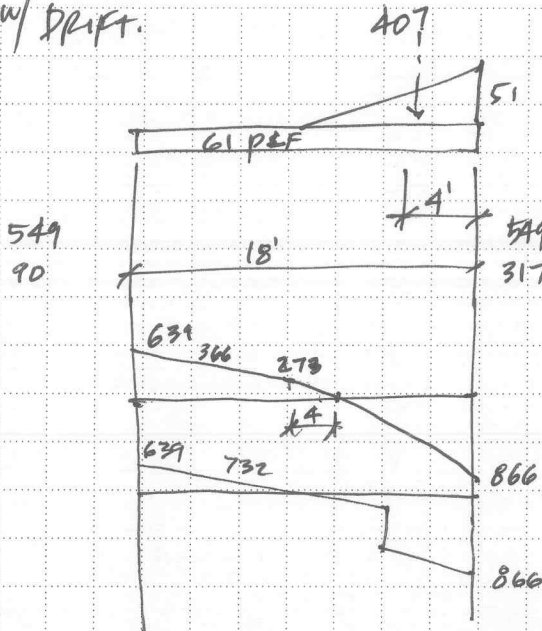


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 Sheet No. _____ of _____
 By _____ Date _____

Joists w/ Drift.



$$\text{DRIFT} = \frac{12}{2}(51) = 306 \text{ \#/ft.}$$

$$306(1.33) = 407 \text{ \# EA. JOIST.}$$

UNIFORM: 25 PSF DEAD. } 46 PSF
 21 PSF LIVE }

$$46(1.33) = 61 \text{ plf PER JOIST}$$

$$x = \frac{x}{639} = \frac{14'}{732} \quad x = 12.2'$$

$$M = 3.9 \text{ kft. APPROX.}$$

$$S_{980} = 43.5$$

$$M = 3.3 \text{ kft.}$$

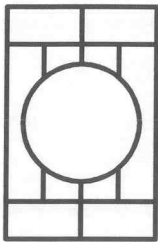
$$S_{980} = 36.7 \text{ NEG.}$$

Joists @ 12" o.c.

$$S = \frac{36.7}{1.33} = 27.6$$

$$V_d = \frac{866}{1.33} - \frac{46(11.25)}{12} = 608 \text{ \#}$$

$$f_r = \frac{608(3)}{2(16.875)} = 54 \text{ ok}$$



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Roof Framing

Rafters SPAN = 18'

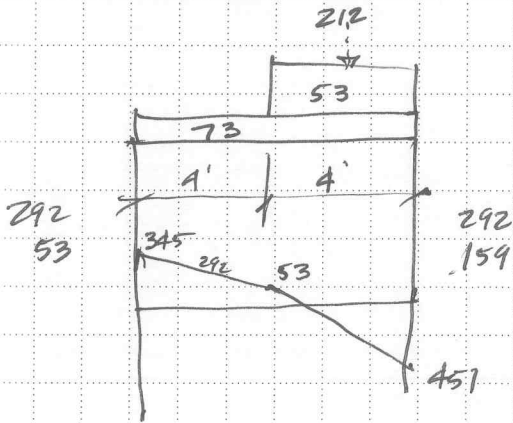
LOADS = DEAD 25 pcf
LIVE 30 pcf

55 pcf total

No 2 SPF 2x12's @ ~~16" o.c.~~ 19' 2" Available
12" o.c. DUE TO DRIFT.

RTU - 7'x4' BOB #s - 30 pcf AVE
Joists @ 16" o.c.

USE 40 pcf 40(1.33) = 53 pcf
55(1.33) = 73 pcf



$$\frac{x}{451} = \frac{4}{504} \quad K = 3.58'$$

$$M = 0.807 \text{ kft}$$

$$S_{980} = 8.9$$

2x12 OK

HEADER

SPAN = 21'

LOAD = 340 pcf + 495 = 835 pcf

$$V = 8768$$

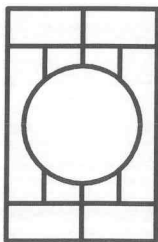
$$M = 46.0 \text{ kft}$$

$$S_{2600} = 193$$

try (3) 16" LVL's

$$\Delta = \frac{5(0.835)(21)^4}{384(1800)(1785)} = 1.14'' \approx \frac{1}{221}$$

USE (4) 16" LVL's



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Header Along Exist

$$\text{SPAN} = 21'$$

$$\text{LOAD} = 345 \text{ psf}$$

$$V = 3623$$

$$M = 19.0$$

$$S_{2600} = 79.8$$

try (2) 16" LVLs

$$\Delta = \frac{5(.345)(21)^4}{384(1800)(1190)} = \frac{1728}{357} = 0.7" \rightarrow \text{ok.}$$

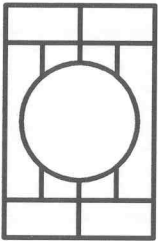
Typ Footings

$$\text{LOAD} = 9(55) + 16(20) = 815 \text{ psf}$$

16" WIDE FTG OK w/ 1500 psf SOIL.

$$866 + 320 = 1186$$

$$\frac{1186}{1500} = 0.8' \rightarrow 16" \text{ FTG OK}$$

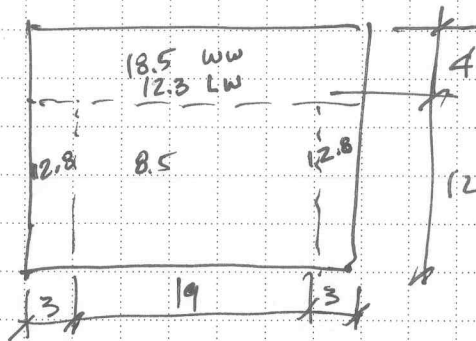


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WIND.



WIND

$$(2)(3') \left(\frac{12.8}{2} \right) \left(\frac{12}{2} \right) + 19' \left(\frac{12}{2} \right) (8.5) = 1430$$

PANES

$$25' (4') (18.5 \text{ psp}) + 25' (4') (12.3 \text{ psp}) = 3080$$

$$\text{TOTAL} = 4510$$

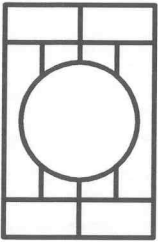
$$\frac{4510}{2} = 2255 \# \text{ EA. WIND}$$

Roof Deck

$$\frac{2255}{25} = 90.2 \text{ pcf}$$

$$\frac{90.2}{0.92 \text{ SPF}} (2 \text{ ASD}) = 196 \text{ pcf}$$

UNBLOCKED DIAPHRAGM - 19/32 Roof Sheathing w/ 2" Nominal Framing
10d Nails @ 6" o.c. @ All Panel Edges & Boundaries



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WALL SHEATHING

$$\text{MAX LOAD} = 2255$$

$$\text{Worst CASE} - \frac{2255}{12} = 188 \text{ PLF}$$

$$\frac{188}{0.92 \text{ SPF}} (2 \text{ ASD}) = 409 \text{ PLF TARGET.}$$

15/32 SHEATHING w/ 10d NAILS @ 6" o.c. @ EDGES

USE 5/8" ϕ ANCHOR BOLTS @ 48" o.c. TYPICAL

**2015-093 Culvers
HVAC Load Analysis**

for

Culver's Of Waukesha, WI



CHVAC COMMERCIAL
HVAC LOADS



Prepared By:

Ollmann Ernest Martin Architects

February 2016



Air Handler #1 - RTU-3 - Summary Loads

Rm No	Description Room Peak Time	Area People Volume	Htg.Loss Htg.CFM CFM/Sqft	Sen.Gain Clg.CFM CFM/Sqft	Lat.Gain S.Exh W.Exh	Htg.O.A. Req.CFM Act.CFM	Clg.O.A. Req.CFM Act.CFM
1	Prep 4pm June	63 1 819	166 7 0.11	4,635 207 3.29	200 0 0	Direct 7 1	Direct 7 21
2	Storage 4pm June	553 0 7,189	13,027 541 0.98	8,779 392 0.71	2,852 0 0	Direct 58 77	Direct 58 40
3	Office 4pm June	153 1 1,989	404 17 0.11	4,361 195 1.27	155 0 0	Direct 16 2	Direct 16 20
Room Peak Totals:		769	13,598	17,774	3,207		
Total Rooms: 3		2	565	794	0	80	80
Unique Rooms: 3		9,997	0.73	1.03	0	80	80



Air Handler #1 - RTU-3 - Total Load Summary

Air Handler Description: RTU-3 Constant Volume - Sum of Peaks
 Sensible Heat Ratio: 0.85 --- This system occurs 1 time(s) in the building. ---

Air System Peak Time: 4pm in June.
 Outdoor Conditions: Clg: 89° DB, 75° WB, 110.00 grains, Htg: -5° DB
 Indoor Conditions: Clg: 75° DB, 50% RH, Htg: 72° DB

Summer: Ventilation controls outside air, ---- Winter: Ventilation controls outside air.

Room Space sensible loss:	5,537 Btuh	
Infiltration sensible loss:	8,061 Btuh	100 CFM
Outside Air sensible loss:	6,449 Btuh	80 CFM
Supply Duct sensible loss:	0 Btuh	
Return Duct sensible loss:	0 Btuh	
Return Plenum sensible loss:	0 Btuh	
Total System sensible loss:		20,047 Btuh

Heating Supply Air: $13,598 / (.969 \times 1.08 \times 23) =$	565 CFM
Winter Vent Outside Air (14.2% of supply) =	80 CFM

Room space sensible gain:	16,277 Btuh	
Infiltration sensible gain:	1,497 Btuh	
Draw-thru fan sensible gain:	0 Btuh	
Supply duct sensible gain:	0 Btuh	
Reserve sensible gain:	0 Btuh	
Total sensible gain on supply side of coil:		17,774 Btuh

Cooling Supply Air: $17,774 / (.969 \times 1.1 \times 21) =$	794 CFM
Summer Vent Outside Air (10.1% of supply) =	80 CFM

Return duct sensible gain:	0 Btuh	
Return plenum sensible gain:	0 Btuh	
Outside air sensible gain:	1,194 Btuh	80 CFM
Blow-thru fan sensible gain:	0 Btuh	
Total sensible gain on return side of coil:		1,194 Btuh
Total sensible gain on air handling system:		18,969 Btuh

Room space latent gain:	355 Btuh	
Infiltration latent gain:	2,852 Btuh	
Outside air latent gain:	2,417 Btuh	
Total latent gain on air handling system:		5,625 Btuh
Total system sensible and latent gain:		24,593 Btuh

Check Figures

Total Air Handler Supply Air (based on a 21° TD):	794 CFM
Total Air Handler Vent. Air (10.08% of Supply):	80 CFM
Total Conditioned Air Space:	769 Sq.ft
Supply Air Per Unit Area:	1.0323 CFM/Sq.ft
Area Per Cooling Capacity:	375.2 Sq.ft/Ton
Cooling Capacity Per Area:	0.0027 Tons/Sq.ft
Heating Capacity Per Area:	26.07 Btuh/Sq.ft
Total Heating Required With Outside Air:	20,047 Btuh
Total Cooling Required With Outside Air:	2.05 Tons

DIVISION 23 – HEATING, VENTILATING AND AIR CONDITIONING

SECTION 233113 - DUCTWORK

1. GENERAL

- A. It must be understood that the heating, ventilating and air conditioning drawings and details are diagrammatic and are intended to show the intent of the specifications. The contractor shall make full allowance in his proposal to cover such contingencies as actual length and routing, proper equipment locations and connections, etc. He shall take all necessary measurements and accept responsibility for their accuracy. Coordinate with the General Contractor for exact location of walls, beams, shafts, etc. Do not scale drawings. Coordinate with equipment suppliers for connections made to equipment furnished by others.
- B. Make Engineer/Architect aware of any discrepancies between drawings and/or existing conditions. The Engineer/Architect reserves the right to eliminate discrepancies through minor changes in work at no change in contract cost.

2. MATERIALS

- A. Sheet Metal: Furnish, install, fit and secure in place all supply, return, exhaust and vent air ducts, risers, branches, etc., as shown and detailed on plans, built of galvanized iron as hereinafter specified.

- 1. Sheet metal work shall be constructed according to practices recommended in the "HVAC Duct Construction Standards, 1st edition 1985" as published by SMACNA, and hereinafter specified. All duct dimensions noted on the drawings are finished inside dimensions. Sheet metal used shall not be lighter than the following:

<u>Rectangular Ducts</u>	<u>Galvanized Sheet Metal Gage</u>	<u>Aluminum Alloy</u>
Up thru 12"	26	.020
13" - 30"	24	.025
31" - 54"	22	.032
55" - 84"	20	.040

<u>Round Ducts</u>	<u>Galvanized Sheet Metal Gage</u>
Up thru 13"	26
14" - 22"	24

- 2. Install ducts, risers, etc., as indicated on the drawings, making necessary changes in cross section, offsets, etc., whether or not same is specifically indicated. If ducts cannot be run as shown on the drawings, install ducts between required point, subject to the approval of the Engineer/Architect without additional cost to the Owner.
- 3. At all outlets and inlets in rooms, flange ducts for attachment of grilles. Install grilles according to manufacturer's recommendations.
- 4. Sheet metal work throughout shall be assembled and erected in such a manner that no vibration will occur and no noise be transmitted by the moving air.
- 5. All duct turns shall have either an inside radius equal to the duct width or be a miter turn with turning vanes.
- 6. All supply take-offs shall be bellmouth or conical type. Square/rectangular take-off fittings shall have 45 degree leading edge for 4" maximum depth. No air turns allowed.

7. Duct Sealant: Non-hardening, non-migrating mastic or liquid elastic sealant gaskets and tapes, except as noted.
- B. Ductwork Pressure - Velocity Classification: Low Pressure, +2" W.G., 2500 FPM maximum, Class "B" seal. All grease ducts shall have welded liquid tight seal.
- C. All duct turns shall have either an inside radius equal to the duct width or a miter turn with turning vanes. Vanes shall be double wall air foil type.
- D. Round take-off fittings shall be bellmouth or conical. Rectangular or square take-off fittings shall have a 45 degree lead edge with 4" minimum depth.
- E. Volume Dampers: Furnish and install in branches of supply air and exhaust ducts. Substantial volume dampers to be fitted with quadrant locking devices for adjusting the air delivery. Damper blades shall not exceed 6" width.
- F. Access Panels: Install access panels with latches and gaskets in ducts at automatic dampers, coils, fire dampers, and other duct mounted equipment. Panels in insulated ducts must be internally insulated.
- G. Backdraft Dampers: Provide backdraft dampers at discharge grille of louvers unless motor operated dampers are specified with these units. Entire perimeter of blade shall be lined with neoprene or vinyl seals to prevent clatter. Damper blades shall be tight closing.
- H. Flexible Duct:
1. Provide factory fabricated insulated low pressure flexible duct with zinc-coated spring steel helix, 1" thick fiberglass insulation sheathed in a seamless vapor barrier (RFK) jacket. Maximum length 8'.
 2. Composite assembly, including insulation and vapor barrier, meeting Class 1 requirements of flame spread rating of 25 or less and smoke developed rating of 50 or less as set forth in NFPA Bulletin 90-A, and bearing the UL label as an air duct.
 3. Flexible ductwork shall meet ductwork pressure classification.
- I. Insulation:
1. Materials:
Materials shall conform to NFPA bulletin 90-A as determined by U.L. method NFPA 225 - ASTM E84, complying with applicable codes with a flame spread rating of 25 or less and a smoke developed rating of 50 or less.
 2. External Ductwork Insulation:
 - a. Concealed ductwork (horizontal): Wrap ductwork with flexible type fiberglass insulation, operating temperature range 40 to 250 degrees F., K=0.25, 1-1/2 PCF density, vapor permeability less than 0.02 perms, installed R of 4.5. Johns Manville Microlite EQ Type 100 duct wrap insulation.
 - b. Concealed ductwork (vertical): Rigid fiberglass duct liner, operating temperature to 250 degrees F., installed R of 6.3. Johns Manville Permacote Linacoustic R-300.
 - c. Application Schedule:

<u>Application Schedule</u>	<u>Thickness</u>
Exhaust air ducts	1-1/2"
Fresh air ducts	1-1/2"

Supply air ducts

1-1/2"

J. Kitchen Hood Exhaust Ductwork

1. Welded Steel

- a. Duct to be constructed with 16 gauge welded black iron.
- b. All external joints, seams and duct connections to the hood shall be welded liquid tight conforming to NFPA 90.
- c. Insulation: 3M "Fire Barrier Duct Wrap 615+".

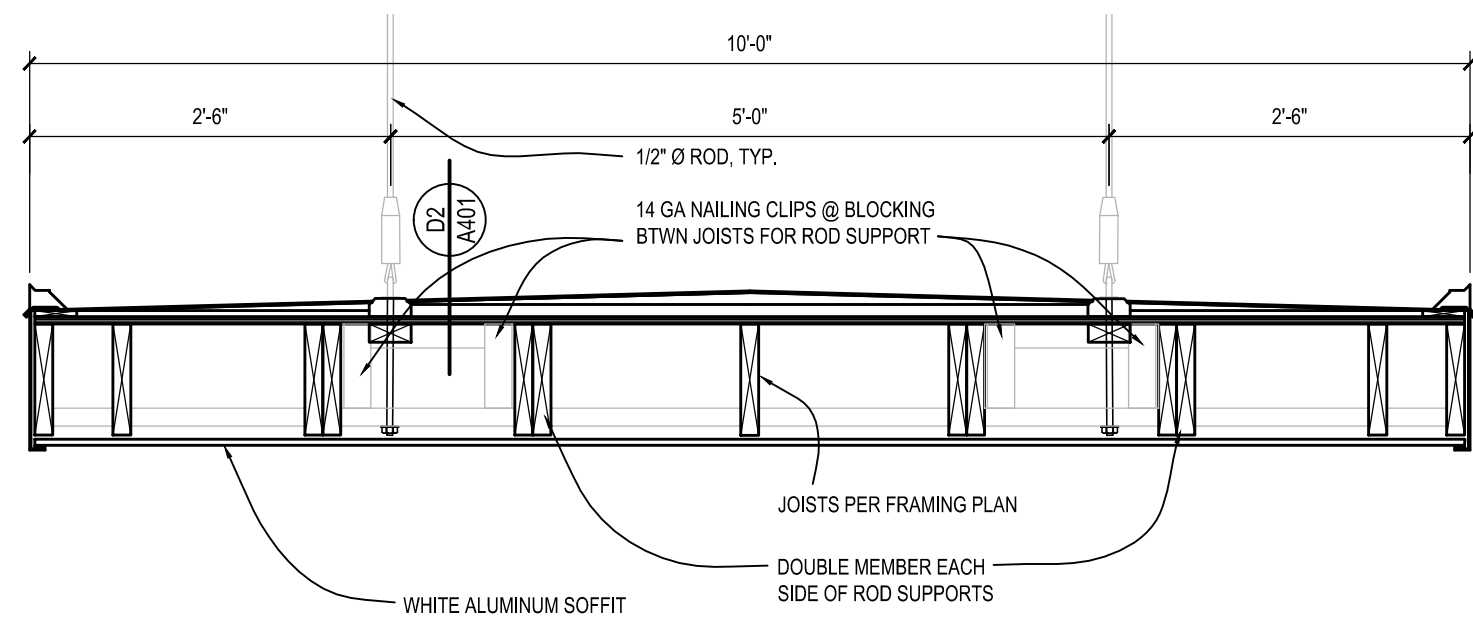
K. Air Outlets and Inlets:

1. Furnish grilles, registers, diffusers and louvers in the sizes, type and capacity as shown on the drawings by the selected manufacturer or approved equal.
2. Grilles, registers, diffusers shall be suitable and compatible with ceiling construction in which they are installed. Check architectural schedules for ceiling construction. Coordinate locations with ceiling system and lighting fixtures.

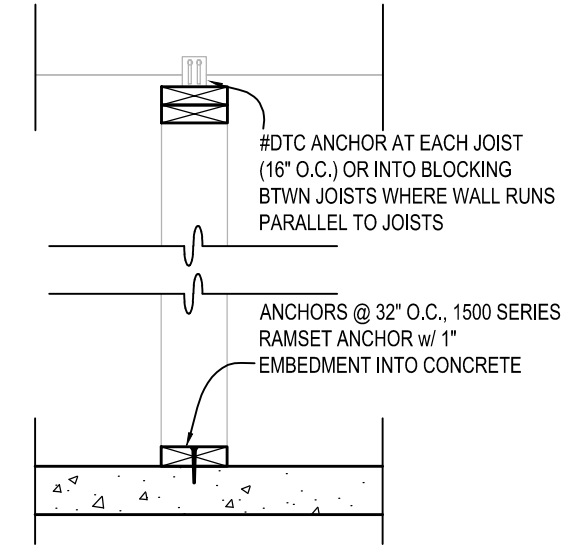
3. EXECUTION

- WI item:
2-19-2016
- A. Ducts shall be constructed, supported and installed in accordance with the latest standards of SMACNA. Install all turning vanes, access doors, extractors, and accessories as indicated or specified herein. Ductwork shall be sealed at all joints, transverse and longitudinal seams and connections in ductwork using listed products as referenced in the code. The referenced ductwork includes all supply, exhaust and return ducts.
 - B. Provide all necessary personnel, equipment, and services and perform all tests necessary to demonstrate the integrity of the completed installation to the approval of the Owner and Engineer/Architect. The air and hydronic systems shall be tested, adjusted and balanced in accordance with the latest edition of the Associated Air Balance Council (AABC) Procedural Standards, NEBB or equivalent.

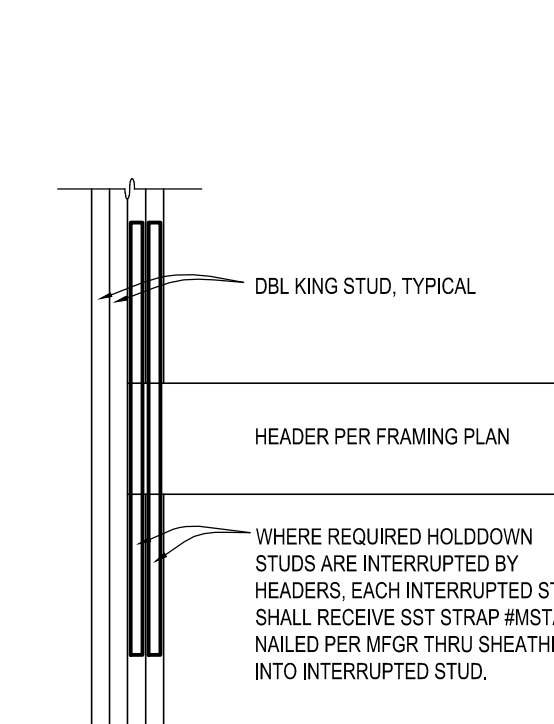
END OF SECTION 233113



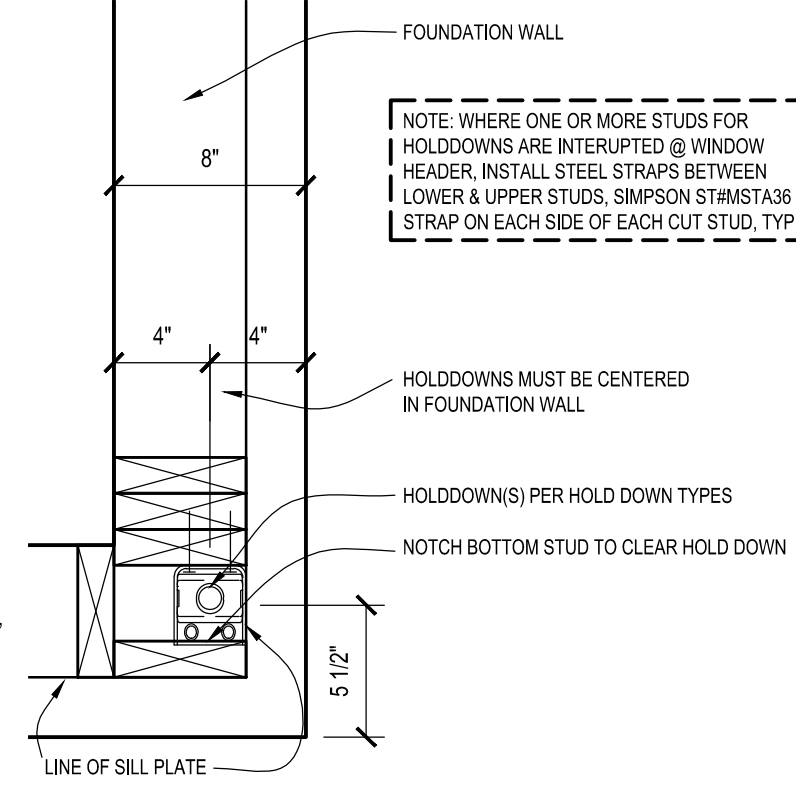
A2 CANOPY SECTION
SCALE : 3/4" = 1'-0"



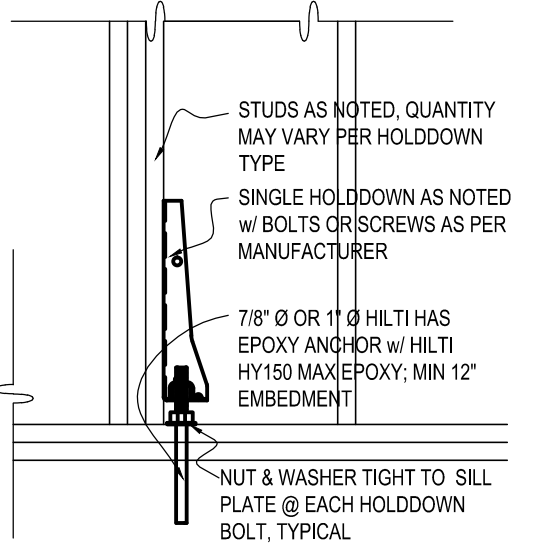
B1 INT. WALL ANCHOR
SCALE : 3/4" = 1'-0"



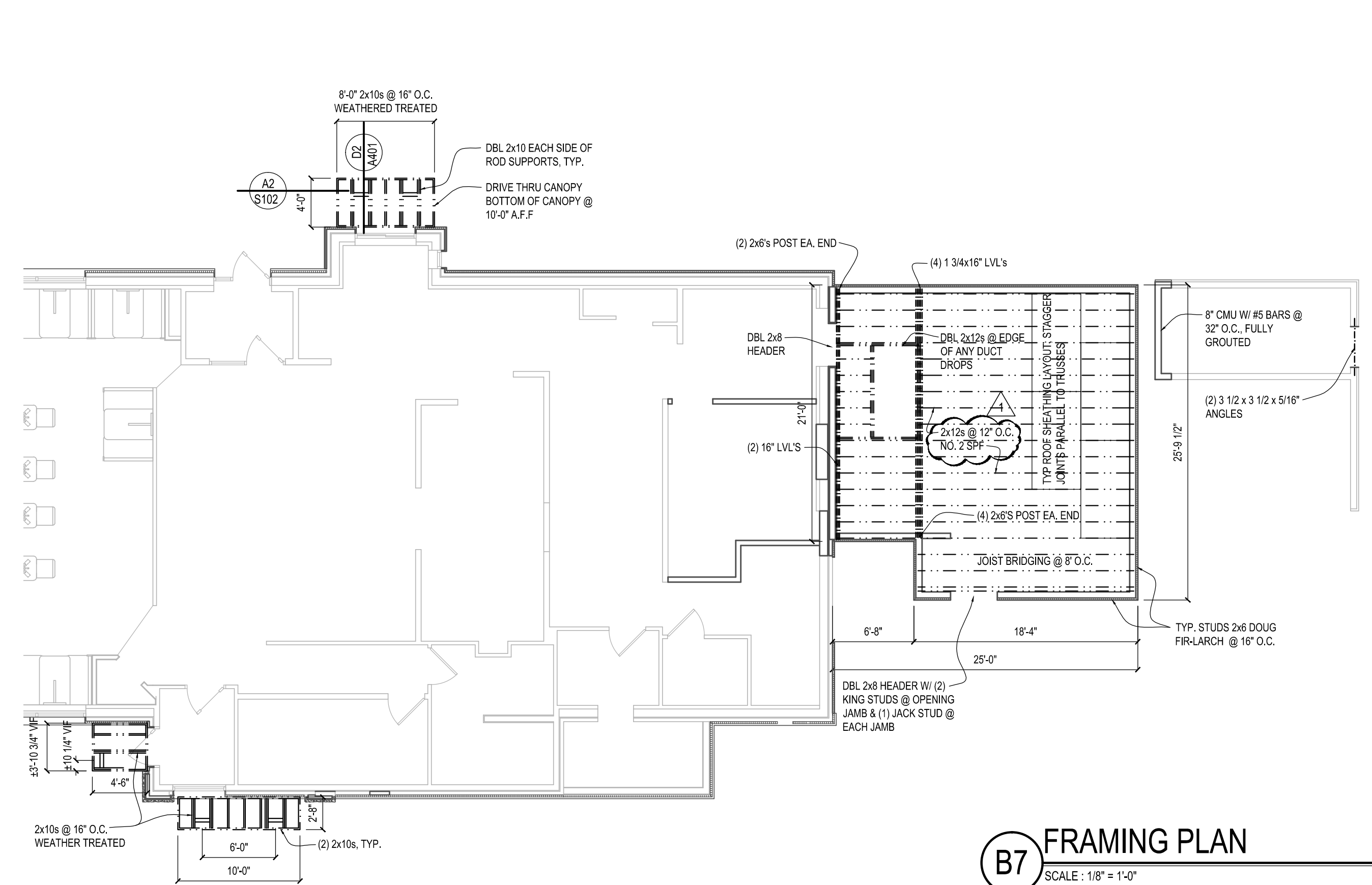
B3 STRAP DETAIL
SCALE : 3/4" = 1'-0"



B4 CORNER HOLDDOWN
SCALE : 1 1/2" = 1'-0"



C3 HOLDDOWN
SCALE : 3/4" = 1'-0"



B7 FRAMING PLAN
SCALE : 1/8" = 1'-0"

- GENERAL SHEATHING REQUIREMENTS**
- INSTALL SHEATHING CONTINUOUS OVER ENTIRE WALL.
 - REFER TO BUILDING PLANS, SECTIONS, AND ELEVATIONS FOR DIMENSIONS.
 - SEE FLOOR PLAN FOR EXACT LOCATIONS OF WINDOW AND DOOR OPENINGS.
 - COORDINATE WITH WALL SECTIONS SHOWN ON SHEET A401
 - ALL SHEATHING SHALL BE INSTALLED W/ 1/8" GAP @ ALL PANEL EDGES.
- GENERAL STRUCTURAL NOTES**
- CARPENTRY - SEE FRAMING PLAN THIS SHEET
- FLASH ALL HEADS OF WINDOWS AND DOORS.
 - ALL STRUCTURAL LUMBER SHALL BE AS SPECIFIED IN PROJECT MANUAL AND BELOW UNLESS OTHERWISE NOTED HEREIN.
 - LAMINATED VENEER LUMBER SHALL HAVE MINIMUM $F_b = 2600$ PSI & $E = 1800$ KSI
 - STUDS: #2 DOUG FIR LARCH U.N.O.
 - HEADERS, JOISTS, ROUGH FRAMES, FRAMING SILLS, etc.: #2 SPF OR #2 HEM FIR
 - WALERS @ MEMBRANE ROOFING: #2 SPF OR #2 HEM FIR
 - WOOD FLOORING & GROUNDS: #2 WHITE PINE
 - PLYWOOD, CONFORMING TO PS 1, APA PRP-108, INCLUDING GRADE STAMPING
- ROOF SHEATHING: C-D GRADE w/ EXTERIOR GLUE (CDX) SHEATHING OVER STUDS. EXTERIOR TYPE, C-C GRADE. INTERIOR WALL SHEATHING: EXTERIOR TYPE, B-C GRADE.
- OSB: CONFORMING TO DOC PS 2, EXPOSURE 1 GRADE
- WALL SHEATHING NOTES:**
- EXTERIOR SHEATHING SHALL BE 1/2" O.S.B. SHEATHING WITH 10d NAILS @ 6" O.C. @ EDGES & 12" O.C. IN PANEL FIELD.
 - JOINTS IN SHEATHING SHALL HAVE 2X BLOCKING BETWEEN STUDS
- ROOF SHEATHING NOTES:**
- NEW ROOF SHEATHING SHALL BE 1/2" APA RATED OSB OR CDX PLYWD. INSTALL 10d NAILS AT:
- 6" O.C. AT ROOF PERIMETER & AT EXISTING
 - 6" O.C. AT OTHER PANEL EDGES.
 - 12" O.C. IN PANEL FIELD.

SEE GENERAL STRUCT. NOTES & DESIGN LOADS ON SHEET S101

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CULVER'S RESTAURANT RE-IMAGE 840 W Sunset Drive Waukesha, WI 53189 County of WAUKESHA
 Culver Franchising System, Inc. 1240 Water Street Prairie du Sac, WI 53578 608-663-1980
OWNER: BERES FOODS, LLC 1650 E Main St. Waukesha, WI 53186 Gary Beres 414-940-7533 Jim Beres 262-443-1989
OLLMANN ERNEST MARTIN ARCHITECTS 5109 South State Street Belleville Illinois 61008 815-544-7790 Phone 815-544-7792 Fax
FRAMING PLAN & DETAILS
Date: 2-5-2016 Revision: 2/19/2016 (W) comments
2015-093
S102

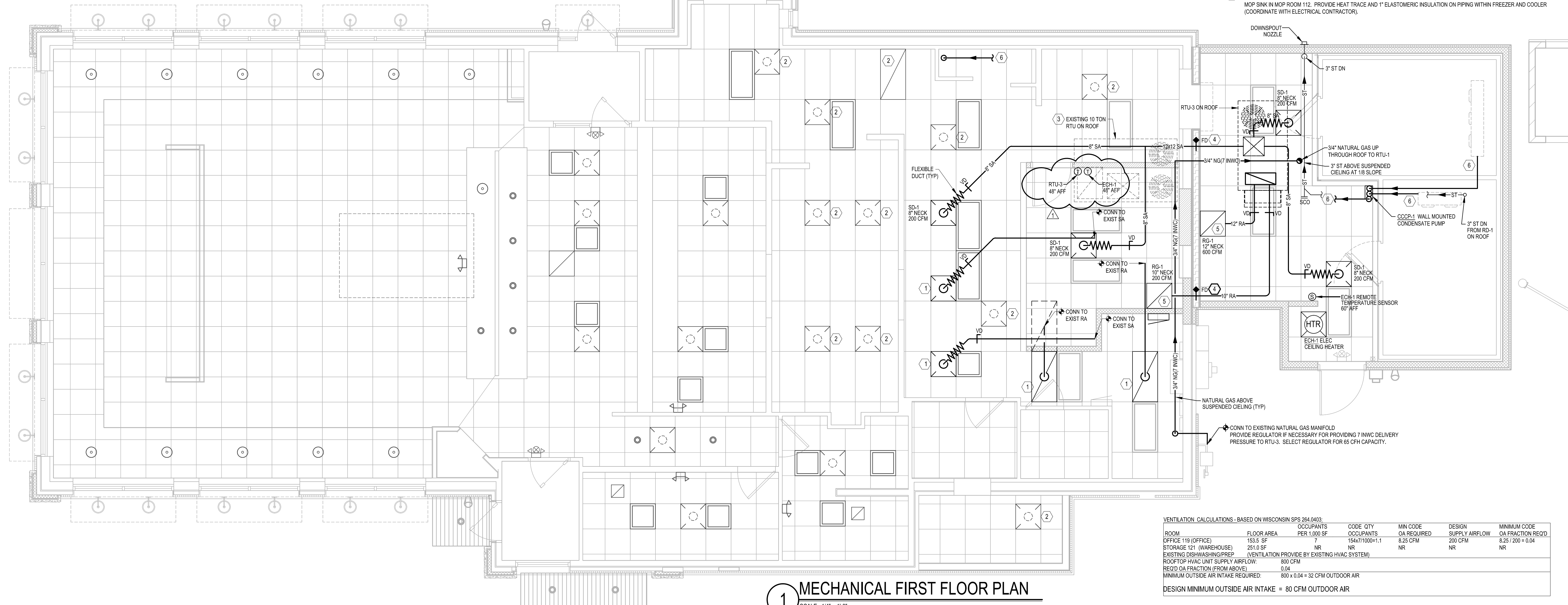
GENERAL NOTES:

- INDICATED DUCT SIZES FOR LINED DUCT ARE INSIDE DIMENSION. CLEAR OF DUCT LINER.
- PROVIDE DUCT LINER FOR ALL VERTICAL RECTANGULAR SUPPLY AND RETURN DUCT DROPS FROM RTU. PROVIDE DUCT LINER WITH MINIMUM 1" THICKNESS AND MINIMUM INSTALLED R-VALUE 4.0. INSTALL AS INDICATED, IN COMPLIANCE WITH NAIMA AND SMACNA GUIDES, AND IN COMPLIANCE WITH BUILDING CODES.
- EXISTING HVAC SYSTEMS AS SHOWN MAY BE INCOMPLETE OR INCORRECT. FIELD VERIFY EXISTING HVAC CONFIGURATIONS AND MODIFY WORK SCOPE AS REQUIRED.
- TEST, ADJUST, AND BALANCE HVAC SYSTEM RTU-3 AS INDICATED AND IN COMPLIANCE WITH BUILDING CODES.
- TEST, ADJUST, BALANCE AND RECORD AIRFLOW RATES FOR ALL SUPPLY AND RETURN DIFFUSERS, REGISTERS, AND GRILLES CONNECTED TO THE EXISTING 10 TON LENNOX ROOFTOP HVAC UNIT. INCLUDE OUTLETS AND INLETS THAT ARE NOT SHOWN, IF ANY.
- DO NOT ALTER EXISTING DUCTWORK, AIR INLETS, AIR OUTLETS, OR AIR BALANCE OF 15 TON TRANE ROOFTOP UNIT SYSTEM.
- PROVIDE TURNING VANES IN MITERED ELBOWS.
- INSTALL THERMOSTATS AT 4'-0" AFF. INSTALL REMOTE TEMPERATURE SENSORS AT 5'-0" AFF.
- VERIFY LOCATION OF ROOFTOP UNIT AND ELECTRIC CEILING HEATER THERMOSTATS AND SENSORS WITH OWNER.

- SET THERMOSTATS AT 70 DEGREE F FOR HEATING AND 76 DEGREE F FOR COOLING.
- PROVIDE BLACK STEEL GAS PIPING SYSTEM COMPLYING WITH APPLICABLE FUEL GAS CODE AND LOCAL CODES. PAINT OUTDOOR NATURAL GAS PIPING YELLOW. GAS PIPING INSTALLATION SHALL COMPLY WITH NFPA 44-2009 NATIONAL FUEL GAS CODE.
- REFER TO ARCHITECTURAL DRAWINGS FOR EXACT LOCATIONS OF EQUIPMENT AND ITEMS INSTALLED IN CEILING.
- INSTALL RTU-1 CONDENSATE TRAP FURNISHED BY RTU MANUFACTURER. ARRANGE TRAP TO DISCHARGE CONDENSATE ON ROOF.
- DO NOT LOCATE PIPING OR DUCTWORK OVER ELECTRICAL PANELS.
- COORDINATE ALL WORK WITH WORK OF OTHER TRADES AND EXISTING CONDITIONS AS REQUIRED TO PROPERLY INSTALL ALL SYSTEMS AS INTENDED, WITHIN THE CONFINES OF THE SPACES AVAILABLE, AND WITHOUT INTERFERENCES.
- PERFORM ALL WORK INDICATED AND/OR AS REQUIRED FOR THE PROPER INSTALLATION AND OPERATION OF THE MECHANICAL SYSTEMS. ALL SYSTEM COMPONENTS SHALL BE INSTALLED IN COMPLIANCE WITH MANUFACTURER'S INSTRUCTIONS AND APPLICABLE MECHANICAL AND ENERGY CODES.
- INSTALL ALL DUCT, PIPE, ETC AS HIGH AS POSSIBLE UNLESS NOTED OTHERWISE.

KEYED NOTES:

- RELOCATED EXISTING DIFFUSER. CONNECT TO SAME SYSTEM WITH SAME DUCT SIZE, MATERIAL, AND INSULATION AS BEFORE RELOCATION. TEST, ADJUST, AND BALANCE TO SAME AIRFLOW RATE AS BEFORE START OF WORK.
- EXISTING DIFFUSER, REGISTER, OR GRILLE. TEST, ADJUST, AND BALANCE TO SAME AIRFLOW RATE AS BEFORE START OF WORK.
- EXISTING ROOFTOP UNIT ON ROOF. TEST, ADJUST, AND BALANCE SUPPLY, RETURN, RELIEF, AND OUTSIDE AIR INTAKE MAXIMUM AND MINIMUM AIRFLOW RATES TO SAME AS BEFORE START OF WORK.
- 1-1/2 HR DYNAMIC FIRE DAMPER AS REQUIRED BY CODE FOR 2 HOUR FIRE RESISTANCE RATED WALL. INSTALL IN COMPLIANCE WITH DAMPER MANUFACTURER'S INSTRUCTIONS, UL LISTING, AND APPLICABLE CODES. PROVIDE INSULATED DUCT ACCESS DOORS LARGE ENOUGH TO PERMIT INSPECTION AND MAINTENANCE. ACCESS POINTS SHALL BE PERMANENTLY IDENTIFIED ON THE EXTERIOR BY A LABEL HAVING LETTERS A MINIMUM OF 0.5 INCH HEIGHT READING "FIRE DAMPER".
- PROVIDE 24"x24" PLENUM BOX; 6" TALL FOR UNITS WITH TOP DUCT CONNECTIONS, 20 INCH TALL FOR UNITS WITH SIDE DUCT CONNECTIONS.
- COPPER EVAPORATOR COIL DRAIN PIPING FROM COOLING COIL DRAIN PANS TO WALL MOUNTED CONDENSATE PUMP CCCR-1. PROVIDE 3/4" PVC PIPING FROM PUMP DISCHARGE ABOVE SUSPENDED CEILING, TO OPEN SIGHT TERMINATION ABOVE FLOOD RIM OF MCP SINK IN MCP ROOM 112. PROVIDE HEAT TRACE AND 1" ELASTOMERIC INSULATION ON PIPING WITHIN FREEZER AND COOLER (COORDINATE WITH ELECTRICAL CONTRACTOR).

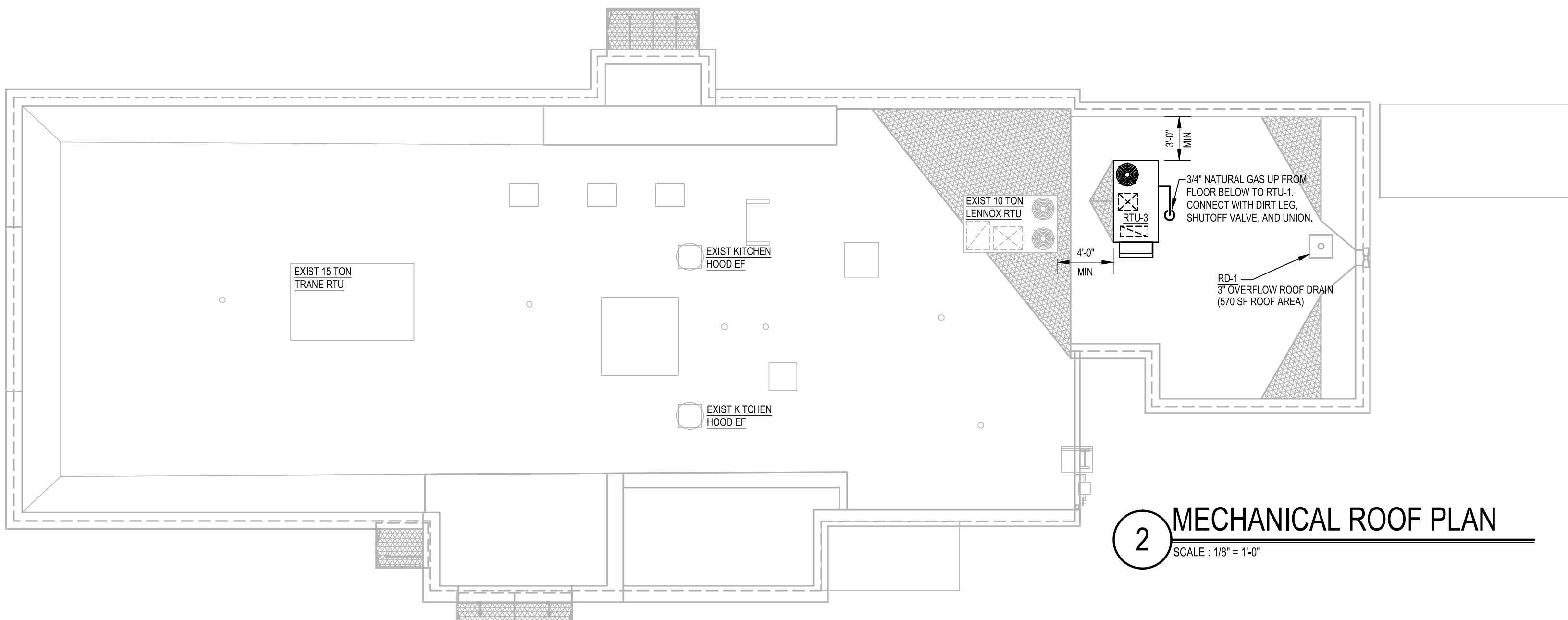


1 MECHANICAL FIRST FLOOR PLAN
SCALE: 1/4" = 1'-0"

VENTILATION CALCULATIONS - BASED ON WISCONSIN SPS 264.0403

ROOM	FLOOR AREA	OCCUPANTS PER 1,000 SF	CODE QTY OCCUPANTS	MIN CODE OA REQUIRED	DESIGN SUPPLY AIRFLOW	MINIMUM CODE OA FRACTION REQ'D
OFFICE 119 (OFFICE)	153.5 SF	7	154x7/1000=1.1	8.25 CFM	200 CFM	8.25/200 = 0.04
STORAGE 121 (WAREHOUSE)	251.0 SF	NR	NR	NR	NR	NR
EXISTING DISHWASHING/PREP	(VENTILATION PROVIDED BY EXISTING HVAC SYSTEM)					
ROOFTOP HVAC UNIT SUPPLY AIRFLOW:	800 CFM					
REQ'D OA FRACTION (FROM ABOVE):	0.04					
MINIMUM OUTSIDE AIR INTAKE REQUIRED:	800 x 0.04 = 32 CFM OUTDOOR AIR					

DESIGN MINIMUM OUTSIDE AIR INTAKE = 80 CFM OUTDOOR AIR



2 MECHANICAL ROOF PLAN
SCALE: 1/8" = 1'-0"

DIFFUSER, REGISTER, AND GRILLE SCHEDULE

TAG	SERVICE	TYPE	MATERIAL	THROW	FACE	NECK	MOUNTING	MANUFACTURER/MODEL	Notes
SD-1	SUPPLY	SQUARE CONCENTRIC CONE	STEEL	4-WAY	24X24	SEE PLAN	LAY-IN	CARNES SFTB24	1, 2
RG-1	RETURN	GRID CORE ('EGGCRATE')	ALUMINUM	N/A	24X24	SEE PLAN	LAY-IN	CARNES RAPAH	2

DIFFUSER NOTES:
1. PROVIDE W/ ADJUSTABLE OPPOSED BLADE DAMPER
2. PROVIDE WITH WHITE FINISH UNLESS NOTED OTHERWISE.

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CULVER'S RESTAURANT RE-IMAGE
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MECHANICAL PLANS

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