



Waukesha Water Utility

SERVING WAUKESHA SINCE 1886

115 DELAFIELD STREET
WAUKESHA, WI 53188-3615

Telephone: (262) 521-5272 • Fax: (262) 521-5265 • E-mail: contactus@waukesha-water.com

MEMORANDUM

Date: September 10, 2021

To: Dan Duchniak, P.E.

From: Chris Walter, P.E.

Re: Request for Approval of CP 5 - Change Order No. 003

On August 6, 2021, Change Order Request No. 003 was submitted by S.J. Louis, regarding horizontal directional drill (HDD) work on Contract Package 5. This request was evaluated in detail by the Construction Management Team and discussed with me at length. I concur with the recommendation by Black & Veatch to approve the proposed revisions to the HDD on Les Paul Parkway adjacent to Sunset Drive.

The contractor is requesting an additional HDD length of 287 feet, which results in a net contract price increase of \$186,112.56. They are also requesting an associated contract time increase of 4 days. The request is being recommended for approval for the following primary reasons:

- Increased angles will allow depth to be achieved sooner and provide greater protection of the existing roadway and utilities.
- Insufficient room for pipe laydown on the original exit side of the HDD.
- Added length and depth to mitigate incidental return risks.

Detailed supporting documentation with a description and engineered design for this HDD Crossing is enclosed with this memo. Along with our Construction Management team, I have reviewed and recommend approval of this Change Order. Please note that five other HDD crossings that were part of CO No. 003 were evaluated and denied. With this approval, the contractor takes full responsibility for the design and method of installation for this HDD crossing.

Recommended Motion: Move to approve of the noted portion of Change Order No. 003 for Contract Package 5 for a total of \$186,112.56 and 4 additional days of contract time.



Great Water Alliance
115 Delafield Street

Waukesha, WI, 53187
P: (262) 521-5272 F: (262) 521-5265

Waukesha Water Utility
Great Lakes Water Supply Program
CP5 - Return Flow Pipeline
S.J. Louis Construction, Inc.
1351 Broadway Street W PO Box 459
Rockville MN
USA 56369

Project No.: 199990-CP5
File No.: 80.1633

Submittal Item

Submittal Item No.:	D-330522-002-011 Rev.: 0
Submittal Set No.:	330522-009 Rev.: 0
Description:	CROSSING PLAN 2 (DWG C123-C127) - SIGNED/SEALED CERTIFICATE OF PLAN AND CALCULATIONS
Expedited Review:	No
Review Disposition:	Acknowledged
Status:	Approved

Specification Section/CSI Code:

Section Reference:

Drawing Reference:

33 05 22 - Horizontal Directional Drilling

Sub-Contractor:

Supplier:

Manufacturer:

Critical Path Item: ☐ Yes ☒ No

Deviation from Contract Requirements: ☐ None / ☐ Yes

Notes:

Workflow Status: Approved

Actioned By: Collin Kruse

Sample Received:

Sample Received Date:

Sample Delivery Method:

Review Due Date:

Actual Review Duration:

Days Overdue:

August 18, 2021

12

9

Review Comments:

This submittal item was marked as approved via the workflow approval of the linked submittal set on 8/9/2021 12:35 PM

Submittal Set No. 330522-009 – HDD Crossing Plan 2

Submittal Item D-330522-002-011– Signed Certificate – Acknowledged

Notes regarding D-330522-002-011 are as follows:

1. The calculations submitted were not reviewed.

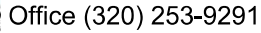
Subject to Excessive Review Clause: ☒ No / ☐ Yes

Engineer's review of submittals covers only general conformity to the Drawings and Specifications, external connections, and dimensions that affect the layout; it does not indicate a thorough review of all dimensions, quantities, and details of the material, equipment, device, or item covered. Engineer's review shall not relieve Contractor of sole responsibility for errors, omissions, or deviations in the drawings and data, nor of Contractor's sole responsibility for compliance with the Contract Documents.

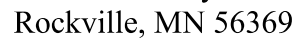
Attached: D-330522-002-011 - Certs and Calcs

Workflow Log

	07/28/2021	Submit	Trevor Scaife(TScaife)
CM - Submittal Coordinator 02	07/28/2021	Approve	Collin Kruse(CKruse)
PM - Submittal Coordinator 02	08/09/2021	Approve	Karissa Brunette(KBrunette)
CM - Submittal Coordinator 02	08/09/2021	Approve	Collin Kruse(CKruse)
CM - Submittal Coordinator 02	08/09/2021	Approve	Collin Kruse(CKruse)
	08/09/2021		Collin Kruse(CKruse)
	08/09/2021		Collin Kruse(CKruse)
	08/09/2021		Collin Kruse(CKruse)



COPIED: File SIGNED: Trevor Scaife



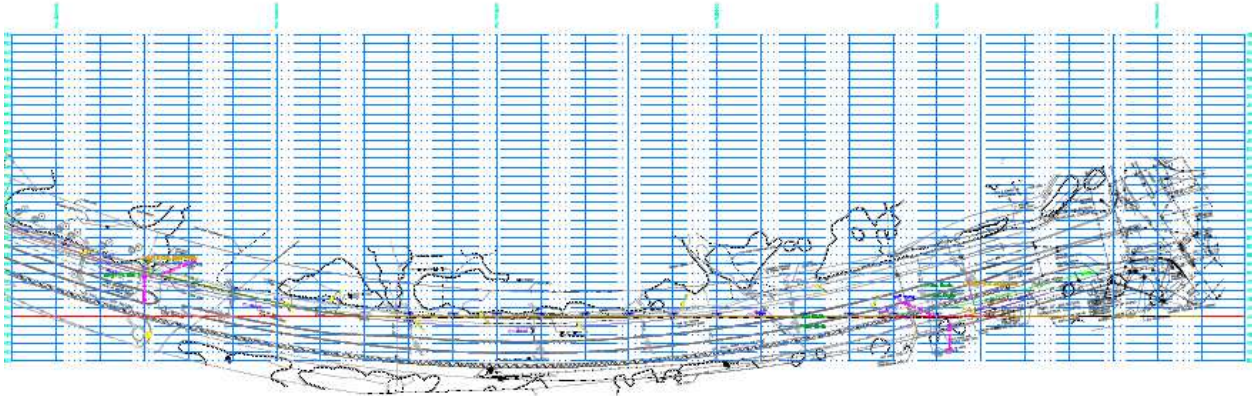
DATE: _____ Date: 2021.07.28 07:25:55-05'00'

Digitally signed by Trevor Scaife
DN: C=US, E=TrevorS@SJLouis.com, O=S.J.
Louis, CN=Trevor Scaife
Reason: I am the author of this document
Date: 2021.07.28 07:25:55-05'00'

Statement:

Estimate the pulling force for the referenced crossing. Based on information, SJL Construction plans to utilize a horizontal directional drilling technique to install a 36-in. return flow pipeline. Refer to the plan and profile below and attached information regarding the crossing and anticipated ground conditions.

SJL Construction
HDD#2-Unnamed
Tributary Pebble Brook



Assumptions and Rationale:

Within the limits of the bore (i.e., approximately 2,139 lin ft), SJL Construction plans to utilize a continuous borehole method that generally includes sequential activities of: a 10 5/8-in. pilot hole (with 12-deg entry/exit angles); ream passes with 30- to 54-in. openers/reamers (rock tooling); a mud pass using a 42 to 48-in. diameter ball; and pullback of the 36-in. carrier pipe (i.e., water filled). A bentonite slurry is planned as a lubricant and aid in borehole stability, and ground surface elevations for the borehole entry and exit points are relatively the same except as shown. Based on information in the Contract Documents, ground conditions along the alignment are anticipated to consist of medium dense silty sand and silt and dolomite rock.

References:

SJL Construction submittal for CP5 - 2 HDD Plan D-330522-002-009

AASHTO LRFD Bridge Design Specifications, 8th ed.

Buried Flexible Steel Pipe: Design and Structural Analysis, Engineering Practice No. 119

ASTM F1962-11, Standard Guide for Use of Maxi-Horizontal Directional Drilling for Placement of Polyethylene Pipe or Conduit Under Obstacles, Including River Crossings (per license agreement).

Estimate Pulling Force:

For the configuration shown above, estimate the pulling force based on ASTM F1962 reference. Below is an illustration of a crossing which identifies variables for this analysis, namely length and points of interest along the bore path.

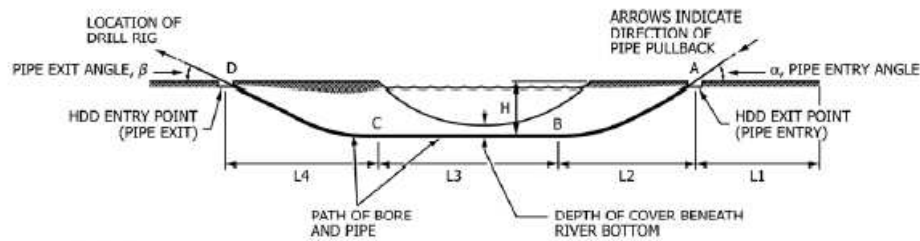


FIG. 1 Maxi-HDD for Obstacle (for example, River) Crossing

$$v_a := 0.1$$

: coefficient of friction applicable at the surface before the pipe enters borehole; pipe on rollers

$$v_b := 0.3$$

: coefficient of friction applicable w/in lubricated borehole

$$L_1 := 50 \text{ ft}$$

: additional pipe length required for handling and thermal effects, assumed

$$L_2 := 322 \text{ ft}$$

: approximate horizontal distance to achieve desired depth

$$L_3 := 1386 \text{ ft}$$

: approximate distance traversed at desired depth

$$L_4 := 402 \text{ ft}$$

: approximate horizontal distance to rise to surface

$$\alpha := 12 \text{ deg}$$

: borehole angle of pipe entry

$$\beta := 12 \text{ deg}$$

: borehole angle of pipe exit

Estimate Pulling Force cont'd:

$H := 50 \text{ ft}$: Approximate depth of borehole from ground surface

$OD_{pipe} := 38.3 \text{ in}$: Outside diameter of pipe

$ID_{pipe} := 30.919 \text{ in}$: Inside diameter of pipe

$t_{wall} := \frac{OD_{pipe} - ID_{pipe}}{2} = 3.69 \text{ in}$: Wall thickness of pipe

$DR := \frac{OD_{pipe}}{t_{wall}} = 10.4$: Dimension ratio

$\gamma_a := 0.955$: Specific gravity of pipe

$\gamma_b := 1.5$: Specific gravity of lubricant, bentonite

$\gamma_c := 1.0$: Specific gravity of ballast, water

$\rho_w := 62.4 \frac{\text{lb}}{\text{ft}^3}$: Density of water

$w_a := \pi \cdot OD_{pipe}^2 \cdot \frac{(DR-1)}{DR^2} \cdot \rho_w \cdot \gamma_a = 166.1 \frac{\text{lb}}{\text{ft}}$: Weight of empty pipe

$w_{b_empty} := \pi \cdot \frac{OD_{pipe}^2}{4} \cdot \rho_w \cdot \left(\gamma_b - \frac{4 \cdot \gamma_a \cdot (DR-1)}{DR^2} \right) = 582.8 \frac{\text{lb}}{\text{ft}}$: Net (upward) buoyant force on empty pipe

$w_b := \pi \cdot \frac{OD_{pipe}^2}{4} \cdot \rho_w \cdot \left(\gamma_b - \gamma_c \cdot \left(1 - \frac{2}{DR} \right)^2 \right) - w_a = 257.4 \frac{\text{lb}}{\text{ft}}$: Net (upward) buoyant force on pipe filled with ballast

$w_{ballast} := \pi \cdot \frac{ID_{pipe}^2}{4} \cdot \rho_w \cdot \gamma_c = 325 \frac{\text{lb}}{\text{ft}}$: Weight of ballast, check

$T_A := \exp(v_a \cdot \alpha) \cdot (v_a \cdot w_a \cdot (L_1 + L_2 + L_3 + L_4)) = 36627.3 \text{ lb}$: Pulling force on pipe at point A

$T_B := \exp(v_b \cdot \alpha) \cdot (T_A + v_b \cdot |w_b| \cdot L_2 + w_b \cdot H - v_a \cdot w_a \cdot L_2 \cdot \exp(v_a \cdot \alpha)) = 73377.1 \text{ lb}$
: Pulling force on pipe at point B

$T_C := T_B + v_b \cdot |w_b| \cdot L_3 - \exp(v_b \cdot \alpha) \cdot (v_a \cdot w_a \cdot L_3 \cdot \exp(v_a \cdot \alpha)) = 155396 \text{ lb}$

: Pulling force on pipe at point C

$T_D := \exp(v_b \cdot \beta) \cdot (T_C + v_b \cdot |w_b| \cdot L_4 - w_b \cdot H - \exp(v_b \cdot \alpha) \cdot (v_a \cdot w_a \cdot L_4 \cdot \exp(v_a \cdot \alpha))) = 177097.8 \text{ lb}$

: Pulling force on pipe at point D

These forces are considered to be a minimum requirement for assessing equipment.

Check stresses in pipe:

Estimate pulling force due to hydrokinetic pressure:

$$\Delta P := 10 \text{ psi}$$

: Hydrokinetic pressure, estimated

$$D_{hole} := 52 \text{ in}$$

: Backreamed hole diameter

$$\Delta T := \Delta P \cdot \frac{\pi}{8} (D_{hole}^2 - OD_{pipe}^2) = 4858.1 \text{ lbf}$$

: Pulling force from hydrokinetic pressure

Maximum axial tensile stress:

$$\sigma_{max} := (\max(T_A, T_B, T_C, T_D) + \Delta T) \left(\frac{1}{\pi \cdot OD_{pipe}^2} \right) \cdot \left(\frac{DR^2}{DR - 1} \right) = 453.5 \text{ psi}$$

Average axial tensile stress at respective locations:

$$\sigma_A := (T_A + \Delta T) \left(\frac{1}{\pi \cdot OD_{pipe}^2} \right) \cdot \left(\frac{DR^2}{DR - 1} \right) = 103.4 \text{ psi}$$

$$\sigma_B := (T_B + \Delta T) \left(\frac{1}{\pi \cdot OD_{pipe}^2} \right) \cdot \left(\frac{DR^2}{DR - 1} \right) = 195 \text{ psi}$$

$$\sigma_C := (T_C + \Delta T) \left(\frac{1}{\pi \cdot OD_{pipe}^2} \right) \cdot \left(\frac{DR^2}{DR - 1} \right) = 399.4 \text{ psi}$$

$$\sigma_D := (T_D + \Delta T) \left(\frac{1}{\pi \cdot OD_{pipe}^2} \right) \cdot \left(\frac{DR^2}{DR - 1} \right) = 453.5 \text{ psi}$$



Axial bending stress (per ASTM F1962):

$$R_1 := 1000 \text{ ft}$$

: Local radius of curvature, pipe entry

$$R_2 := 2000 \text{ ft}$$

: Local radius of curvature, pipe exit

$$E_a := 110 \text{ ksi}$$

: Apparent Modulus of Elasticity

$$\varepsilon_{a1} := \frac{OD_{pipe}}{2 \cdot R_1} = 0.002 \quad \varepsilon_{a2} := \frac{OD_{pipe}}{2 \cdot R_2} = 0.001 \quad \text{: Peak axial strain}$$

$$\sigma_{a1} := E_a \cdot \varepsilon_{a1} = 175.5 \text{ psi} \quad \sigma_{a2} := E_a \cdot \varepsilon_{a2} = 87.8 \text{ psi} \quad \text{: Peak axial stress}$$

Peak tensile stress at respective locations (per ASTM F1962):

$$\sigma_{pA} := \sigma_A + \sigma_{a1} = 278.9 \text{ psi}$$

$$\sigma_{pB} := \sigma_B + \sigma_{a1} = 370.5 \text{ psi}$$

$$\sigma_{pC} := \sigma_C + \sigma_{a2} = 487.1 \text{ psi}$$

$$\sigma_{pD} := \sigma_D + \sigma_{a2} = 541.2 \text{ psi}$$

$$SPS := 1100 \text{ psi}$$

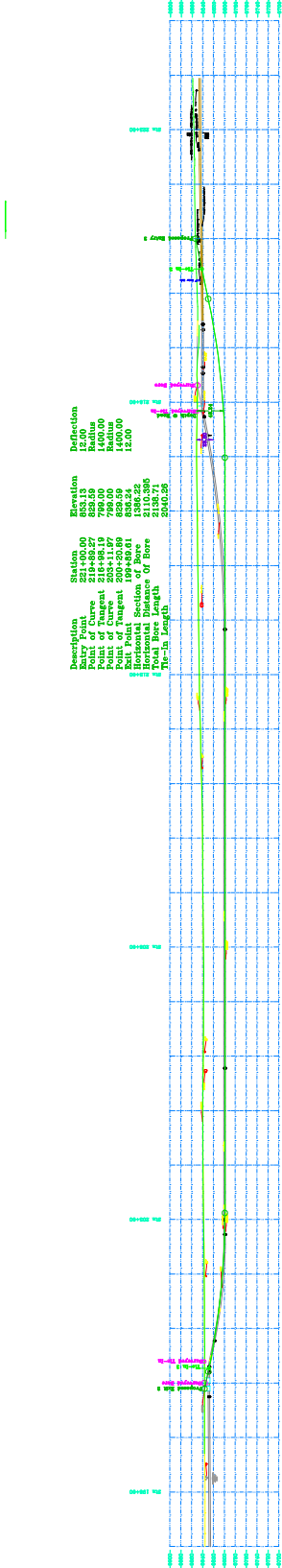
: Safe pull tensile stress, Table X1.1

$$\sigma_{pi} < SPS$$

: OK

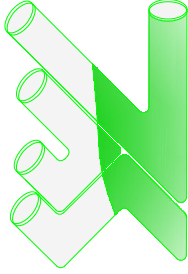
$$ATL := SPS \cdot \pi \cdot OD_{pipe}^2 \left(\frac{1}{DR} - \frac{1}{DR^2} \right) = 220.7 \text{ tonf} \quad \text{: Allowable tensile load (safe pull tensile load)}$$

SJL Constuction HDD#2-Unnamed Tributary Pebble Brook



Circumstance	Justified (%)	Not justified (%)
If someone is attacking you	85	15
If someone is threatening you	75	25
If someone is stealing from you	65	35
If someone is harassing you	55	45
If someone is insulting you	45	55

Date	Revision	Drawn By
9/10/20	1	SL
10.16.20	2	GL
04.07.21	3	GL
04.16.21	4	GL



**S.J. LOUIS
CONSTRUCTION, INC.**

Project 42081-30

Date	04.16.2021
Sheet 1	