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Project No. \$230787

By SUL

Date 2/23/26

Page of

	144 ~ 10 PSF (34"+ WE) = for 1/4"	R3B OR THO HOLLOWBUR FGC = GC
	- 5-4, 14.0 0 0 00000	MAX Sunce cow Car's = 19K
18"	wr=1000 4/4.	60 SW19-5 = 20 KIRS
⁸ 1 1	USA 1500 4/FT.	$\frac{49}{3} = 16.33$
<u> </u>	wow/BKIA.	60 (Se x)=16.33
	10" 0c 25(15)+14 = 51.5 K	x = /5.8°
	KMO 1	A-15.15
	der 182 for Sphering	3.1 am order 3.5:12
1 = USE (3)	#7 148	
As = 1-80	100(B(18x51)=1.75	
T= 1001	(105 (-05(4)(10) = 1-76"	
	(B-12)(9)(12) = 30/K-Pr.	
1.8	(e) 6 8 = 301 L= 41	
(18 * 48)	(2) \(\int 3000 \left(.75 \right) = 71 K \(\int 2 \right) \) \(I = \frac{1}{6} \text{B} \left(\frac{1}{2} \right) \) \(L = 7 \text{B} \)	
·	50/4 = 37.5	

Nucor Building Systems

Frame: 1

Job #:

Ву:

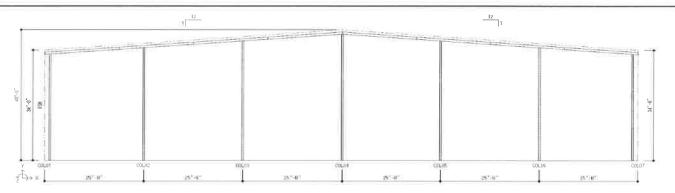
Job Name: Central Disposal

Page: 2

Date: 02/08/2024

Control #: P202402081520

Building: Transfer station *** Design Summary - Frame Reactions by Load Case ***



Member	X (kips	Y (kips	Z (kips	Member	X (kips	Y (kips	Z (kips
LOAD CASE 1 - DEAD		T	1	LOAD CASE 7 - WIND CASE 2 TO RIGHT			1
COL01	0	1	0	COL01	0	-5	0
COL02	0	2	0	COL02	0	-12	0
COL03	0	2	0	COL03	0	-13	0
COL04	0	2	0	COL04	0	-8	0
COL05	0	2	0	COL05	0	-9	0
COL06	0	2	0	COL06	0	-9	0
COL07	0	1	0	COL07	0	-4	0
LOAD CASE 2 - COLLATERAL				LOAD CASE 8 - WIND CASE 2 TO LET			
COL01	0	1	0	COL01	0	-4	0
COL02	0	2	0	COLO2 REV	0	-9	0
COL03	0	2	0	CD108	0	-9	0
COL04	0	1	PILOS	CQ104 /	0	±7	0
COL05	0	200	1101	COL05	0	-13	0
COL06	0	1210	0	COL06	0	-12	0
COL07	0	1 1	0	COL07	0	-6	0
LOAD CASE 3 - ROOF LIVE				LOAD CASE 9 - LONG. WIND 1 TO BACK		İ	
COL01	0	3	0	COL01	0	-5	-5
COL02	0	8	0	COL02	0	-13	-9
COL03	0	8	0	COL03	0	-13	-10
COL04	0	6	0	COL04	0	-9	-11
COL05	0	8	0	COL05	0	-13	-10
COL06	0	8	0	COL06	0	-13	-9
COL07	0	3	0	COL07	0	-5	-5
LOAD CASE 4 - SNOW				LOAD CASE 10 - LONG. WIND 1 TO FRONT			
COL01	0	4	0	COL01	0	-5	5
COL02	0	9	0	COL02	0	-13	10
COL03	0	10	0	COL03	0	-13	11
COL04	0	7	0	COL04	0	-9	11
COL05	0	10	0	COL05	0	-13	11
COL06	0	9	0	COL06	0	-13	10
COL07	0	4	0	COL07	0	-5	5
LOAD CASE 5 - WIND CASE 1 TO RIGHT				LOAD CASE 11 - SEISMIC TO RIGHT			- 1
COL01	0	-2	0	COL01	0	0	0
COL02	0	-4	0	COL02	0	0	0
COL03	0	-4	0	COL03	0	0	0
COL04	0	-3	0	COLO4 -tiOII	0	-1	0
COL05	0	1	0	COLOS OCCUPANTO	0	0	0
COL06	0	1	0	COLOG / KEO	0	0	0
COL07	0	1	0 -	COLOT V	0	1	0
LOAD CASE 6 - WIND CASE 1 TO LEFT			IIm:	LOAD CASE 12 - SEISMIC TO LEFT			
COL01	0	DIVO	110	COL01	0	0	0
COL02	0	PIL	0	COL02	0	0	0
COL03	0	1	0	COL03	0	0	0
COL04	0	-2	0	COL04	0	1	0
COL05	0	-4	0	COL05	0	0	0
COL06	0	-4	0	COL06	0	0	0
COL07	0	-2	0	COL07	0	-1	0

Nucor Building Systems

Frame: 2,3,4

Job #:

By:

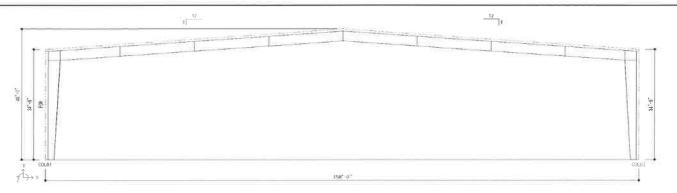
Job Name: Central Disposal

Page: 3

Date: 02/08/2024

Control #: P202402081520

Building: Transfer station *** Design Summary - Frame Reactions by Load Case ***



Member	X (kips	Y (kips	Z (kips	Member	X (kips	Y (kips	Z (kips
LOAD CASE 1 - DEAD			1	LOAD CASE 8 - WIND CASE 2 TO LEFT			
COL01	7	13	0	COL01	-22	-39	0
COL02	-7	13	0	COL02	36	-50	0
LOAD CASE 2 - COLLATERAL				LOAD CASE 9 - LONG. WIND 1 TO BACK			
COL01	5	6	0	COL01	1	-3	0
COL02	-5	6	0	CQL02	1	4	0
LOAD CASE 3 - ROOF LIVE				LOAD CASE 10 - LONG. WIND 1 TO FRONT			
COL01	18	24	0	COL01	-1	4	0
COL02	-18	24	0	COL02	-1	-3	0
LOAD CASE 4 - SNOW				LOAD CASE 11 - LONG. WIND 2/TO BACK			
COL01	37	50	0	COLOI , REU	-25	-48	0
COL02	-37	50	0	cbfds /	26	-42	0
LOAD CASE 5 - WIND CASE 1 TO RIGHT			I mi	LOAD CASE 12 - LONG. WIND 2 TO FRONT			
COL01	-11	5.0	11011	COL01	-26	-42	0
COL02	-4	M	0	COL02	25	-48	0
LOAD CASE 6 - WIND CASE 1 TO LEFT		,		LOAD CASE 13 - SEISMIC TO RIGHT			
COL01	4	7	0	COL01	-1	-1	0
COL02	11	-5	0	COL02	-1	1	0
LOAD CASE 7 - WIND CASE 2 TO RIGHT				LOAD CASE 14 - SEISMIC TO LEFT			
COL01	-36	-50	0	COL01	1	1	0
COL02	22	-39	0	COL02	1	-1	0

Preliminary Reactions

Nucor Building Systems

Frame: 5

Building: Transfer station

Job #:

By:

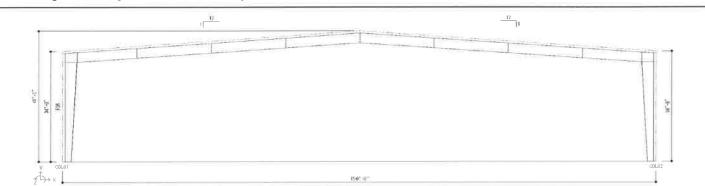
*** Design Summary - Frame Reactions by Load Case ***

Job Name: Central Disposal

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Date: 02/08/2024

Control #: P202402081520



Member	X (kips	Y (kips	Z (kips	Member	X (kips	Y (kips	Z (kips
LOAD CASE 1 - DEAD				LOAD CASE 8 - WIND CASE 2 TO LEFT			
COL01	4	8	0	COL01	-16	-25	0
COL02	-4	8	0	COL02	23	-32	0
LOAD CASE 2 - COLLATERAL				LOAD CASE 9 - LONG. WIND 1 TO BACK			
COL01	3	3	0	COL01	-4	-8	0
COL02	-3	3	0	COL02	5	-3	0
LOAD CASE 3 - ROOF LIVE				LOAD CASE 10 - LONG. WIND 1 TO FRONT			
COL01	9	12	0	COL01	-5	-3	0
COL02	-9	12	0	COL02	4	-8	0
LOAD CASE 4 - SNOW				LOAD CASE 11 - LONG, WIND 2/TO BACK			
COL01	19	25	0	COLOI, REU	-17	-31	0
COL02	-19	25	0	cbros	18	-26	0
LOAD CASE 5 - WIND CASE 1 TO RIGHT			Low !	LOAD CASE 12 - LONG. WIND 2 TO FRONT			
COL01	-11	3.0	1101	COL01	-18	-26	0
COL02	3	1-21	0	COL02	17	-31	0
LOAD CASE 6 - WIND CASE 1 TO LEFT				LOAD CASE 13 - SEISMIC TO RIGHT			
COL01	-3	-2	0	COL01	-1	-1	0
COL02	11	-9	0	COL02	-1	1	0
LOAD CASE 7 - WIND CASE 2 TO RIGHT				LOAD CASE 14 - SEISMIC TO LEFT			
COL01	-23	-32	0	COL01	1	1	0
COL02	16	-25	0	COL02	1	-1	0
	The second second	7					

Preliminary Reactions

B NAME: Central Disposal

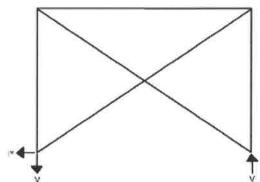
JOB NUMBER:

BUILDING: Transfer station

ENGINEER:

LONGITUDINAL X-BRACING REACTIONS

(These reactions must be combined with the appropriate longitudinal frame reactions)



Horizontal bracing reactions are orthogonal to horizontal frame reactions.

Line:	Bay:	H (kips	V (kips	Case
A	F.L. 1 - 2	12	16	WIND
A	F.L. 1 - 2	1	2	SEISMIC
A	F.L. 4 - 5	12	16	WIND
A	F.L. 4 - 5	1	2	SEISMIC
N	F.L. 2 - 3	12	16	WIND
N	F.L. 2 - 3	1	2	SEISMIC
N	F.L. 3 - 4	12	16	WIND
N	F.L. 3 - 4	1	2	SEISMIC
N	F.L. 4 - 5	12	16	WIND
N	F.L. 4 - 5	1	2	SEISMIC

Frames 2, 3 & 4

D-		X Y 12 19 -12 19	Z	RL X Y		RS	;	1 1	W1	- 11	W2	- 1																1410		F4									Documen		
Column 1 D D-D-D-		12 19	Z	v V				-	***	_	VVZ		W3		W4	_	W5		W6		W7	_	W8	-	W			W8 Z	1	E1		E2	7 V	E3	7 \	E4		×	Results		Z
Column 1 D D-D-D-		12 19		^ '	Z	X Y	Z	X	Y 2	z X	Y	ZX	Y	Z	X Y	Z	XY	Z			X Y -25 -48	4	26 -42	-	X Y	12		16	-1	-1		1	-		1	-2					
Column 1 D		I -12 19		18 24		37 50		-11			7	-3	6 -50		22 -39 36 -50	-	1 -3 1 4		-1 4 -1 -3	-	26 -42		25 -48	-	16	12		-16 -12				-1	_	2			-1		-		
D- D-		120		-18 24		-37 50)	-4	7	11	-5	2	2 -39		6 -50		1 4	ــــــــــــــــــــــــــــــــــــــ	-1 -3		20 -42		25 -46	_	10			-10 -12	-1-1		1	-		1 - 1			1 -1				
D- D-		1 1 4								=1	ГТ		1 1		T	П	Т					T			1															19.0	0.0
D-	D+RL		-	1			1				†		1																							_				43.0	0.0
D	D+RS	1					1																			\vdash		_		_	+	_	_	\vdash	-	-	\vdash		19.0 5.4	69.0 16.0	0.0 0.0 0.0
	D+.6W _x	1							0.6			_							-	-		-	_	-	_	+			+		+	_		++		_				23.2	0.0
		1	\vdash		_		-	-	-		0.6	_	0.6		-	\vdash	_	-				-	-			+														-11.0	0.0
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											\Box						0.6															_	_			_				17.2	0.0
		4																	0.6				\rightarrow	_	_	-	-		-			-	_	\vdash	-	+	+		-3.0	-9.8	0.0
		1								_	\vdash	_	+		+	-	-		-	-	0.6	_	0.6	-		+	-		+	-		\dashv	-			_			-3.6	-6.2	0.0 0.0 0.0 7.2
		1		_	-		4-	-	-	-+-	+		+-1	-	+	-				-			0.6	-	0	.6	\vdash												12.0	9.4	7.2
		- 3	\vdash			\rightarrow	+		_	-	\vdash																	0.6												28.6	0.0
D	D+.7E _X	1					1																							0.7			_		_		+			18.3 19.7	0.0
		1																				_	-			-			+		+	0.7	-	0.2	_	+-				17.6	0.7
		1										_		_	_	-	_			-		-	_	-		+			+-		+-+	-	_	.0.7	_	0.3	7			17.6	0.0
	STORE APILL	1	_	-	-			\vdash	0.45		-		+-1		+	-	_						++	-	-				+	\vdash									20.6	34.8	0.0
D	0+.75RL+.45W _X	1 1	\vdash	0,75		-	+	\vdash	0,45	-	0.45	_			_	$\pm \pm$																							27.3	40.2	0.0
				0.75			1	\vdash		_	30,93		0.45																							4				14.5	0.0
		1		0.75											0.45	5						_			_	_	\square		-		1	-	_	\vdash	_	_	-			19.5 35.7	0.0
		1		0.75													0.45						-	_	-	-	\vdash		+	-	+	-	_		-	+	-		25.1	38.8	0.0
		1		0.75		_	1	\vdash	_	_	-	_	\perp	-	_	\vdash	_		0,45		0.45	-	+	-	_	+						_								15.4	0.0
		1	\vdash	0.75			1	-	-	+-	\vdash		1		_	+			-1-		0.45		0.45																13.8	18.1	0.0
		1	\vdash	0.75		_	+-		_	-	+	_	1	-		\vdash									0.4	45										\perp				29.8	0.0 5.4 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
		1		0.75				\Box																_				0,45				_				-	+		25.5 34.8	44.2 54.3	0.0
D	D+.75RS+.45W _x	1				0.7	75		0.45														_		_	-			-			+	_	+	-	+	+		41.6	59.7	0.0
		1				0.7	_			_	0.45						-	-	-			-	-	-	_				+-1		+	_		+	\dashv	_	+			34.0	0.0
		1	-	_	-	0.7		-		-	+		0.45	-	0.4	+	_		_	\vdash				-	_		\vdash					\neg							29.9	39.0	0.0
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	D+.75RS+.525E _x	1 1	\vdash		\vdash	0.7		\vdash	-	_	1					+														0.525						_			39.2	56.0	0.0
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		1				0.7	75		_	_	\vdash	_	-		-	\vdash	_	-	_	-	-	-	-	-	-	+-	-		-		+	_				0,52		1	0.6	8.4	0.0
€	6D+.6W _x	0.6	-	_	-		-	\vdash	0.6		0.6	_	-		_	+	-		_	\vdash	\rightarrow	-	-																	15.6	0.0
		0.6	_	-	\vdash	_	_	\vdash	-		0.0		0,6																											-18.6	0.0
		0.6	-												0.	6																_				_				-12.0 9.6	0.0
		0.6	-												_		0;6							_	-	-	-		-		-	-	_	-	-	_	+-			13.8	0.0
		0.6	-							_		_			_	-	_	-	0.6		0.6	-	-		-	+	-		+				_		_					-17.4	0.0
		0.6	-		-		+-	\vdash		_				\vdash	-	+	-	-	-		0.6		0.6			T													-8.4	-13.8	0.0
		0.6	-		\vdash				-).6													7.2	1.8	7.2
		0.6	-																									0.6			\perp									21.0	0.0
	.6D+.7E _x	0.6	-																								-		_	0,7	+			+		+	+	-		10.7	0.0
		0.6														-	_		_			-			-	-	-		-		+	0,7	-	0.7						10.0	0.7
		0.6	+		\vdash			\vdash		-		_		-	-	+	-		-																	0	7			10.0	0.0
		0.6	11			!_		1 1									_																				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		14.4		

Frames 2, 3 & 4

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	D+RS	\vdash		_			_		+	-	+	\vdash	_			_	+	_	-	-	-			+	-		\vdash	-			+-+		\neg		-	\neg	1	\neg		-49.0	69.0	0.0
	D+.6W _x	-		_		-	_	4	\vdash	0.6		\vdash	_	+			+	_	-	\vdash		+		_	\neg	_	-	_	\vdash	_	1	_		+	-	_	+		11	-14.4	23.2	0.0
	DT.OVV _y	-			-		_	_	\leftarrow	0.6	-	0,6	_	+		_	+-	-	-	\vdash	-	+-		-	_	_	-	-	-		+	-	-	+	-	\rightarrow	+	-	++	-5.4	16.0	0.0
		\vdash	1	-	-	_	_	+	+	\rightarrow	-	0,6	_	+	_	_	+	\rightarrow	\rightarrow	+	-	+		+	_	-		_		_	+ +	-	-	+	-	+-	+	-	++	1.2	-4.4	0.0
		-	1	_		_	_	-	\vdash	_		\vdash	-	0,6		_	+	-	\rightarrow	\rightarrow		+		_	_	-		_	\vdash	_	+	-	_	+	-	_	+	_	++	9.6	-11.0	0.0
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		Ш	1	-			_	-	\leftarrow	_		-		\vdash			1	_	0.6	\rightarrow				-		-	-	_	-	_	+	\rightarrow	_	+	-	\rightarrow	+	-	+	-11.4	17.2	0.0
		\square	1						\vdash				_	-				_	-	\rightarrow	0,6	-	_	_	_	-		_	\vdash	_	+	-	_	+	\rightarrow	_	+		++	3.6	-6.2	0.0
			1	_						_				\vdash			-	_		\rightarrow	_	-	0.6	_		_		_		_	+		-	+	-	_	+		++	3.6	-9.8	0.0
			1						\vdash					-		_	\perp			\vdash		-		_	0.6				_	_	+	_	——	+	_		+		++	3.0		0.0
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	D+.7E _X		1																												0.7									-12.7	19.7	0.0
			1																														0.7	7						-11.3	18.3	0.0
			1																																	0,7				-12.0	20.4	0.0
			1																																			0.7	1_{\perp}	-12.0	20.4	-0.7
	D+.75RL+.45W _X		1		0,75		1			0.45																														-27.3	40.2	0.0
			1		0,75							0.45																												-20.6	34.8	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
			- 3		0.75									0.45																	1 1									-15.6	19.5	0.0
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-		\vdash	- 1		0,75	-	_	+	\vdash			-				Ť			0,45						=			\top		\neg								7		-25.1	38.8	0.0
				_	0,75	-	_	-	\vdash	-	+	-	\neg	+		_	1 1	_	5,44		0.45	1	-	1	_	7		_		_	1 1		\neg	+			+		11	-26.0	35.7	0.0
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		-	-1						\leftarrow	+	+	\vdash	_	+	-	-	+	_	\rightarrow	+		_	_	+	0,43	+-1	0.45	_	-	\rightarrow	+	-		+	-		+	\rightarrow	11	-25.5	44.2	0.0
		-	_1_		0,75		_	-	\vdash	_	-		_	+		_	+	_	-	+	\rightarrow	-	_	+	_		0.45	_	0.45	_	+	\rightarrow	-	+	-		+	-	++	-25.5	29.8	5.4
	- TERO 45W	_	- 1		0.75	_	_		\leftarrow	_	+	-	_	+	-	+	+	_	+	\vdash	_	-	_	+	_	-		-	0.45	_	+	-	-	+	-	-	+	-	++	-41.6	59.7	0.0
91	D+.75RS+.45W _X	-	11				0.3		\vdash	0,45	-	\vdash	_			-	+	_		\vdash		-		+	_	-	_	_		_	+	=	_	+	\rightarrow		+	\rightarrow	++	-34.8	54.3	0.0
			1				0.		\vdash	_	-	0.45	_	-		_				\vdash	_	-	_	-	_	-		_	-	_	+	-		+	\rightarrow		+	\rightarrow	+	-29.9	39.0	0.0
			1				0,1		\leftarrow	\rightarrow	-		_	0.45			-	_		\vdash		-	_	-	_	4-4		_	_	_	+	_	_	+	\rightarrow		+		+			0.0
			1				0,:		\leftarrow	_				\perp		0,	45					-		-		-		_	_	_		-		+	-	—	+		+	-23.6	34.0	0.0
			1				0.3							\perp					0.45	\vdash		-		-		4		_		_	+	_		+	_		+		+	-39.3	58.3	0.0
			1					75													0.45	-						_		_	\vdash	_		+	_	_	+	_	++	-40.2	55.2	0.0
			1				0													\sqcup			0,45								-	_		\vdash	_		\vdash		++	-28.1	37.6	0.0
			1				0.																		0.45							_		\perp			\perp		11	-28.5	34.9	0.0
			1					75																			0.45												11	-39.8	63.7	0.0
			1				0.																			\perp			0.45					\bot					1	-39.8	49.3	-5.4
	D+.75RS+.525E _x		1				0	75																							0,525								11	-40.3	57.0	0.0
			1				0.:	75																									0,525	5					11	-39.2	56.0	0.0
			1				0	75																											0	525				-39.8	57.6	0.0
			1				0.:	75																														0.525	11	-39.8	57.6	-0.5
	.6D+.6W _x		0,6							0,6																													11	-9.6	15.6	0.0
			0,6					1				0.6																												-0.6	8.4	0.0
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	.6D+.7E _x		0.6	_	1	_	_		\vdash	-	-		+	+	_	+	+	_	+-	+	_			+	_	-		+			0.7	-	0.7	+++	-	_	+	-	++	-6.5	10.7	0.0
		\vdash	0.6	_		_	_	-	\vdash	_	+		_	\vdash		_	+	_	-	\vdash		+		+				_	_		+	-	0,7	+	\rightarrow	0.7	+	-	++	-7.2	12.8	0.0
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Frame 5

		De	ad	R	oof Li	ve	Roof	f Snow	v \	Wind	1	Wi	nd 2	Wi	ind 3		Wind	4	W	ind 5	1 '	Wind 6		Wind 7		Wind	8	BF - W	Vind	BF -	wind	Se	ismic	:1	Seis	mic 2	RF	- Seism	IIC S	Seism	iic 2			1
i e)		RL			RS		W1			V2		<i>N</i> 3		W4			W5		W6		W7		W8		W		٧	V8		E1			E2		E3		E4	.	Re	sults	
		X Y		V		Z :		YZ	, v					X		7 V					V		7 Y	Y	7 X		Z :					Х		7			X	Υ	7)		Z	х		Z
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	D+.75RL+.45W _x		1		0.75					0,45																																8.8		
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			1		0,75															0.45												3										12.0	16.4	4
			1		0.75																	0.45																				11.5	18.7	
			1		0,75																			0.45																		6.1		1
			1		0.75																					0,45																5.7		
			1		0.75																							0,4	15												ii	13.8		8
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	D+.75RS+.45W _x		1					0.75		0.45																																16.3		
	100		1					0,75					0.45																													19.9		
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			1					0.75																0.45																		13.6		3
			1					0.75																		0,45																13.2	18.1	1
			1					0.75																				0.4	15													21.3		5
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	D+.75RS+.525E _x		1					0.75																									0,525					\perp		_		20.7		2
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			0.6												0,6																							\perp				-9.6		
			0.6														0.6	5																	_			\perp				-5.4	-8.4	
			0,6																	0.6																					1	1.8		
			0.6																			0,6																\vdash				1.2		
			0.6										Ü											0.6														\vdash	\rightarrow	\perp		-6.0	-12.0	
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			0.6																												0.6										1_1	4.2		2
	.6D+.7E _x		0.6																														0,7									3.5		
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Frame 5

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	.6D+.7E _x	0.0	Éi						-	_	\vdash	-	_	+		+-		-	+	_	+	_	+	_		+++			\neg			.7			+		-3.5	5.9
	.6D+.7E _x		Éi																												0	J	0.2				-3.5	5.9
	.6D+.7E _x	0.0	fi fi																													7	0.7		0.7		-3.5 -4.2	5.4 1.2 8.4 1.2.6 4.8 1.8 9.0 1.2.0 1.6.2 3.0 7.3 5.9 8.0 8.0 1.2.6

-26.0 -12.6 =7.2 9.6 37.0 0.0

Braced Frame Line

		De	ead	Ro	of Live	Ro	of Snov	v I	Wind :	1	Wind	2	Wir	nd 3	Wir	nd 4	Wir	nd 5	W	ind 6	T v	Wind 7	ΙV	Vind 8	1	BF - W	ind	BF - W	/ind	Seisn	nic 1	Sei	ismic 2	BF	- Seismi	ic	Seism	nic 2			
			D		RL		RS		W1		W2			/3		/4	l v			W6		W7		W8		W7		W	3	E:	1		E2		E3		E4			Results	
		X				X		z X		ZX				YZ	X I	γZ	х	/ Z	x	ΥZ		YZ			ZX							x	ΥZ	Х	Y 2	z >	KY	Z)	K Y	Z
Column 1			2		3		4		-2		1			5		4		5	5	-5																					
Column 3			4		8		10		-4		1			13	1 -	9	-10 -:		11	-13																					
COMMITTE											_																1				-1										-
Column 1	D		1																																						.0 0.0
	D+RL		1		1																															4				0.0 5.	.0 0.0
	D+RS		1				1																	\vdash	_	_	\vdash	_	_		_	\vdash			+	+	_				.0 0.0
	D+.6W _x		1	_	_	-			0,6			-		_		_		_	-	_	-	\vdash	-	-	_	_	-		-		-	-		-		+	-	+-+	_	0.0 0.	.8 0.0 .6 0.0
			1	\rightarrow	_	-			-		0,6	-		_	-	_		_	\vdash		-	-	+			+-	\vdash				+	H		+	+	+	+	+		0.0 -1.	.0 0.0
	-	+	1	-	_	+-	-		\vdash		-	\vdash	_	0.6	-	0.6		_	+		+					_	\vdash				_	\dagger				\rightarrow	_	1		0.0 -0.	
		+-+	1	_	_	+	-			_	$\overline{}$		-		-	0.0		0.6													1	T					\neg		_	-3.0 -1.	0 00
			1	1		\top		_												0,6																				3.0 -1.	0.0
			1																			0.6																		0.0 2.	.0 0.0
			1																					0.6					-		\perp							\perp		0.0 2.	0.0
			1																\sqcup							0,6	\vdash				-	_			\vdash	_		1		0.0 2.	0.0
			1			_		_				-		_		-		-	\vdash		+		-		-	-		0	.6		2	\vdash		_	+	+	-	+		0.0 2. 0.0 2.	.0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0
-	D+.7E _x	+	1			_			\vdash		-	\vdash		-				+	\vdash		+	-	-	-	_	_	\vdash		+-		0.7	+	0.7	_	\vdash	+	_	+		0.0 2.	.0 0.0
			1	1		-			1	_	+	\vdash	-	_		-		+-	\vdash		+		-	-	_	+	\vdash	-	1			1	0,7	_	0.7	+	-	+-+		0.0 2.	0.0
		+	1	-	-	+	-	-1-	\vdash	_	+	\vdash				_					+											\dagger					0	1.7		0.0 2.	
	D+.75RL+.45W _x	+-	1		0.75			-1-	0.45																															0.0 3.	.4 0.0
		\pm	1		0.75				\Box		0.45																									\equiv				0.0 4.	
			1		0.75									0.45																						\perp		4		0.0 2.	
			1		0.75											0.45					1				_				-		_	1		-	\vdash		4	1		0.0 2.	
		\perp	1		0,75				\vdash		_		_			_		0.45	\vdash	_	-		-		_	_	\vdash	-	-		-	\vdash		-	-	+	+	1-1		-2.3 2. 2.3 2.	
		+	1	-	0.75	_		_	\vdash	_		-		-	\vdash	_		_	\vdash	0.45	+	0.45	-		_		-	_	+		+-	+		+	\vdash	+	+	+		0.0 4.	
-			1	-	0.75	+-	-			_	-	-	_	_		_	_	_			+	0.45	+	0.45	_	+	\vdash		1							+		1 1		0.0 4.	.3 0.0
			1	1	0.75	_	\vdash		\vdash															0.43		0.45						\Box				\neg			_	0.0 4.	
		+ +	1	-	0.75					_			-															0.4	15											0.0 4.	.3 0.0
	D+.75RS+.45W _x		1				0.75		0,45																															0.0 4.	
			1				0.75				0.45															_								_			_	1		0.0 5.	
			1				0.75		\sqcup					0.45	\vdash			_		_	-		-		-	_	-	_	-	_	_	\vdash		-	\vdash	+	+	+		0.0 2. 0.0 3.	
		+	1	-			0.75	_		_	-		-	-		0.45				_	-		-		_	-	-	-	+		_	\vdash		+	\vdash	_	+	+-+		-2.3 2.	
		-	1	-		_	0.75		\vdash	_	_	-		_	\vdash	-		0.45	\vdash	0,45	+		-	-	_	-			+		-	+		+-		_	+	+		2.3 2.	
-		++	1	+		+-	0.75	-1-	+		+	\vdash				_		_	\vdash	0,45	+-	0,45							1			\Box						1 1		0.0 5.	
		+	1	+		-	0.75		+												1			0.45								\Box								0.0 5.	.0 0.0
			1			\top	0.75		\Box																	0.45														0.0 5.	
			1				0.75																					0,4	15			\sqcup			\vdash			+		0.0 5.	0.0
	D+.75RS+.525E _x		1				0.75														1_		-			-		_	-	0.5	25	\vdash		1	\vdash		-			0.0 5.	
			1				0,75	-			-	\square		_		-		_	\vdash	_			-	-	-	-	\vdash	-	-		-	\vdash	0,525		0,525	-	-	1		0.0 5. 0.0 5.	0.0
		+	1				0.75	_	+		-	\vdash		_		_		-	\vdash		+-		-	-	+		-	_	-		+	+		1	0,525	+	0.52	25	-1-	0.0 5.	0.0
-	.6D+.6W _x	+ +	0.6	+			0.75	-	0,6		-	\vdash		-					\vdash	_	+ -										\top	\Box				\neg	0.52			0.0 5. 0.0 0.	0.0
	,x		0.6								0.6								\Box																					0.0 1.	0.0
			0.6											0.6																										0.0 -1.	8 0.0
			0.6													0.6																\sqcup								0.0 -1.	.2 0.0
			0.6									Ш						0.6													_	\vdash		-			_			-3.0 -1.	
			0.6			_					-	\square		_		_		_		0.6			-			-		_			-	\vdash		-	-	-	-	+		3.0 -1. 0.0 1.	5 0.0
-			0.6						\vdash		-	\vdash				-	-	-	\vdash		1	0.6	-	-	\dashv	+	-	+			_	+	-	+		+	+	+		0.0 1.	2 0.0
		+-+	0,6	-		_	-	-		_	-	\vdash	_	-	\vdash	_		_	\vdash	_	+-		-	0,6	-	0.6		_	+		+	+			\vdash	+				0.0 1.	2 0.0
-			0,6	+			\vdash	-	\vdash		+	\vdash				_		_	\vdash		1					0.0		0	6			\Box								0.0 1.	2 0.0
	.6D+.7E _x		0.6																		1										0.7									0.0 1.	2 0.0
	^	-	0,6																														0.7							0.0 1.	2 0.0
			0,6																													\Box			0.7					0.0 1.	
			0,6																															1			0,	.7		0.0 1.	2 0.0
																																								-3.0 -1.	8 0.0

Braced Frame Line

I.D.																									0.0 4.
D	1		+-+-		-					+-															0.0 12.
D+RL	1	1			-								\rightarrow				_								0.0 14.
D+RS	1		1															_		-	+				0.0 1.
D+.6W _x	1				0.6								_					_		+	_				0,0 4.
	1					0,6												_						\vdash	
							0,6																	-	0.0 -3.
			1 1 1 -					0.6																	0,0 -1,
+			1 1		+++					0,6															-6.0 -3.
+			1 1 - 								0.6	1													6.6 -3.
	1						-	+-+-			- 0.0		0.6	_											0.0 4.
	1							+-+-	_			+	0.0	0.6					-						0.0 4
	1											\rightarrow	\rightarrow	0.6			+	_					-		0.0 4.
	1													\rightarrow		0.6	\rightarrow				+				0.0 4
	1																0,6					-11	-	-++	0.0 4
D+.7E _x																			0.7						
25.3150EX.3			++-																		0.7				0.0 4
			+	\rightarrow					-													0.7			0.0 4
	1							+-		+-		-											0.		0.0 4
	1					_					-	\rightarrow													0.0 8
D+.75RL+.45W _x	1	0.75			0.45						-	_	\rightarrow	\rightarrow				_							0.0 10
	3	0,75				0.45														+	+			++	0.0 4
	1	0.75					0.45																-	-+	0.0 6
	1	0.75						0.45																	0.0 6
	-1	0,75								0,45															-4.5 4
		0.75								1 1	0.45														5.0 4
			+						-	_			0.45												0.0 10
	1	0.75							_	+-			0.43	0.45			-								0.0 10
	1	0.75								-			\rightarrow	0,43		0:45	_	_		-					0.0 10
	1	0.75														0,45		-							0.0 10
	1	0.75															0.45	_							0.0 9
D+.75RS+.45W _x	1		0.75 0.75 0.75		0.45																				
-	1		0.75			0.45																			
+			0.75				0.45																		0.0 5
			0.75					0.45																	0,0 7
	1	_	0.75 0.75 0.75	-				1 1 5.4		0,45															-4.5 5
	1		0,75						_	UAS	++	_													5.0 5
	11		0.75							+	0,45	_	VIVA	\rightarrow				_	1	+					0.0 11
	1		0.75										0.45				_	_		-	-		-	\vdash	0.0 11
	1		0,75											0.45				_					-	+	0.0 11
	1		0.75 0.75 0.75 0.75													0.45		_						\rightarrow	
	1		0.75														0.45						-	\longrightarrow	0.0 11
D+.75RS+.525E _x			0.75			-1-1													0.525						0.0 11
DT.75R5T.525Lg			0.75 0.75 0.75				-			+										0	525				0.0 11
			0.75							-												0.525			0.0 11
	1		0.75				-			+		-		\rightarrow			-	$\neg \vdash$					0.52	5	0.0 11
	1		0,75																	-			1 -		0.0
.6D+.6W _x	0.6				0,6													_	+				+	+	0.0 3
	0.6					0.6											_		1	1 -	+	-	+-+-	+++	0.0 -5
	0,6						0,6														\rightarrow		-	++	
1	0.6							0,6																-	0.0 -3
	0.6		1-1-							0.6															-6.0 -5
		-	++-			_					0.6														6.6 -5
	0.6							+	\vdash	1	0.6		0.6												0.0 2
	0.6					\rightarrow	-			+	+	_	0.0	0.6		_									0.0 2
	0.6										+++	\rightarrow		0.6	_		+		+						0.0 2
	0.6													-		0.6	+	_	+-	+		-	+	+	0.0 2
	0.6																0.6			-		+		+	
.6D+.7E _X	0.6		1 1																0.7					$\perp \perp \downarrow \perp$	0.0
	0.6																				0.7				0.0 2
	0,6		+		+++							_										0.7			0.0 2
					1 1 1	1 1	1 1																		

6.6 14.0 0.0

